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Oliver, R. Crant. 2235 300T-12AN BOUL-V97 NEW VORK

THE

AMERICAN HOUSE-CARPENTER:

A TREATISE UPON

ARCHITECTURE,

CORNICES AND MOULDINGS

FRAMING,

DOORS, WINDOWS, AND STAIRS.

TOGETHER WITH

THE MOST IMPORTANT PRINCIPLES

OF

PRACTICAL GEOMETRY.

BY R. G. HATFIELD, ARCHITECT.

SECOND EDITION.

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Allustrated by more than three hundred Bugrabings.

NEW-YORK & LONDON: WILEY AND PUTNAM.

1845.

Oliber R. Ert

2285 SOUTHEAD NEW Y



Entered according to the Act of Congress, in the year 1844, BY R. G. HATFIELD, In the Clerk's office of the District Court of the Southern District of New-York.



PREFACE.

THIS book is intended for carpenters—for masters, journeymen and apprentices. It has long been the complaint of this class that architectural books, intended for their instruction, are of a price so high as to be placed beyond their reach. This is owing, in a great measure, to the costliness of the plates with which they are illustrated : an unnecessary expense, as illustrations upon wood, printed on good paper, answer every useful purpose. Wood engravings, too, can be distributed among the letter-press; an advantage which plates but partially possess, and one of great importance to the reader.

Considerations of this kind induced the author to undertake the preparation of this volume. The subject matter has been gleaned from works of the first authority, and subjected to the most careful examination. The explanations have all been written out from the figures themselves, and not taken from any other work; and the figures have all been drawn expressly for this book. a doing this, the utmost care has been taken to measure the solution and the figures themselves are the solution and the solution and the solution are the solution and the solution and the solution are the solution are the solution and the solution are the solution are the solution and the solution are the solution and the solution are the solution and the solution are the solution are the solution and the solution are the solution and the solution are the solution are the solution are the solution and the solution are the solution and the solution are the solution are the solution and the solution are the solution are the solution are the solution are the solution and the solution are the solution are the solution are the solution and the solution are the solution ar

PREFACE.

The attention of the reader is particularly directed to the following new inventions, viz : an easy method of describing the curves of mouldings through three given points; a rule to determine the projection of eave cornices; a new method of proportioning a cornice to a larger given one; a way to determine the lengths and bevils of rafters for hip-roofs; a way to proportion the rise to the tread in stairs; to determine the true position of butt-joints in hand-rails; to find the bevils for splayed-work ; a general rule for scrolls, &c. Many problems in geometry, also, have been simplified, and new ones introduced. Much labour has been bestowed upon the section on stairs, in which the subject of hand-railing is presented, in many respects, in a new, and, it is hoped, more practical form than in previous treatises on that subject.

The author has endeavoured to present a fund of useful information to the *American house-carpenter* that would enable him to excel in his vocation; how far he has been successful in that object, the book itself must determine.

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PREFACE TO THE SECOND EDITION. .

In preparing a second edition, the author regrets his want of leisure to give the work that thorough revision, which is demanded by the importance and intricacy of the subjects treated of. He has corrected all the typographical errors in the references, &c., that he could discover, and added a Section on the subject of Shadows. He cannot refrain from giving expression to the satisfaction which he feels at the unexpected success of his undertaking. But it is evident that in a wide-spread, new country like ours, works of a practical character, adapted to the wants of the people, and calculated to instruct our operative citizens in the everyday employment of their heads and hands, cannot but meet with a favourable reception. In another edition, perhaps, opportunity will be given for additions and improvements of a still more important nature.

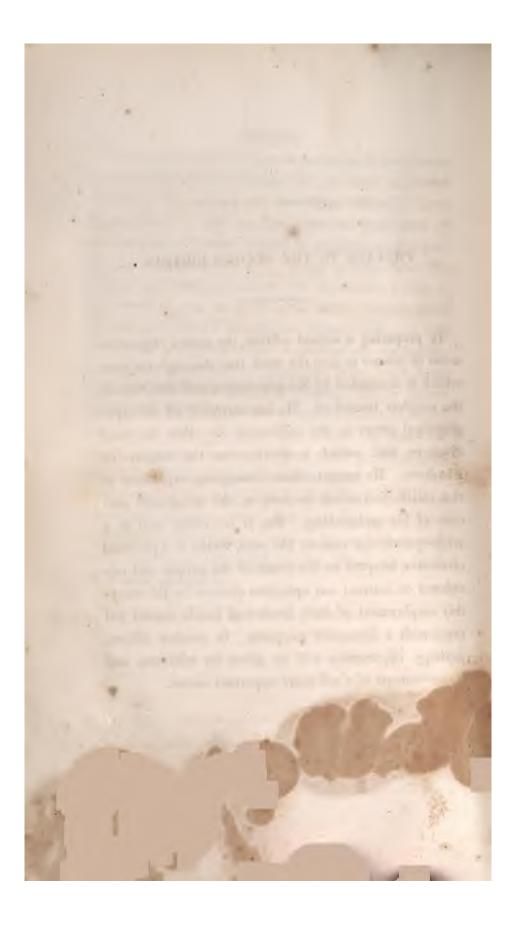


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INTRODUCTION.

ART. 1.—A knowledge of the properties and principles of lines can best be acquired by practice. Although the various problems throughout this work may be understood by inspection, yet they will be impressed upon the mind with much greater force, if they are actually performed with pencil and paper by the student. Science is acquired by study-art by practice : he, therefore, who would have any thing more than a theoretical, (which must of necessity be a superficial,) knowledge of Carpentry, will attend to the following directions, provide himself with the articles here specified, and perform all the operations described in the following pages. Many of the problems may appear, at the first reading, somewhat confused and intricate; but by making one line at a time, according to the explanations, the student will not only succeed in copying the figures correctly, but by ordinary attention will learn the principles upon which they are based, and thus be able to make them available in any unexpected case to which they may apply.

2.—The following articles are necessary for drawing, viz: a drawing-board, paper, drawing-pins or mouth-glue, a sponge, a T-square, a set-square, two straight-edges, or flat rulers, a lead pencil, a piece of india-rubber, a cake of india-ink, a set of drawing-instruments, and a scale of equal parts.

3.—The size of the *drawing-board* must be regulated according to the size of the drawings which are to be made upon it. Yet for ordinary practice, in learning to draw, a board about 15

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by 20 inches, and one inch thick, will be found large enough, and more convenient than a larger one. This board should be well-seasoned, perfectly square at the corners, and without clamps on the ends. A board is better without clamps, because the little service they are supposed to render by presenting the board from warping, is overbalanced by the consideration that the shrinking of the panel leaves the ends of the clamps projecting beyond the edge of the board, and thus interfering with the proper working of the stock of the T-square. When the stuff is well-seasoned, the warping of the board will be but trifling; and by exposing the rounding side to the fire, or to the sun, it may be brought back to its proper shape.

4.—For mere line drawings, the *paper* need not commonly be what is called drawing-paper; as this is rather costly, and will, where much is used, make quite an item of expense. Cartridge-paper, as it is called, of about 20 by 26 inches, and of as good a quality nearly as drawing-paper, can be bought for about 50 cts. a quire, or 2 pence a sheet; and each sheet may be cut in halves, or even quarters, for practising. If the drawing is to be much used, as working drawings generally are, cartridgepaper is much better than the other kind.

5.—A drawing-pin is a small brass button, having a steel pin projecting from the under side. By having one of these at each corner, the paper can be fixed to the board; but this can be done in a much better manner with *mouth-glue*. The pins will prevent the paper from changing its position on the board; but, more than this, the glue keeps the paper perfectly tight and smooth, thus making it so much the more pleasant to work on.

To attach the paper with mouth-glue, lay it with the bottom side up, on the board; and with a straight-edge and penknife, cut off the rough and uneven edge. With a sponge moderately wet, rub all the surface of the paper, except a strip around the edge about half an inch wide. As soon as the glistening of the water disappears, turn the sheet over, and place it upon the

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INTRODUCTION.

board just where you wish it glued. Commence upon one of the longest sides, and proceed thus: lay a flat ruler upon the paper, parallel to the edge, and within a quarter of an inch of it. With a knife, or any thing similar, turn up the edge of the paper against the edge of the ruler, and put one end of the cake of mouth-glue between your lips to dampen it. Then holding it upright, rub it against and along the entire edge of the paper that is turned up against the ruler, bearing moderately against the edge of the ruler, which must be held firmly with the left hand. Moisten the glue as often as it becomes dry, until a sufficiency of it is rubbed on the edge of the paper. Take away the ruler, restore the turned-up edge to the level of the board, and lay upon it a strip of pretty stiff paper. By rubbing upon this, not very hard but pretty rapidly, with the thumb nail of the right hand, so as to cause a gentle friction, and heat to be imparted to the glue that is on the edge of the paper, you will make it adhere to the board. The other edges in succession must be treated in the same manner.

Some short distances along one or more of the edges, may afterwards be found loose: if so, the glue must again be applied, and the paper rubbed until it adheres. The board must then be laid away in a warm or dry place; and in a short time, the surface of the paper will be drawn out, perfectly tight and smooth, and ready for use. The paper dries best when the board is laid level. When the drawing is finished, lay a straight-edge upon the paper, and cut it from the board, leaving the glued strip still attached. This may afterwards be taken off by wetting it freely with the sponge; which will soak the glue, and loosen the paper. Do this as soon as the drawing is taken off, in order that the board may be dry when it is wanted for use again. Care must be taken that, in applying the glue, the edge of the paper does not become damper than the rest: if it should, the paper must be laid aside to dry, (to use at another time,) and another sheet be used in its place.

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AMERICAN HOUSE CARPENTER.

Sometimes, especially when the drawing board is new, the paper will not stick very readily; but by persevering, this difficulty may be overcome. In the place of the mouth-glue, a strong solution of gum-arabic may be used, and on some accounts is to be preferred; for the edges of the paper need not be kept dry, and it adheres more readily. Dissolve the gum in a sufficiency of warm water to make it of the consistency of linseed oil. It must be applied to the paper with a brush, when the edge is turned up against the ruler, as was described for the mouth-glue. - If two drawing-boards are used, one may be in use while the other is laid away to dry; and as they may be cheaply made, it is advisable to have two. The drawing-board having a frame around it, commonly called a panel-board, may afford rather more facility in attaching the paper when this is of the size to suit; yet it has objections which overbalance that consideration.

6.—A *T*-square of mahogany, at once simple in its construction, and affording all necessary service, may be thus made. Let the stock or handle be seven inches long, two and a quarter inches wide, and three-eighths of an inch thick: the blade, twenty inches long, (exclusive of the stock,) two inches wide, and one-eighth of an inch thick. In joining the blade to the stock, a very firm and simple joint may be made by dovetailing it—as shown at Fig. 1.

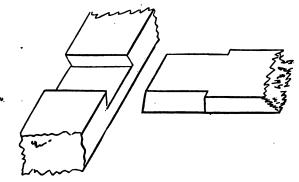


Fig. 1.

INTRODUCTION.

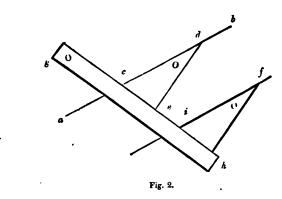
7.—The set-square is in the form of a right-angled triangle; and is commonly made of mahogany, one-eighth of an inch in thickness. The size that is most convenient for general use, is six inches and three inches respectively for the sides which contain the right angle; although a particular length for the sides is by no means necessary. Care should be taken to have the square corner exactly true. This, as also the T-square and rulers, should have a hole bored through them, by which to hang them upon a nail when not in use.

8.—One of the *rulers* may be about twenty inches long, and the other six inches. The *pencil* ought to be hard enough to retain a fine point, and yet not so hard as to leave ineffaceable marks. It should be used lightly, so that the extra marks that are not needed when the drawing is inked, may be easily rubbed off with the rubber. The best kind of *india-ink* is that which will easily rub off upon the plate; and, when the cake is rubbed against the teeth, will be free from grit.

9.—The drawing-instruments may be purchased of mathematical instrument makers at various prices: from one to one hundred dollars a set. In choosing a set, remember that the lowest price articles are not always the cheapest. A set, comprising a sufficient number of instruments for ordinary use, well made and fitted in a mahogany box, may be purchased at Pike and Son's, (Broadway, near Maiden-lane, N. Y.,) for three or four dollars. The compasses in this set have a *needle* point, which is much preferable to a common point.

10.—The best scale of equal parts for carpenters' use, is one that has one-eighth, three-sixteenths, one-fourth, three-eighths, one-half, five-eighths, three-fourths, and seven-eighths of an inch, and one inch, severally divided into *twelfths*, instead of being divided, as they usually are, into tenths. By this, if it be required to proportion a drawing so that every foot of the object represented will upon the paper measure one-fourth of an inch, use that part of the scale which is divided into one-fourths of an inch, taking for every foot one of those divisions, and for every inch one of the subdivisions into twelfths; and proceed in like manner in proportioning a drawing to any of the other divisions of the scale. An instrument in the form of a semi-circle, called a *protractor*, and used for laying down and measuring angles, is of much service to surveyors, but not much to carpenters.

11.—In drawing parallel lines, when they are to be parallel to either side of the board, use the T-square; but when it is required to draw lines parallel to a line which is drawn in a direction oblique to either side of the board, the set-square must be used. Let $a \ b$, (Fig. 2,) be a line, parallel to which it is



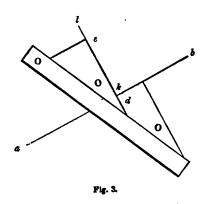
desired to draw one or more lines. Place any edge, as c d, of the set-square even with said line; then place the ruler, g h, against one of the other sides, as c e, and hold it firmly; slide the set-square along the edge of the ruler as far as it is desired, as at f; and a line drawn by the edge, i f, will be parallel to a b.

12.—To draw a line, as k i, (Fig. 3,) perpendicular to another, as a b, set the shortest edge of the set-square at the line, a b; place the ruler against the longest side, (the hypothenuse of the right-angled triangle;) hold the ruler firmly, and slide the setsquare along until the side, e d, touches the point, k; then the line, l k, drawn by it, will be perpendicular to a b. In like

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manner, the drawing of other problems may be facilitated, as will be discovered in using the instruments.



13.—In drawing a problem, proceed, with the pencil sharpened to a point, to lay down the several lines until the whole figure is completed; observing to let the lines cross each other at the several angles, instead of merely meeting. By this, the length of every line will be clearly defined. With a drop or two of water, rub one end of the cake of ink upon a plate or saucer, until a sufficiency adheres to it. Be careful to dry the cake of ink; because if it is left wet, it will crack and crumble in pieces. With an inferior camel's-hair pencil, add a little water to the ink that was rubbed on the plate, and mix it well. It should be diluted sufficiently to flow freely from the pen, and yet be thick enough to make a black line. With the hair pencil, place a little of the ink between the nibs of the drawing-pen, and screw the nibs together until men makes a fine line. Beginning with the curved lines, proceed where all the lines of the figure; being careful now to make every line wits requisite length. If they are a trifle too short or too long, the drawing will have a ragged appearance; and this is opposed to that meatness and accuracy which is indispensable to a good drawing. When the ink is dry, efface the pencil-marks with the india-rubber. If

the pencil is used lightly, they will all rub off, leaving those lines only that were inked.

14.—In problems, all auxiliary lines are drawn light; while the lines given and those sought, in order to be distinguished at a glance, are made much heavier. The heavy lines are made so, by passing over them a second time, having the nibs of the pen separated far enough to make the lines as heavy as desired. If the heavy lines are made before the drawing is cleaned with the rubber, they will not appear so black and neat; because the india-rubber takes away part of the ink. If the drawing is a ground-plan or elevation of a house, the shade-lines, as they are termed, should not be put in until the drawing is shaded; as there is danger of the heavy lines spreading, when the brush, in shading or coloring, passes over them. If the lines are inked with common writing-ink, they will, however fine they may be made, be subject to the same evil; for which reason, india-ink is the only kind to be used.

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SECTION I.-PRACTICAL GEOMETRY.

DEFINITIONS.

15.—Geometry treats of the properties of magnitudes.

16.—A point has neither length, breadth, nor thickness.

17.—A line has length only.

18.—Superficies has length and breadth only.

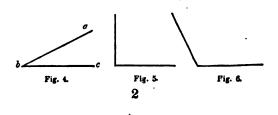
19.—A plane is a surface, perfectly straight and even in every direction; as the face of a panel when not warped nor winding.

20.-A solid has length, breadth and thickness.

21.—A right, or straight, line is the shortest that can be drawn between two points.

22.—Parallel lines are equi-distant throughout their length.

23.—An angle is the inclination of two lines towards one another. (Fig. 4.)



24.—A right angle has one line perpendicular to the other. (Fig. 5.)

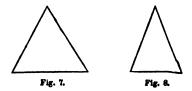
25.—An oblique angle is either greater or less than a right angle. (Fig. 4 and 6.) .

26.—An acute angle is less than a right angle. (Fig. 4.)

27.—An obtuse angle is greater than a right angle. (Fig. 6.)

When an angle is denoted by three letters, the middle one, in the order they stand, denotes the angular point, and the other two the sides containing the angle; thus, let $a \ b \ c$, (Fig. 4,) be the angle, then b will be the angular point, and $a \ b$ and $b \ c$ will be the two sides containing that angle.

28.—A triangle is a superficies having three sides and angles. (Fig. 7, 8, 9 and 10.)



29.—An equi-lateral triangle has its three sides equal. (Fig. 7.)

30.—An isoceles triangle has only two sides equal. (Fig. 8.)

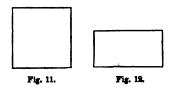
31.—A scalene triangle has all its sides unequal. (Fig. 9)



32.—A right-angled triangle has one right angle. (Fig. 10.) 33.—An acute-angled triangle has all its angles acute. (Fig. 7 and 8.)

34.—An obtuse-angled triangle has one obtuse angle. (Fig. 9.)

35.—A quadrangle has four sides and four angles. (Fig. 11 to 16.)

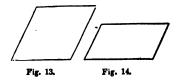


36.—A parallelogram is a quadrangle having its opposite sides parallel. (*Fig.* 11 to 14.)

· 37.—A rectangle is a parallelogram, its angles being right angles. (Fig. 11 and 12.)

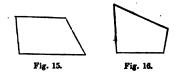
38.—A square is a rectangle having equal sides. (Fig. 11.)

39.—A rhombus is an equi-lateral parallelogram having oblique angles. (Fig. 13.)



40.—A rhomboid is a parallelogram having oblique angles. (Fig. 14.)

41.—A trapezoid is a quadrangle having only two of its sides parallel. (Fig. 15.)



42.—A trapezium is a quadrangle which has no two of its sides parallel. (Fig. 16.)

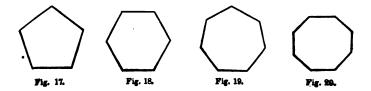
43.—A polygon is a figure bounded by right lines.

44.—A regular polygon has its sides and angles equal.

45.—An irregular polygon has its sides and angles unequal.

46.—A trigon is a polygon of three sides, (Fig. 7 to 10;) a tetragon has four sides, (Fig. 11 to 16;) a pentagon has

five, (Fig. 17;) a hexagon six, (Fig. 18;) a heptagon seven, (Fig. 19;) an octagon eight, (Fig. 20;) a nonagon nine; a decagon ten; an undecagon eleven; and a dodecagon twelve sides.

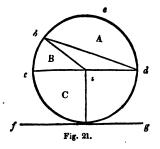


47.—A circle is a figure bounded by a curved line, called the circumference; which is every where equi-distant from a certain point within, called its centre.

The circumference is also called the *periphery*, and sometimes the *circle*.

48.—The radius of a circle is a right line drawn from the centre to any point in the circumference. (a b, Fig. 21.)

All the *radii* of a circle are equal.



49.—The diameter is a right line passing through the centre, and terminating at two opposite points in the circumference. Hence it is twice the length of the radius. (c d, Fig. 21.)

50.—An arc of a circle is a part of the circumference. (c b or b e d, Fig. 21.)

51.—A chord is a right line joining the extremities of an arc. (b d, Fig. 21.)

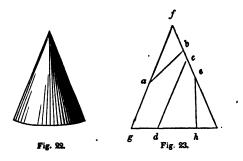
52.—A segment is any part of a circle bounded by an arc and its chord. (A, Fig. 21.)

53.—A sector is any part of a circle bounded by an arc and two radii, drawn to its extremities. (B, Fig. 21.)

54.—A quadrant, or quarter of a circle, is a sector having a quarter of the circumference for its arc. (C, Fig. 21.)

55.—A tangent is a right line, which in passing a curve, touches, without cutting it. (fg, Fig. 21.)

56.—A cone is a solid figure standing upon a circular base diminishing in straight lines to a point at the top, called its vertex. (Fig. 22.)



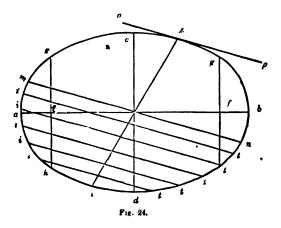
57.—The axis of a cone is a right line passing through it, from the vertex to the centre of the circle at the base.

58.—An *ellipsis* is described if a cone be cut by a plane, not parallel to its base, passing quite through the curved surface.
(a b, Fig. 23.)

59.—A parabola is described if a cone be cut by a plane, parallel to a plane touching the curved surface. (c d, Fig. 23 c d being parallel to fg.)

60.—An hyperbola is described if a cone be cut by a plane, parallel to any plane within the cone that passes through its vertex. (e h, Fig. 23.)

61.—Foci are the points at which the pins are placed in describing an ellipse. (See Art. 115, and f, f, Fig. 24.)



62.—The transverse axis is the longest diameter of the ellipsis. (a b, Fig. 24.)

63.—The conjugate axis is the shortest diameter of the ellipsis; and is, therefore, at right angles to the transverse axis. (c d, Fig. 24.)

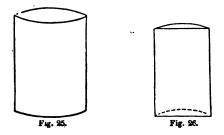
64.—The *parameter* is a right line passing through the focus of an ellipsis, at right angles to the transverse axis, and terminated by the curve. (g h and g t, Fig. 24.)

65.—A diameter of an ellipsis is any right line passing through the centre, and terminated by the curve. (k l, or m n, Fig. 24.)

66.—A diameter is conjugate to another when it is parallel to a tangent drawn at the extremity of that other—thus, the diameter, m n, (Fig. 24,) being parallel to the tangent, o p, is therefore conjugate to the diameter, k l.

67.—A double ordinate is any right line, crossing a diameter of an ellipsis, and drawn parallel to a tangent at the extremity of that diameter. (*i* t, Fig. 24.)

68.—A cylinder is a solid generated by the revolution of a right-angled parallelogram, or rectang.e, about one of its sides; and consequently the ends of the cylinder are equal circles. (Fig. 25.)



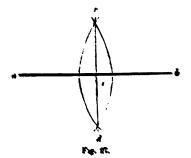
69.—The axis of a cylinder is a right line passing through it, from the centres of the two circles which form the ends.

70.—A segment of a cylinder is comprehended under three planes, and the curved surface of the cylinder. Two of these are segments of circles : the other plane is a parallelogram, called by way of distinction, the *plane of the segment*. The circular segments are called, the ends of the cylinder. (*Fig.* 26.)

PROBLEMS.

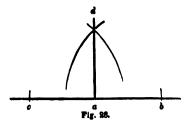
RIGHT LINES AND ANGLES.

71. To bisect a line. Upon the ends of the line, a b, (Fig. M7.) an control, with any distance for radius greater than half



a b, describe arcs cutting each other in c and d; draw the line, o d, and the point, c, where it cuts a b, will be the middle of the line, a b.

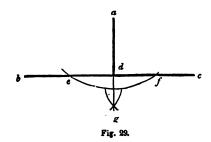
In practice, a line is generally divided with the compasses, or dividers; but this problem is useful where it is desired to draw, at the middle of another line, one at right angles to it. (See Art. 85.)



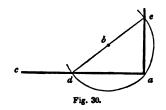
72.—To erect a perpendicular. From the point, a, (Fig. 28,)

set off any distance, as a b, and the same distance from a to c_{\downarrow} upon c, as a centre, with any distance for radius greater than c a, describe an arc at d; upon b, with the same radius, describe another at d; join d and a, and the line, d a, will be the perpendicular required.

This, and the three following problems, are more easily performed by the use of the set-square—(see Art. 12.) Yet they are useful when the operation is so large that a set-square cannot be used.



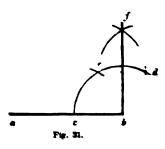
73.—To let fall a perpendicular. Let a, (Fig. 29,) be the point, above the line, b c, from which the perpendicular is required to fall. Upon a, with any radius greater than a d, describe an arc, cutting b c at e and f; upon the points, e and f, with any radius greater than e d, describe arcs, cutting each other at g; join a and g, and the line, a d, will be the perpendicular required.



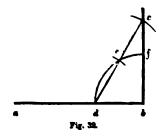
74.—To erect a perpendicular at the end of a line. Let a, (Fig. 30,) at the end of the line, c a, be the point at which the perpendicular is to be erected. Take any point, as b, above the

line, c a, and with the radius, b a, describe the arc, d a e; through d and b, draw the line, d e; join e and a, then e a will be the perpendicular required.

The principle here made use of, is a very important one; and is applied in many other cases—(see Art. 81, b, and Art. 84. For proof of its correctness, see Art. 156.)



14. a.-. A second method. Let b. (Fig. 31,) at the end of the line, a b, be the point at which it is required to erect a perpendicular. Upon b, with any radius less than b a, describe the arc, $c \in d$; upon c, with the same radius, describe the small arc at c, and upon c, another at d; upon c and d, with the same or any other radius greater than half c d, describe arcs intersecting at f; join f and b, and the line, f b, will be the perpendicular required.



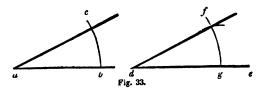
74, b.—A third method. Let b, (Fig. 32,) be the given point at which it is required to erect a perpendicular. Upon b, with any radius less than b a, describe the quadrant, d e f; upon d, with the same radius, describe an arc at e, and upon e, another at c;

through d and e, draw dc, cutting the arc in c; join c and b, then cb will be the perpendicular required.

This problem can be solved by the six, eight and ten rule, as it is called; which is founded upon the same principle as the problems at Art. 103, 104; and is applied as follows. Let a d, (Fig. 30,) equal eight, and a e, six; then, if d e equals ten, the angle, e a d, is a right angle. Because the square of six and that of eight, added together, equal the square of ten, thus: $6 \times 6 = 36$, and $8 \times 8 = 64$; 36 + 64 = 100, and $10 \times 10 =$ 100. Any sizes, taken in the same proportion, as six, eight and ten, will produce the same effect: as 3, 4 and 5, or 12, 16 and 20. (See note to Art. 103.)

By the process shown at Fig. 30, the end of a board may be squared without a carpenters'-square. All that is necessary is a pair of compasses and a ruler. Let c a be the edge of the board, and a the point at which it is required to be squared. Take the point, b, as near as possible at an angle of forty-five degrees, or on a mitre-line, from a, and at about the middle of the board. This is not necessary to the working of the problem, nor does it affect its accuracy, but the result is more easily obtained. Stretch the compasses from b to a, and then bring the leg at a around to d; draw a line from d, through b, out indefinitely; take the distance, d b, and place it from b to e; join e and a; then e a will be at right angles to c a. In squaring the foundation of a building, or laying-out a garden, a rod and chalk-line may be used instead of compasses and ruler.

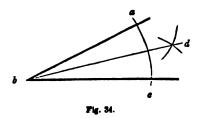
75.—To let fall a perpendicular near the end of a line. Let e, (Fig. 30,) be the point above the line, c a, from which the perpendicular is required to fall. From e, draw any line, as e d, obliquely to the line, c a; bisect e d at b; upon b, with the radius, b e, describe the arc, e a d; join e and a; then e a will be the perpendicular required.



76.—To make an angle, (as e d f, Fig. 33,) equal to a given angle, (as b a c.) From the angular point, a, with any radius, describe the arc, b c; and with the same radius, on the line, d e,

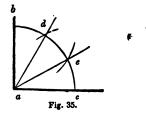
and from the point, d, describe the arc, fg; take the distance, bc, and upon g, describe the small arc at f; join f and d; and the angle, edf, will be equal to the angle, bac.

If the given line upon which the angle is to be made, is situated parallel to the similar line of the given angle, this may be performed more readily with the set-square. (See Art. 11.)



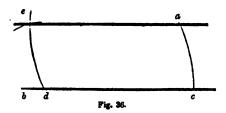
77.—To bisect an angle. Let $a \ b \ c$, (Fig. 34,) be the angle to be bisected. Upon b, with any radius, describe the arc, $a \ c$; upon a and c, with a radius greater than half $a \ c$, describe arcs cutting each other at d; join b and d; and $b \ d$ will bisect the angle, $a \ b \ c$, as was required.

This problem is frequently made use of in solving other problems; it should therefore be well impressed upon the memory.



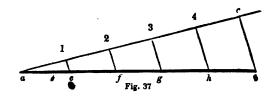
78.— To trisect a right angle. Upon a, (Fig. 35,) with any radius, describe the arc, bc; upon b and c, with the same radius, describe arcs cutting the arc, bc, at d and e; from d and e, draw lines to a, and they will trisect the angle as was required.

The truth of this is made evident by the following operation. Divide a circle into quadrants : also, take the radius in the dividers, and space off the circumference. This will divide the circumference into just six parts. A semi-circumference, therefore, is equal to three, and a quadrant to one and a half of those parts. The radius, therefore, is equal to $\frac{1}{2}$ of a quadrant; and this is equal to a right angle.



79.—Through a given point, to draw a line parallel to a given line. Let a, (Fig. 36,) be the given point, and b c the given line. Upon any point, as d, in the line, b c, with the radius, d a, describe the arc, a c; upon a, with the same radius, describe the arc, d e; make d e equal to a c; through e and a, draw the line, e a; which will be the line required.

This is upon the same principle as Art. 76.

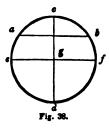


80.— To divide a given line into any number of equal parts. Let $a \ b$, (Fig. 37,) be the given line, and 5 the number of parts. Draw $a \ c$, at any angle to $a \ b$; on $a \ c$, from a, set off 5 equal parts of any length, as at 1, 2, 3, 4 and c; join c and b; through the points, 1, 2, 3 and 4, draw $1 \ e$, $2 \ f$, $3 \ g$ and $4 \ h$, parallel to $c \ b$; which will divide the line, $a \ b$, as was required.

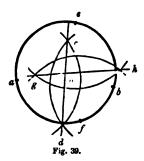
The lines, $a \ b$ and $a \ c$, are divided in the same proportion. (See Art. 109.)

THE CIRCLE.

81.—To find the centre of a circle. Draw any chord, as a b,

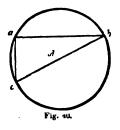


(Fig. 38,) and bisect it with the perpendicular, c d; bisect c d with the line, e f, as at g; then g is the centre as was required.



81, a.—A second method. Upon any two points in the circumference nearly opposite, as a and b, (Fig. 39,) describe arcs cutting each other at c and d; take any other g wo points, as e and f, and describe arcs intersecting as at g and h; join g and h, and c and d; the intersection, o, is the centre.

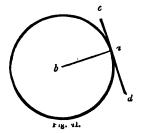
This is upon the same principle as Art. 85.



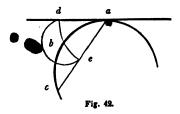
81, b.-A third method. Draw any chord, as a b, (Fig. 40,)

and from the point, a, draw a c, at right angles to a b; join c and b; bisect c b at d—which will be the centre of the circle.

If a circle be not too large for the purpose, its centre may very readily be ascertained by the help of a carpenters'-square, thus: app'y the corner of the square to any point in the circumference, as at a; by the edges of the square, (which the lines, a b and a c, represent,) draw lines cutting the circle, as at b and c; join b and c; then if b c is bisected, as at d, the point, d, will be the centre. (See Art. 156.)

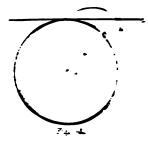


82.—At a given point in a circle, to draw a tangent thereto. Let a, (Fig. 41,) be the given point, and b the centre of the circle. Join a and b; through the point, a, and at right angles to a b, draw c d; c d is the tangent required.

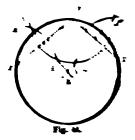


83.—The same, without making use of the centre of the circle. Let a, (Fig. 42,) be the given point. From a, set off any distance to b, and the same from b to c; join a and c; upon a, with a b for radius, describe the arc, d b e; make d b equal to b e; through a and d, draw a line; this will be the tangent required.

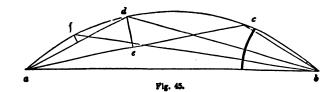
84.—A circle and a tangent given, to find the point of contact. From any point, as a, (Fig. 43,) in the tangent, b c, draw



a line to the sentre i baset (int s. 11000 a with the radius, c. describe the un, of i f is the point if rannet required. If f and i were based the line would form regit angles with the tangent 5 a. [See Arr. 136.



85.—Through any three points not in a straight line, to draw a circle. Let a, b and c. Fig. 11 by the three given points. Upon a and b, with any radius greater than half a b, describe arcs intersecting at d and e: upon b and c. with any radius greater than half b c, describe arcs intersecting at f and g; through d and e, draw a right line, also another through f and g; upon the intersection, h, with the radius, h a, describe the circle, a b c, and it will be the one required.

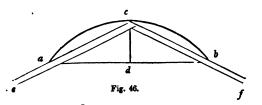


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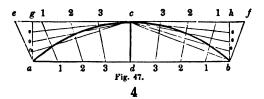
86.—Three points not in a straight line being given, to find a fourth that shall, with the three, lie in the circumference of a circle. Let $a \ b \ c$, (Fig. 45,) be the given points. Connect them with right lines, forming the triangle, $a \ c \ b$; bisect the angle, $c \ b \ a$, (Art. 77,) with the line, $b \ d$; also bisect $c \ a$ in e, and erect $e \ d$, perpendicular to $a \ c$, cutting $b \ d$ in d; then d is the fourth point required.

A fifth point may be found, as at f, by assuming a, d and b, as the three given points, and proceeding as before. So, also, any number of points may be found; simply by using any three already found. This problem will be serviceable in obtaining short pieces of very flat sweeps. (See Art. 311.)



87.—To descrip a segment of a circle by a set-triangle. Let a b, (Fig. 46,) be the chord, and c d the height of the segment. Secure two straight-edges, or rules in the position, c e and c f, by nailing them together at c, and affixing a brace from e to f; put in pins at a and b; move the angular point, c, in the direction, a c b; keeping the edges of the triangle hard against the pins, a and b; a pencil held at c will describe the arc, a c b.

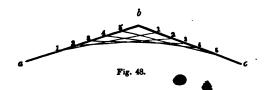
If the angle formed by the rulers at c be a right angle, the segment described will be a semi-circle. This problem is useful in describing centres for brick arches, when they are required to be rather flat. Also, for the head hanging-stile of a windowframe, where a brick arch, instead of a stone lintel, is to be placed over it.



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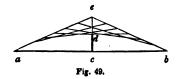
88.—To describe the segment of a circle by intersection of lines. Let a b, (Fig. 47,) be the chord, and c d the height of the segment. Through c, draw e f, parallel to a b; draw b f at right angles to c b; make c e equal to c f; draw a g and b h, at right angles to a b; divide c e, c f, d a, d b, a g and b h, each into a like number of equal parts, as four; draw the lines, 1 1, 2 2, &c., and from the points, o, o and o, draw lines to c; at the intersection of these lines, trace the curve, a c b, which will be the segment required.

In very large work, or in laying out ornamented gardens, &c., this will be found useful; and where the centre of the proposed arc of a circle is inaccessible, it will be invaluable. (To trace the curve, see note at Art. 117.)



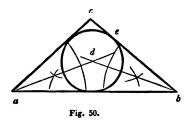
89.—In a given angle, to describe a tanged curve. Let a b c, (Fig. 48,) be the given angle, and 1 in the line, a b, and 5 in the line, b c, the mination of the curve. Divide 1 b and b 5 into a like number of equal parts, as at 1, 2, 3, 4 and 5; join 1 and 1, 2 and 2, 3 and 3, &c.; and a regular curve will be formed that will be tangical to the line, a b, at the point, 1, and to b c at 5.

This is of much use in stair-building, in easing the angles formed between the wall-string and base of the hall, also between the front string and level facia, and in many other instances. The curve is not circular, but of the form of the parabola, (*Fig.* 93;) yet in large angles the difference is not perceptible. This problem can be applied to describing segments of circles for door-

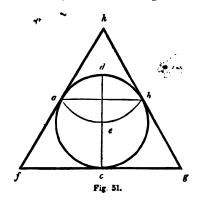


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heads, window-heads, &c., to rather better advantage than Art. 87. For instance, let a b, (Fig. 49,) be the width of the opening, and c d the height of the arc. Extend c d, and make d eequal to c d; join a and e, also e and b; and proceed as directed at Art. 89.



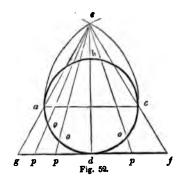
90.—To describe a circle within any given triangle, so that the sides of the triangle shall be tangical. Let a b c, (Fig. 50,) be the given triangle. Bisect the angles, a and b, according to Art. 77; upon d, the point of intersection of the bisecting lines, with the radius, d e, describe the required circle.



91.—About a given circle, to describe an equi-lateral triangle. Let $a \ d \ b \ c$, (Fig. 51,) be the given circle. Draw the diameter, $c \ d$; upon d, with the radius of the given circle, describe the arc, $a \ e \ b$; join a and b; draw $f \ g$, at right angles to $d \ c$; make $f \ c$ and $c \ g$, each equal to $a \ b$; from f, through a, draw $f \ h$, also from g, through b, draw $g \ h$; then $f \ g \ h$ will be the triangle required.

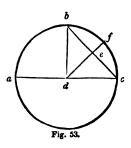






92.— To find a right line nearly equal to the circumference of a circle. Let a b c d, (Fig. 52,) be the given circle. Draw the diameter, a c; on this erect an equi-lateral triangle, a e c, according to Art. 96; draw g f, parallel to a c; extend e c to f, also e a to g; then g f will be nearly the length of the semicircle, a d c; and twice g f will nearly equal the circumference of the circle, a b c d, as was required.

Lines drawn from e, through any points in the circle, as o, o and o, to p, p and p, will divide g f in the same way as the semicircle, a d c, is divided. So, any portion of a circle may be transferred to a straight line. This is a very useful problem, and should be well studied; as it is frequently used to solve problems on stairs, domes, &c.



92, a.—Another method. Let $a \ b \ f \ c$, (Fig. 53,) be the given circle. Draw the diameter, $a \ c$; from d, the centre, and at right angles to $a \ c$, draw $d \ b$; join b and c; bisect $b \ c$ at e; from d, through e, draw $d \ f$; then $e \ f$ added to three times the diameter,

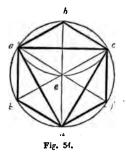


PRACTICAL GEOMETRY.

will equal the circumference of the circle within the $_{\sigma \sigma \sigma}$ part of its length.

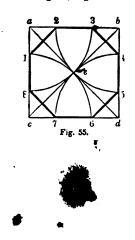
POLYGONS, &C.

93.—Within a given circle, to inscribe an equi-lateral triangle, hexagon or dodecagon. Let $a \ b \ c \ d$, (Fig. 54,) be the



given circle. Draw the diameter, b d; upon b, with the radius of the given circle, describe the arc, a e c; join a and c, also aand d, and c and d—and the triangle is completed. For the hexagon: from a, also from c, through e, draw the lines, a fand c g; join a and b, b and c, c and f, &c., and the hexagon is completed. The dodecagon may be formed by bisecting the sides of the hexagon.

Each side of a regular hexagon is exactly equal to the radius of the circle that circumscribes the figure. For the radius is equal to a chord of an arc of 60 degrees; and, as every circle is supposed to be divided into 360 degrees, there is just 6 times 60, or 6 arcs of 60 degrees, in the whole circumference. A line drawn from each angle of the hexagon to the centre, (as in the figure,) divides it into six equal, equi-lateral triangles.

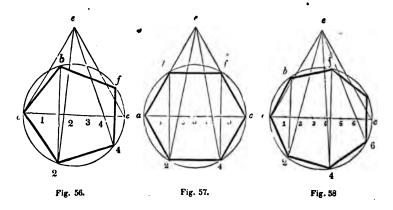


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94.— Within a square to inscribe an octagon. Let a b c d, (Fig. 55,) be the given square. Draw the diagonals, a d and b c; upon a, b, c and d, with a e for radius, describe arcs cutting the sides of the square at 1, 2, 3, 4, 5, 6, 7 and 8; join 1 and 2, 3 and 4, 5 and 6, &c., and the figure is completed.

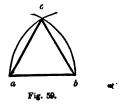
In order to eight-square a hand-rail, or any piece that is to be afterwards rounded, draw the diagonals, a d and b c, upon the end of it, after it has been squared-up. Set a gauge to the distance, a e, and run it upon the whole length of the stuff, from each corner both ways. This will show how much is to be chamfered off, in order to make the piece octagonal.



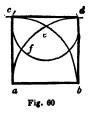
95.— Within a given circle to inscribe any regular polygon. Let a b c 2, (Fig. 56, 57 and 58,) be given circles. Draw the diameter, a c; upon this, erect an equi-lateral triangle, $a \ e \ c$, according to Art. 96; divide a c into as many equal parts as the polygon is to have sides, as at 1, 2, 3, 4, &c.; from e, through each even number, as 2, 4, 6, &c., draw lines cutting the circle in the points, 2, 4, &c.; from these points and at right angles to $a \ c$, draw lines to the opposite part of the circle; this will give the remaining points for the polygon, as b, f, &c.

In forming a hexagon, the sides of the triangle erected upon a c, (as at Fig. 57,) mark the points, b and f.

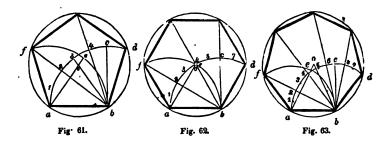
96.—Upon a given line to construct an equi-lateral triangle. Let a b, (Fig. 59,) be the given line. Upon a and b, with a b



for radius, describe arcs intersecting at c; join a and c, also c and b; then a c b will be the triangle required.



97.—To describe an equi-lateral rectangle, or square. Let $a \ b, (Fig. 60,)$ be the length of a side of the proposed square. Upon a and b, with $a \ b$ for radius, describe the arcs, $a \ d$ and $b \ c \ j$ bisect the arc, $a \ e, \ in \ f \ j$ upon e, with $e \ f$ for radius, describe the arc, $c \ f \ d \ j$ join a and c, c and d, d and $b \ j$ then $a \ c \ d \ b$ will be the square required.

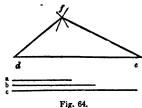


98.— Upon a given line to describe any regular polygon. Let a b, (Fig. 61, 62 and 63,) be given lines, equal to a side of the required figure. From b, draw b c, at right angles to a b; upon a and b, with a b for radius, describe the arcs, a c d and

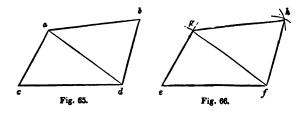
AMERICAN HOUSE-CARPENTER.

f e b; divide a c into as many equal parts as the polygon is to have sides, and extend those divisions from c towards d; from the second point of division counting from c towards a, as 3, (Fig. 61,) 4, (Fig. 62,) and 5, (Fig. 63,) draw a line to b; take the distance from said point of division to a, and set it from bto e; join e and a; upon the intersection, o, with the radius, o a, describe the circle, a f d b; then radiating lines, drawn from b through the even numbers on the arc, a d, will cut the circle at the several angles of the required figure.

In the hexagon, (Fig. 62,) the divisions on the arc, a d, are not necessary; for the point, o, is at the intersection of the arcs, a d and f b, the points, f and d, are determined by the intersection of those arcs with the circle, and the points above, g and h, can be found by drawing lines from a and b, through the centre, o. In polygons of a greater number of sides than the hexagon, the intersection, o, comes above the arcs; in such case, therefore, the lines, a e and b 5, (Fig. 63,) have to be extended before they will intersect.



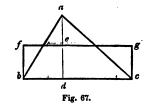
99.— To construct a triangle whose sides shall be severally equal to three given lines. Let a, b and c, (Fig. 64) be the given lines. Draw the line, d e, and make it equal to c; upon e, with b for radius, describe an arc at f; upon d, with a for radius, describe an arc intersecting the other at f; join d and f, also f and e; then d f e will be the triangle required.



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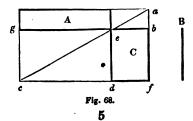
100.—To construct a figure equal to a given, right-lined figure. Let $a \ b \ c \ d$, (Fig. 65,) be the given figure. Make $e \ f$, (Fig. 66,) equal to $c \ d$; upon f, with $d \ a$ for radius, describe an arc at g; upon e, with $c \ a$ for radius, describe an arc intersecting the other at g; join g and e; upon f and g, with $d \ b$ and $a \ b$ for radius, describe arcs intersecting at h; join g and h, also hand f; then Fig. 66 will every way equal Fig. 65.

So, right-lined figures of any number of sides may be copied, oy first dividing them into triangles, and then proceeding as above. 'The shape of the floor of any room, or of any piece of land, &c., may be accurately laid out by this problem, at a scale upon paper; and the contents in square feet be ascertained by the next.



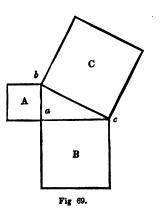
101.—To make a parallelogram equal to a given triangle. Let $a \ b \ c$, (Fig. 67,) be the given triangle. From a, draw $a \ d$, at right angles to $b \ c$; bisect $a \ d$ in e; through e, draw $f \ g$, parallel to $b \ c$; from b and c, draw $b \ f$ and $c \ g$, parallel to $d \ e$; then $b \ f \ g \ c$ will be a parallelogram containing a surface exactly equal to that of the triangle, $a \ b \ c$.

Unless the parallelogram is required to be a rectangle, the lines, b f and c g, need not be drawn parallel to d e. If a rhomboid is desired, they may be drawn at an oblique angle, provided they be parallel to one another. To ascertain the area of a triangle, multiply the base, b c, by half the perpendicular height, d a. In doing this, it matters not which side is taken for base.

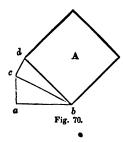


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102.—A parallelogram being given, to construct another equal to it, and having a side equal to a given line. Let A, (Fig. 68,) be the given parallelogram, and B the given line. Produce the sides of the parallelogram, as at a, b, c and d; make e d equal to B; through d, draw c f, parallel to g b; through e, draw the diagonal, c a; from a, draw a f, parallel to e d; then C will be equal to A. (See Art. 144.)



103.— To make a square equal to two or more given squares. Let A and B, (Fig. 69,) be two given squares. Place them so as to form a right angle, as at a; join b and c; then the square, C, formed upon the line, b c, will be equal in extent to the squares, A and B, added together. Again : if a b, (Fig. 70,) be equal to



the side of a given square, c a, placed at right angles to a b, be the side of another given square, and c d, placed at right angles to

c b, be the side of a third given square; then the square, A, formed upon the line, d b, will be equal to the three given squares. (See Art. 157.)

The usefulness and importance of this problem are proverbial. To ascertain the length of braces and of rafters in framing, the length of stair-strings, &c., are some of the purposes to which it may be applied in carpentry. (See note to Art. 74, b.) If the length of any two sides of a right-angled triangle is known, that of the third can be ascertained. Because the square of the hypothenuse is equal to the united squares of the two sides that contain the right angle.

(1.)—The two sides containing the right angle being known, to find the hypothenuse. *Rule.*—Square each given side, add the squares together, and from the product extract the squareroot: this will be the answer. For instance, suppose it were required to find the length of a rafter for a house, 34 feet wide, the ridge of the roof to be 9 feet high, above the level of the wall-plates. Then 17 feet, half of the span, is one, and 9 feet, the height, is the other of the sides that contain the right angle. Proceed as directed by the rule:

17	9
17	9
119	81 = square of 9.
17	289 = square of 17.
$\frac{1}{289} - \text{square of } 17.$	370 Product.
1 1 near	-root of 370; equal 19 feet, $2\frac{7}{8}$ in. ly: which would be the required th of the rafter.
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(By reference to the table of square-roots in the appendix, the root of almost any number may be found ready calculated.)

Again: suppose it be required, in a frame building, to find the length of a brace, having a run of three feet each way from the point of the right angle. The length of the sides containing the right angle will be each 3 feet: then, as before—

3

9 =square of one side.

3 times 3 = 9 = square of the other side.

18 Product : the square-root of which is 4.2426 + ft, or 4 feet, 2 inches and $\frac{7}{6}$ ths. full.

(2.)—The hypothenuse and one side being known, to find the other side. Rule.—Subtract the square of the given side from the square of the hypothenuse, and the square-root of the product will be the answer. Suppose it were required to ascertain the greatest perpendicular height a roof of a given span may have, when pieces of timber of a given length are to be used as rafters. Let the span be 20 feet, and the rafters of 3×4 hemlock joist. These come about 13 feet long. The known hypothenuse, then, is 13 feet, and the known side, 10 feet—that being half the span of the building.

13 13
39 13

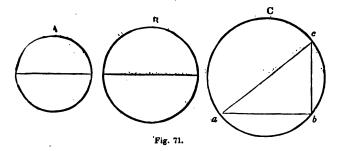
169 = square of hypothenuse. 10 times 10 = 100 = square of the given side.

69 Product: the square-root of which is 8 :3066 + feet, or 8 feet, 3 inches and the full. This will be the greatest perpendicular height, as required. Again: suppose that in a story of 8 feet, from floor to floor, a step-ladder is required, the strings of which are to be of plank, 12 feet long; and it is desirable to know the greatest run such a length of string will afford. In this case, the two given sides are—hypothenuse 12, perpendicular 8 feet.

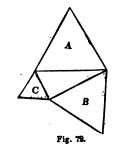
12 times 12 - 144 = square of hypothenuse. 8 times 8 = 64 = square of perpendicular.

80 Product : the square-root of which is 8.9442 + feet, or 8 feet, 11 inches and $\frac{1}{5}$ ths.—the answer, as required.

Many other cases might be adduced to show the utility of this problem. A practical and ready method of ascertaining the length of braces, rafters, &cc., when not of a great length, is to apply a rule across the carpenters'-square. Suppose, for the length of a rafter, the base be 12 feet and the height 7. Apply the rule diagonally on the square, so that it touches 12 inches from the corner on one side, and 7 inches from the corner on the other. The number of inches on the rule, which are intercepted by the sides of the square, $13\frac{2}{5}$ nearly, will be the length of the rafter in feet; viz, 13 feet and 4ths of a foot. If the dimensions are large, as 30 feet and 20, take the half of each on the sides of the square, viz, 15 and 10 inches; then the length in inches across, will be one-half the number of feet the rafter is long. This method is just as accurate as the preceding; but when the length of a very long rafter is sought, it requires great care and precision to ascertain the fractions. For the least variation on the square, or in the length taken on the rule, would make perhaps several inches difference in the length of the rafter. For shorter dimensions, however, the result will be true enough.



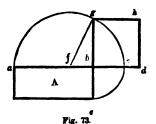
104.—To make a circle equal to two given circles. Let A and B, (Fig. 71,) be the given circles. In the right-angled triangle, $a \ b \ c$, make $a \ b$ equal to the diameter of the circle, B, and $c \ b$ equal to the diameter of the circle, A; then the hypothenuse,



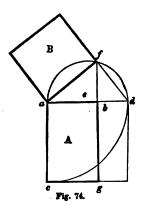
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a c, will be the diameter of a circle, C, which will be equal in area to the two circles, A and B, added together.

Any polygonal figure, as A, (Fig. 72,) formed on the hypothenuse of a right-angled triangle, will be equal to two similar figures,* as B and C, formed on the two legs of the triangle.



105.—To construct a square equal to a given rectangle. Let A, (Fig. 73,) be the given rectangle. Extend the side, a b, and make b c equal to b e; bisect a c in f, and upon f, with the radius, f a, describe the semi-circle, a g c; extend e b, till it cuts the curve in g; then a square, b g h d, formed on the line, b g, will be equal in area to the rectangle, A.

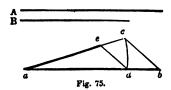


105, a.—Another method. Let A, (Fig. 74,) be the given rectangle. Extend the side, a b, and make a d equal to a c;

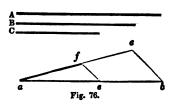
^{*} Similar figures are such as have their several angles respectively equal, and their sides respectively proportionate.

bisect $a \ d$ in e; upon e, with the radius, $e \ a$, describe the semicircle, $a \ f \ d$; extend $g \ b$ till it cuts the curve in f; join a and f; then the square, B, formed on the line, $a \ f$, will be equal in area to the rectangle, A. (See Art. 156 and 157.)

106.—To form a square equal to a given triangle. Let a b, (Fig. 73,) equal the base of the given triangle, and b e equal half its perpendicular height, (see Fig. 67;) then proceed as directed at Art. 105.

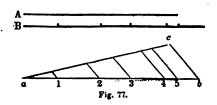


107.—Two right lines being given, to find a third proportional thereto. Let A and B, (Fig. 75,) be the given lines. Make a b equal to A; from a, draw a c, at any angle with a b; make a c and a d each equal to B; join c and b; from d, draw d e, parallel to c b; then a e will be the third proportional required. That is, a e bears the same proportion to B, as B does to A.



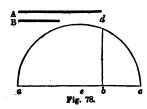
108.—Three right lines being given, to find a fourth proportional thereto. Let A, B and C, (Fig. 76,) be the given lines. Make a b equal to A; from a, draw a c, at any angle with a b; make a c equal to B, and a e equal to C; join c and b; from e, draw e f, parallel to c b; then a f will be the fourth proportional required. That is, a f bears the same proportion to C, as B does to A.

To apply this problem, suppose the two axes of a given ellipsis, and the longer axis of a proposed ellipsis are given. Then, by this problem, the length of the shorter axis to the proposed ellipsis, can be found; so that it will bear the same proportion to the longer axis, as the shorter of the given ellipsis does to its longer. (See also, Art. 126.)



109.—A line with certain divisions being given, to divide another, longer or shorter, given line in the same proportion. Let A, (Fig. 77,) be the line to be divided, and B the line with its divisions. Make a b equal to B, with all its divisions, as at 1, 2, 3, &c.; from a, draw a c, at any angle with a b; make a cequal to A; join c and b; from the points, 1, 2, 3, &c., draw lines, parallel to c b; then these will divide the line, a c, in the same proportion as B is divided—as was required.

This problem will be found useful in proportioning the members of a proposed cornice, in the same proportion as those of a given cornice of another size. (See Art. 243 and 244.) So of a pilaster, architrave, &c.

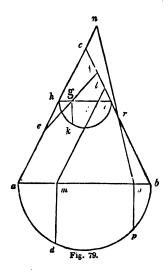


110.—Between two given right lines, to find a mean proportional. Let A and B, (Fig. 78,) be the given lines. On the line, a c, make a b equal to A, and b c equal to B; bisect ac in e; upon e, with e a for radius, describe the semi-circle, a d c; at b, erect b d, at right angles to a c; then b d will be the mean proportional between A and B.

For an application of this problem, see Art. 105.

CONIC SECTIONS.

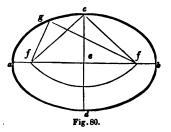
111.—If a cone, standing upon a base that is at right angles with its axis, be cut by a plane, perpendicular to its base and passing through its axis, the section will be an isoceles triangle; (as $a \ b \ c, \ Fig. \ 79$;) and the base will be a semi-circle. If a



cone be cut by a plane in the direction, ef, the section will be an *ellipsis*; if in the direction, ml, the section will be a *parabola*; and if in the direction, ro, an *hyperbola*. (See Art. 56 to 60.) If the cutting planes be at right angles with the plane, a b c, then—

112.—To find the axes of the ellipsis, bisect e f, (Fig. 79,) in g; through g, draw h i, parallel to a b; bisect h i in j; upon j, with j h for radius, describe the semi-circle, h k i; from g, draw g k, at right angles to h i; then twice g k will be the conjugate axis, and e f the transverse. 113.—To find the axis and base of the parabola. Let ml, (Fig. 79,) parallel to a c, be the direction of the cutting plane. From m, draw m d, at right angles to a b; then l m will be the axis and height, and m d an ordinate and half the base; as at Fig. 92, 93.

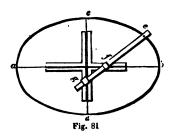
114.—To find the height, base and transverse axis of an hyperbola. Let o r, (Fig. 79,) be the direction of the cutting plane. Extend o r and a c till they meet at n; from o, draw o p, at right angles to a b; then r o will be the height, n r the transverse axis, and o p half the base; as at Fig. 94.



115.—The axes being given, to find the foci, and to describe an ellipsis with a string. Let a b, (Fig. 80,) and c d, be the given axes. Upon c, with a e or b e for radius, describe the arc, f f; then f and f, the points at which the arc cuts the transverse axis, will be the foci. At f and f place two pins, and another at c; tie a string about the three pins, so as to form the triangle, f f c; remove the pin from c, and place a pencil in its stead; keeping the string taut, move the pencil in the direction, cg a; it will then describe the required ellipsis. The lines, fg and g f, show the position of the string when the pencil arrives at g.

This method, when performed correctly, is perfectly accurate; but the string is liable to stretch, and is, therefore, not so good to use as the trammel. In making an ellipse by a string or twine, that kind should be used which has the least tendency to elasticity. For this reason, a cotton cord, such as chalk-lines are commonly made of, is not proper for the purpose: a linen, or flaxen cord is much better.

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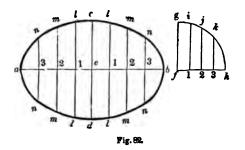


116.—The axes being given, to describe an ellipsis with a trammel. Let a b and c d, (Fig. 81,) be the given axes. Place the trammel so that a line passing through the centre of the grooves, would coincide with the axes; make the distance from the pencil, e, to the nut, f, equal to half c d; also, from the pencil, e, to the nut, g, equal to half a b; letting the pins under the nuts slide in the grooves, move the trammel, e g, in the direction, c b d; then the pencil at e will describe the required ellipse.

A trammel may be constructed thus: take two straight strips of board, and make a groove on their face, in the centre of their width; join them together, in the middle of their length, at right angles to one another; as is seen at Fig. 81. A rod is then to be prepared, having two moveable nuts made of wood, with a mortice through them of the size of the rod, and pins under them large enough to fill the grooves. Make a hole at one end of the rod, in which to place a pencil. In the absence of a regular trammel, a temporary one may be made, which, for any short job, will answer every purpose. Fasten two straight-edges at right angles to one another. Lay them so as to coincide with the axes of the proposed ellipse, having the angular point at the centre. Then, in a rod having a hole for the pencil at one end, place two brad-awls at the distances described at Art. 116. While the pencil is moved in the direction of the curve, keep the brad-awls hard against the straight-edges, as directed for using the trammel-rod, and one-quarter of the ellipse will be drawn. Then, by shifting the straight-edges, the other three quarters in succession may be drawn. If the required ellipse be not too large, a carpenters'-square may be made use of, in place of the straightedges.

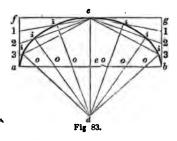
An improved method of constructing the trammel, is as follows: make the sides of the grooves bevilling from the face of the stuff, or dove-tailing instead of square. Prepare two slips of wood, each about two inches long, which shall be of a shape to just fill the groove when slipped in at the end. 'These, instead of

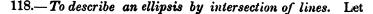
pins, are to be attached one to each of the moveable nuts with a screw, loose enough for the nut to move freely about the screw as an axis. The advantage of this contrivance is, in preventing the nuts from slipping out of their places, during the operation of describing the curve.



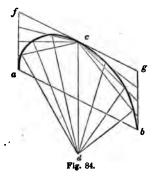
117.—To describe an ellipsis by ordinates. Let $a \ b$ and $c \ d$, (Fig. 82,) be given axes. With $a \ e$ or $e \ b$ for radius, describe the quadrant, $f \ g \ h$; divide $f \ h$, $a \ e$ and $e \ b$, each into a like number of equal parts, as at 1, 2 and 3; through these points, draw ordinates, parallel to $c \ d$ and $f \ g$; take the distance, $1 \ i$, and place it at $1 \ l$, transfer $2 \ j$ to $2 \ m$, and $3 \ k$ to $3 \ n$; through the points, a, n, m, l and c, trace a curve, and the ellipsis will be completed.

The greater the number of divisions on a e, &c., in this and the following problem, the more points in the curve can be found, and the more accurate the curve can be traced. If pins are placed in the points, n, m, l, &c., and a thin slip of wood bent around by them, the curve can be made quite correct. This method is mostly used in tracing face-moulds for stair handrailing.

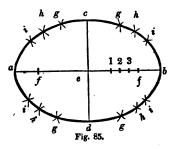




a b and c d; (Fig. 83,) be given axes. Through c, draw fg, parallel to a b; from a and b; draw a f and b g, at right angles to a b; divide f a, g b, a e and e b, each into a like number of equal parts, as at 1, 2, 3 and o, o, o; from 1, 2 and 3, draw lines to c; through o, o and o, draw lines from d, intersecting those drawn to c; then a curve, traced through the points, i, i, i, will be that of an ellipsis.



Where neither trammel nor string is at hand, this, perhaps, is the most ready method of drawing an ellipsis. The divisions should be small, where accuracy is desirable. By this method, an ellipsis may be traced without the axes, provided that a diameter and its conjugate be given. Thus, $a \ b$ and $c \ d$, (Fig. 84,) are conjugate diameters: $f \ g$ is drawn parallel to $a \ b$, instead of being at right angles to $c \ d$; also, $f \ a$ and $g \ b$ are drawn parallel to $c \ d$, instead of being at right angles to $a \ b$.

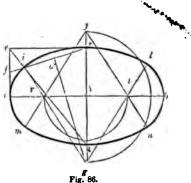


119.—To describe an ellipsis by intersecting arcs. Let a b

AMERICAN HOUSE-CARPENTER.

and c d, (Fig. 85,) be given axes. Between one of the foci, fand f, and the centre, e, mark any number of points, at random, as 1, 2 and 3; upon f and f, with b 1 for radius, describe arcs at g, g, g and g; upon f and f, with a 1 for radius, describe arcs intersecting the others at g, g, g and g; then these points of intersection will be in the curve of the ellipsis. The other points, h and i, are found in like manner, viz: h is found by taking b 2 for one radius, and a 2 for the other; i is found by taking b 3 for one radius, and a 3 for the other, always using the foci for centres. Then by tracing a curve through the points, c, g, h, i, b, &c., the ellipse will be completed.

This problem is founded upon the same principle as that of the string. This is obvious, when we reflect that the length of the string is equal to the transverse axis, added to the distance between the foci. See Fig. 80; in which c f equals a e, the half of the transverse axis.

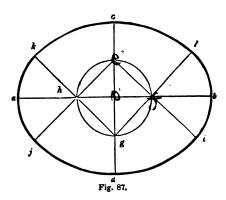


120.—To describe a figure nearly in the shape of an ellipsis, by a pair of compasses. Let a b and c d, (Fig. 86,) be given axes. From c, draw c e, parallel to a b; from a, draw a e, parallel to c d; join e and d; bisect e a in f; join f and c, intersecting e d in i; bisect i c in o; from o, draw og, at right angles, to i c, meeting c d extended to g; join i and g, cutting the transverse axis in r; make h j equal to h g, and h k equal to h r; from j, through r and k, draw j m and j n; also, from g, through k, draw g l; upon g and j, with g c for radius, describe the

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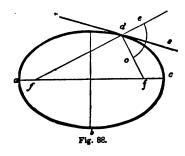
arcs, $i \ l$ and $m \ n$; upon r and k, with $r \ a$ for radius, describe the arcs, $m \ i$ and $l \ n$; this will complete the figure.

When the axes are proportioned to one another as 2 to 3, the extremities, c and d, of the shortest axis, will be the centres for describing the arcs, i l and m n; and the intersection of e d with the transverse axis, will be the centre for describing the arc, m i, &c. As the elliptic curve is continually changing its course from that of a circle, a true ellipsis cannot be described with a pair of compasses. The above, therefore, is only an approximation.

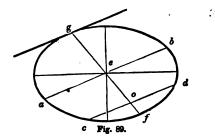


121.— To draw an oval in the proportion, seven by nine. Let cd, (Fig. 87,) be the given conjugate axis. Bisect cd in o, and through o, draw ab, at right angles to cd; bisect co in e; upon o, with oe for radius, describe the circle, efgh; from e, through h and f, draw ej and ei; also, from g, through h and f, draw gk and gl; upon g, with gc for radius, describe the arc, kl; upon e, with ed for radius, describe the arc, ji; upon h and f, with hk for radius, describe the arcs, jk and li; this will complete the figure.

This is a very near approximation to an ellipsis; and perhaps no **mathod** can be found, by which a well-shaped oval can be drawn with greater facility. By a little variation in the process, ovals of different proportions may be obtained. If quarter of the transverse axis is taken for the radius of the circle, e f g h, one will be drawn in the proportion, five by seven.



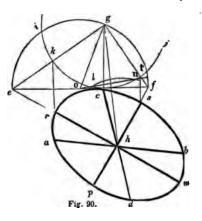
122.—To draw a tangent to an ellipsis. Let a b c d, (Fig. 88,) be the given ellipsis, and d the point of contact. Find the foci, (Art. 115,) f and f, and from them, through d, draw f e and f d; bisect the angle, (Art. 77,) e d o, with the line, s r; then s r will be the tangent required.



123.—An ellipsis with a tangent given, to detect the point of contact. Let ag b f, (Fig. 89,) be the given ellipsist and tangent. Through the centre, e, draw a b, parallel to the tangent; any where between e and f, draw c d, parallel to a b; bisect c d in o; through o and e, draw f g; then g will be the point of contact required.

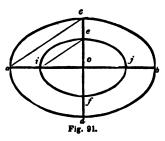
124.—A diameter of an ellipsis given, to find its conjugate. Let a b, (Fig. 89,) be the given diameter. Find the line, fg, by the last problem; then fg will be the diameter required.

PRACTICAL GEOMETRY.

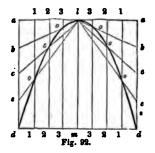


125.—Any diameter and its conjugate being given, to ascertain the two axes, and thence to describe the ellipsis. Let a b and c d, (Fig. 90,) be the given diameters, conjugate to one another. Through c, draw ef, parallel to a b; from c, draw c g, at right angles to ef; make c g equal to a h or h b; join g and h; upon g, with g c for radius, describe the arc, $i \ k \ c \ j$; upon h, with the same radius, describe the arc, ln; through the intersections, l and n, draw n o, cutting the tangent, ef, join e and g, also g and f, cutting the arc, $i \ c \ j$, in k and t; from e, through h, draw em, also from f, through h, draw fp; from k and t, draw kr and t s, parallel to g h, cutting em in r, and fp in s; make h m equal to h r, and h p equal to h s; then r m and s p will be the axes required, by which the ellipsis may be drawn in the usual way.

126.—To describe an ellipsis, whose axes shall be proportionate to the axes of a larger or smaller given one. Let a cbd, (Fig. 91,) be the given ellipsis and axes, and ij the transverse axis of a proposed smaller one. Join a and c; from i, lraw ie, parallel to ac; make of equal to oe; then ef will be

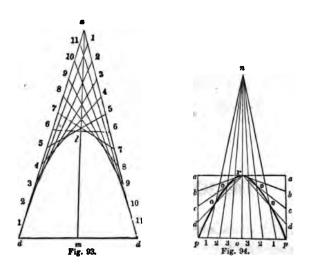


the conjugate axis required, and will bear the same proportion to ij, as cd does to ab. (See Art. 108.)



127.—To describe a parabola by intersection of lines. Let m l, (Fig. 92,) be the axis and height, (see Fig. 79,) and d d, a double ordinate and base of the proposed parabola. Through l, draw a a, parallel to d d; through d and d, draw d a and d a, parallel to m l; divide a d and d m, each into a like number of equal parts; from each point of division in d m, draw the lines, 1 1, 22, &c., parallel to m l; from each point of division in d a, draw lines to l; then a curve traced through the points of intersection, o, o and o, will be that of a parabola.

127, a.—Another method. Let m l, (Fig. 93,) be the axis and height, and d d the base. Extend m l, and make l a equal to m l; join a and d, and a and d; divide a d and a d, each into a like number of equal parts, as at 1, 2, 3, &c.; join 1 and 1, 2 and 2, &c., and the parabola will be completed.

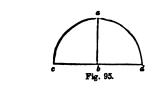


128.—To describe an hyperbola by intersection of lines. Let r o, (Fig. 94,) be the height, p p the base, and n r the transverse axis. (See Fig. 79.) Through r, draw a a, parallel to p p; from p, draw a p, parallel to r o; divide a p and p o, each into a like number of equal parts; from each of the points of divisions in the base, draw lines to n; from each of the points of division in a p, draw lines to r; then a curve traced through the points of intersection, o, o, &c., will be that of an hyperbola.

The parabola and hyperbola afford handsome curves for various mouldings.

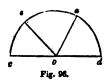
DEMONSTRATIONS.

129.—To impress more deeply upon the mind of the learner some of the more important of the preceding problems, and to indulge a very common and praiseworthy curiosity to discover the cause of things, are some of the reasons why the following exercises are introduced. In all reasoning, definitions are necessary; in order to insure, in the minds of the proponent and respondent, identity of ideas. A corollary is an inference deduced from a previous course of reasoning. An axiom is a proposition evident at first sight. In the following demonstrations, there are many axioms taken for granted; (such as, things equal to the same thing are equal to one another, &cc.;) these it was thought not necessary to introduce in form.



130.—Definition. If a straight line, as $a \ b$, (Fig. 95,) stand inpon another straight line, as $c \ d$, so that the two angles made at the point, b, are equal—a b c to a b d, (see note to Art. 27,) then each of the two angles is called a right angle.

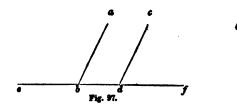
131.—Definition. The circumference of every circle is supposed to be divided into 360 equal parts, called *degrees*; hence a semi-circle contains 180 degrees, a quadrant 90, &c.



132.—Definition. The measure of an angle is the number of degrees contained between its two sides, using the angular point as a centre upon which to describe the arc. Thus the arc, c e, (Fig. 96,) is the measure of the angle, c b e ; e a, of the angle, e b e ; and a d, of the angle, a b d.

133.—Corollary. As the two angles at b, (Fig. 95,) are right angles, and as the semi-circle, $c \ a \ d$, contains 180 degrees, (Art. 131,) the measure of two right angles, therefore, is 180 degrees; of one right angle, 90 degrees; of half a right angle, 45; of one-third of a right angle, 30, &c.

134.—Definition. In measuring an angle, (Art. 132,) no regard is to be had to the length of its sides, but only to the degree of their inclination. Hence equal angles are such as have the same degree of inclination, without regard to the length of their sides.



135.—Axiom. If two straight lines, parallel to one another,

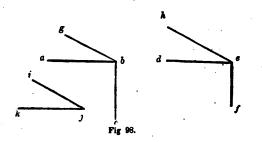
as a b and c d, (Fig. 97,) stand upon another straight line, as e f, the angles, a b f and c d f, are equal; and the angle, a b e, is equal to the angle, c d e.

136.—Definition. If a straight line, as $a \ b$, (Fig. 96,) stand obliquely upon another straight line, as $c \ d$, then one of the angles, as $a \ b \ c$, is called an obtuse angle, and the other, as $a \ b \ d$, an acute angle.

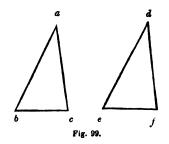
137.—Axiom. The two angles, $a \ b \ d$ and $a \ b \ c$, (Fig. 96,) are together equal to two right angles, (Art. 130, 133;) also, the three angles, $a \ b \ d$, $e \ b \ a$ and $c \ b \ e$, are together equal to two right angles.

138.—Corollary. Hence all the angles that can be made upon one side of a line, meeting in a point in that line, are together equal to two right angles.

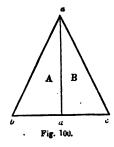
139.—Corollary. Hence all the angles that can be made on both sides of a line, at a point in that line, or all the angles that can be made about a point, are together equal to four right angles.



140.—Proposition. If to each of two equal angles a third angle be edded, their sums will be equal. Let $a \ b \ c$ and $d \ e \ f$, (Fig. 98,) be equal angles, and the angle, $i \ j \ k$, the one to be added. Make the angles, $g \ b \ a$ and $h \ e \ d$, each equal to the given angle, $i \ j \ k$; then the angle, $g \ b \ c$, will be equal to the angle, $h \ e \ f$; for, if $a \ b \ c$ and $d \ e \ f$ be angles of 90 degrees, and $i \ j \ k$, 30, then the angles, $g \ b \ c$ and $h \ e \ f$, will be each equal to 90 and 30 added, viz: 120 degrees.

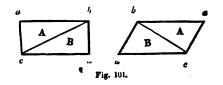


141.—Proposition. Triangles that have two of their sides and the angle contained between them respectively equal, have also their third sides and the two remaining angles equal; and consequently one triangle will every way equal the other. Let ab c, (Fig. 99,) and d e f be two given triangles, having the angle at a equal to the angle at d, the side, a b, equal to the side, d e, and the side, a c, equal to the side, d f; then the third side of one, b c, is equal to the third side of the other, e f; the angle at bis equal to the angle at e, and the angle at c is equal to the angle at f. For, if one triangle be applied to the other, the three points, b, a, c, coinciding with the three points, e, d, f, the line, b c, must coincide with the line, e f; the angle at b with the angle at e; the angle at c with the angle at f.

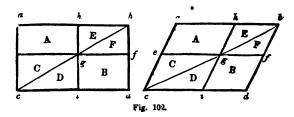


142.—Proposition. The two angles at the base of an isoceles triangle are equal. Let a b c, (Fig. 100,) be an isoceles triangle, of which the sides, a b and a c, are equal. Bisect the angle, (Art.

77,) b a c, by the line, a d. Then the line, b a, being equal to the line, a c; the line, a d, of the triangle, A, being equal to the line, a d, of the triangle, B, being common to each; the angle, b a d, being equal to the angle, d a c; the line, b d, must, according to Art. 141, be equal to the line, d c; and the angle at b must be equal to the angle at c.



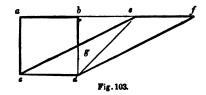
143.—Proposition. A diagonal crossing a parallelogram divides it into two equal triangles. Let $a \ b \ c \ d$, (Fig. 101,) be a given parallelogram, and $b \ c$, a line crossing it diagonally. Then, as $a \ c$ is equal to $b \ d$, and $a \ b$ to $c \ d$, the angle at a to the angle at d, the triangle, A, must, according to Art. 141, be equal to the triangle, B.



144.—Proposition. Let $a \ b \ c \ d$, (Fig. 102,) be a given parallelogram, and $b \ c$ a diagonal. At any distance between $a \ b$ and $c \ d$, draw $e \ f$, parallel to $a \ b$; through the point, g, the intersection of the lines, $b \ c$ and $e \ f$, draw $h \ i$, parallel to $b \ d$. In every parallelogram thus divided, the parallelogram, A, is equal to the parallelogram, B. According to Art. 143, the triangle, $a \ b \ c$, is equal to the triangle, $b \ c \ d$; the triangle, C, to the triangle, D; and E to F; this being the case, take D and F from the triangle, $b \ c \ d$, and C and E from the triangle, $a \ b \ c$, and what remains

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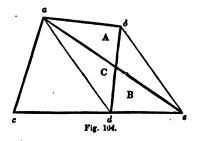
in one must be equal to what remains in the other; therefore, the **parallelogram**, A, is equal to the parallelogram, B.



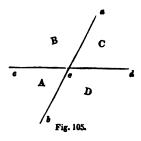
145.—Proposition. Parallelograms standing upon the same base and between the same parallels, are equal. Let $a \ b \ c \ d$ and $e \ f \ c \ d$, (Fig. 103,) be given parallelograms, standing upon the same base, $c \ d$, and between the same parallels, $a \ f$ and $c \ d$. Then, $a \ b$ and $e \ f$ being equal to $c \ d$, are equal to one another; $b \ e$ being added to both $a \ b$ and $e \ f$, $a \ e$ equals $b \ f$; the line, $a \ c$, being equal to $b \ d$, and $a \ e \ to \ b \ f$, and the angle, $c \ a \ e$, being equal, (Art. 135,) to the angle, $d \ b \ f$, the triangle, $a \ e \ c$, must be equal, (Art. 141,) to the triangle, $b \ f \ d$; these two triangles being equal, take the same amount, the triangle, $b \ e \ g$, from each, and what remains in one, $a \ b \ g \ c$, must be equal to what remains in the other, $e \ f \ d \ g$; these two quadrangles being equal, add the same amount, the triangle, $c \ g \ d$, to each, and they must still be equal; therefore, the parallelogram, $a \ b \ c \ d$, is equal to the parallelogram, $e \ f \ c \ d$.

146.—Corollary. Hence, if a parallelogram and triangle stand upon the same base and between the same parallels, the parallelogram will be equal to double the triangle. Thus, the parallelogram, a d, (Fig. 103,) is double, (Art. 143,) the triangle, c e d.

147.—Proposition. Let $a \ b \ c \ d$, (Fig. 104,) be a given quadrangle with the diagonal, $a \ d$. From b, draw $b \ e$, parallel to $a \ d$; extend $c \ d$ to $e \ ;$ join a and $e \ ;$ then the triangle, $a \ e \ c$, will be equal in area to the quadrangle, $a \ b \ c \ d$. Since the triangles, $a \ d \ b$ and $a \ d \ e$, stand upon the same base, $a \ d$, and between the same paral-

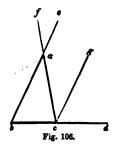


lels, a d and b e, they are therefore equal, (Art. 145, 146;) and since the triangle, C, is common to both, the remaining triangles, A and B, are therefore equal; then B being equal to A, the triangle, a e c, is equal to the quadrangle, a b c d.



148.—Proposition. If two straight lines cut each other, as a b and c d, (Fig. 105,) the vertical, or opposite angles, A and C, are equal. Thus, a e, standing upon c d, forms the angles, B and C, which together amount, (Art. 137,) to two right angles; in the same manner, the angles, A and B, form two right angles; since the angles, A and B, are equal to B and C, take the same amount, the angle, B, from each pair, and what remains of one pair is equal to what remains of the other; therefore, the angle, A, is equal to the angle, C. The same can be proved of the opposite angles, B and D.

149.—*Proposition.* The three angles of any triangle are equal to two right angles. Let a b c, (*Fig.* 106,) be a given triangle, with its sides extended to f, e, and d, and the line, c g,



drawn parallel to b e. As g c is parallel to e b, the angle, g c d, is, equal, (Art. 135,) to the angle, e b d; as the lines, f c and b e, cut one another at a, the opposite angles, f a e and b a c, are equal, (Art. 148;) as the angle, f a e, is equal, (Art. 135,) to the angle, a c g, the angle, a c g, is equal to the angle, b a c; therefore, the three angles meeting at c, are equal to the three angles of the triangle, a b c; and since the three angles at c are equal, (Art. 137,) to two right angles, the three angles of the triangle, a b c; must likewise be equal to two right angles. Any triangle can be subjected to the same proof.

150.—Corollary. Hence, if one angle of a triangle be a right angle, the other two angles amount to just one right angle.

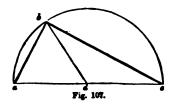
• 151.—Corollary. If one angle of a triangle be a right angle, and the two remaining angles are equal to one another, these are each equal to half a right angle.

152.—Corollary. If any two angles of a triangle amount to a right angle, the remaining angle is a right angle.

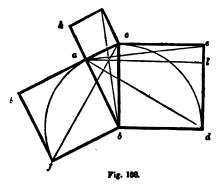
153.—Corollary. If any two angles of a triangle are together equal to the remaining angle, that remaining angle is a right angle.

154.—Corollary. If any two angles of a triangle are each equal to two-thirds of a right angle, the remaining angle is also equal to two-thirds of a right angle.

155.—Corollary. Hence, the angles of an equi-lateral triangle, are each equal to two-thirds of a right angle.



156.—Proposition. If from the extremities of the diameter of a semi-circle, two straight lines be drawn to any point in the circumference, the angle formed by them at that point will be a right angle. Let $a \ b \ c$, (Fig. 107,) be a given semi-circle; and $a \ b \ and \ b \ c$, lines drawn from the extremities of the diameter, $a \ c$, to the given point, b; the angle formed at that point by these lines, is a right angle. Join the point, b, and the centre, d; the lines, $d \ a, d \ b \ and \ d \ c$, being radii of the same circle, are equal; the angle at a is therefore equal, (Art. 142,) to the angle, $a \ b \ d$, also, the angle at c is, for the same reason, equal to the angle, $d \ b \ c$; the angle, $a \ b \ c$, being equal to the angles at $a \ and \ c$ taken together, must therefore, (Art. 153,) be a right angle.



157.—Proposition. The square of the hypothenuse of a right-angled triangle, is equal to the squares of the two remaining sides. Let $a \ b \ c$, (Fig. 108,) be a given right-angled triangle, having a square formed on each of its sides: then, the square, $b \ e$, is equal to the squares, $h \ c$ and $g \ b$, taken together. This can be

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proved by showing that the parallelogram, b l, is equal to the square, g b; and that the parallelogram, c l, is equal to the square, h c. The angle, c b d, is a right angle, and the angle, a b f, is a right angle; add to each of these the angle, a b c; then the angle, f b c, will evidently be equal, (Art. 140), to the angle, a b d; the triangle, f b c, and the square, g b, being both upon the same base, f b, and between the same parallels, f b and g c, the square, g b, is equal, (Art. 146,) to twice the triangle, f b c; the triangle, a b d, and the parallelogram, b l, being both upon the same base, b d, and between the same parallels, b d and a l, the parallelogram, b l, is equal to twice the triangle, a b d; the triangles, f b c and a b d, being equal to one another, (Art. 141,) the square, g b, is equal to the parallelogram, bl, either being equal to twice the triangle, fbc or abd. The method of proving h c equal to c l is exactly similar—thus proving the square, b e, equal to the squares, h c and g b, taken together.

This problem, which is the 47th of the First Book of Euclid, is said to have been demonstrated first by Pythagoras. It is stated, (but the story is of doubtful authority,) that as a thank-offering for its discovery he sacrificed a hundred oxen to the gods. From this circumstance, it is sometimes called the *hecatomb* problem. It is of great value in the exact sciences, more especially in Mensuration and Astronomy, in which many otherwise intricate calculations are by it made easy of solution.

These demonstrations, which relate mostly to the problems previously given, are introduced to satisfy the learner in regard to their mathematical accuracy. By studying and thoroughly understanding them, he will soonest arrive at a knowledge of their importance, and be likely the longer to retain them in memory. Should he have a relish for such exercises, and wish to continue them farther, he may consult Euclid's Elements, in which the whole subject of theoretical geometry is treated of in a manner sufficiently intelligible to be understood by the young mechanic.

The house carpenter, especially, needs information of this kind, and were he thoroughly acquainted with the principles of geometry, he would be much less liable to commit mistakes, and be better qualified to excel in the execution of his often difficult undertakings.

SECTION II.—ARCHITECTURE.

HISTORY OF ARCHITECTURE.

158.—Architecture has been defined to be—"the art of building;" but, in its common acceptation, it is—" the art of designing and constructing buildings, in accordance with such principles as constitute stability, utility and beauty." The literal signification of the Greek word *archi-tecton*, from which the word *architect* is derived, is chief-carpenter; but the architect has always been known as the chief *designer* rather than the chief *builder*. Of the three classes into which architecture has been divided—viz., Civil, Military, and Naval, the first is that which refers to the construction of edifices known as dwellings, churches and other public buildings, bridges, &c., for the accommodation of civilized man—and is the subject of the remarks which follow.

159.—This is one of the most ancient of the arts: the scriptures inform us of its existence at a very early period. Cain, the son of Adam,—"builded a city, and called the name of the city after the name of his son, Enoch"—but of the peculiar style or manner of building we are not informed. It is presumed that it was not remarkable for beauty, but that utility and perhaps stability were its characteristics. Soon after the deluge—that me



morable event, which removed from existence all traces of the works of man-the Tower of Babel was commenced. This was a work of such magnitude that the gathering of the materials, according to some writers, occupied three years; the period from its commencement until the work was abandoned, was twentytwo years; and the bricks were like blocks of stone, being twenty feet long, fifteen broad and seven thick. Learned men have given it as their opinion, that the tower in the temple of Belus at Babylon was the same as that which in the scriptures is called the Tower of Babel. The tower of the temple of Belus was square at its base, each side measuring one furlong, and consequently half a mile in circumference. Its form was that of a pyramid and its height was 660 feet. It had a winding passage on the outside from the base to the summit, which was wide enough for two carriages.

160.-Historical accounts of ancient cities, of which there are now but few remains-such as Babylon, Palmyra and Ninevah of the Assyrians; Sidon, Tyre, Aradus and Serepta of the Phoenicians; and Jerusalem, with its splendid temple, of the Israelites ---show that architecture among them had made great advances. Ancient monuments of the art are found also among other nations; the subterraneous temples of the Hindoos upon the islands, Elephanta and Salsetta; the ruins of Persepolis in Persia; pyramids, obelisks, temples, palaces and sepulchres in Egypt-all prove that the architects of those early times were possessed of skill and judgment highly cultivated. The principal characteristics of their works, are gigantic dimensions, immoveable solidity, and, in some instances, harmonious splendour. The extraordinary size of some is illustrated in the pyramids of Egypt. The largest of these stands not far from the city of Cairo: its base, which is square, covers about 11[‡] acres, and its height is nearly 500 feet. The stones of which it is built are immense-the smallest being full thirty feet long.

•161.—Among the Greeks, architeting was cultivated as a fine



art, and rapidly advanced towards perfection. Dignity and grace were added to stability and magnificence. In the Doric order, their first style of building, this is fully exemplified. Phidias, Ictinus and Callicrates, are spoken of as masters in the art at this period: the encouragement and support of Pericles stimulated them to a noble emulation. The Leautiful temple of Minerva, erected upon the acropolis of Athens, the Propyleum, the Odeum and others, were lasting monuments of their success. The Ionic and Corinthian orders were added to the Doric, and many magnificent edifices arose. These exemplified, in their chaste proportions, the elegant refinement of Grecian taste. Improvement in Grecian architecture continued to advance, until perfection seems to have been attained. The specimens which have been partially preserved, exhibit a combination of elegant proportion, dignified simplicity and majestic grandeur. Architecture among the Greeks was at the height of its glory at the period immediately preceding the Peloponnesian war; after which the art declined. An excess of enrichment succeeded its former simple grandeur; yet a strict regularity was maintained amid the profusion of ornament. After the death of Alexander, 323 B. C., a love of gaudy splendour increased: the consequent decline of the art was visible, and the Greeks afterwards paid but little attention to the science.

162.—While the Greeks were masters in architecture, which they applied mostly to their temples and other public buildings, the Romans gave their attention to the science in the construction of the many aqueducts and sewers with which Rome abounded; building no such plendid edifices as adorned Athens, Corinth and Ephesus, until about 200 years B. C., when their intercourse with the Greeks became more extended. Grecian architecture was introduced into Rome by Sylla; by whom, as also by Marius and Cæsar, many large edifices were erected in various cities of ltaly. But under Cæsar Augustus, at about the beginning of the christian era, the art arose to the greatest perfection it ever at-

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tained in Italy. Under his patronage, Grecian artists were encouraged, and many emigrated to Rome. It was at about this time that Solomon's temple at Jerusalem was rebuilt by Heroda Roman. This was 46 years in the erection, and was most probably of the Grecian style of building-perhaps of the Corinthian order. Some of the stones of which it was built were 46 feet long, 21 feet high and 14 thick; and others were of the astonishing length of 82 feet. 'The porch rose to a great height; the whole being built of white marble exquisitely polished. This is the building concerning which it was remarked-"Master, see what manner of stones, and what buildings are here." For the construction of private habitations also, finished artists were employed by the Romans: their dwellings being often built with the finest marble, and their villas splendidly adorned. After Augustus, his successors continued to beautify the city, until the reign of Constantine; who, having removed the imperial residence to Constantinople, neglected to add to the splendour of Rome; and the art, in consequence, soon fell from its high excellence.

Thus we find that Rome was indebted to Greece for what she possessed of architecture-not only for the knowledge of its principles, but also for many of the best buildings themselves; these having been originally erected in Greece, and stolen by the unprincipled conquerors-taken down and removed to Rome. Greece was thus robbed of her best monuments of architecture. Touched by the Romans, Grecian architecture lost much of its elegance and dignity. The Romans, though justiv celebrated for their scientific knowledge as displayed in the construction of their various edifices, were not capable of approxiating the simple grandeur, the refined elegance of the Grecian style; but sought to improve upon it by the addition of luxurious enrichment, and thus deprived it of true elegance. In the days of Nero, whose palace of gold is so celebrated, buildings were lavishly adorned. Adrian did much to encourage the art; but not satisfied with the simplicity of the Grecian style, the artists of his time aimed at

inventing new ones, and added to the already redundant embellishments of the previous age. Hence the origin of the pedestal, the great variety of intricate ornaments, the convex frieze, the round and the open pediments, &c. The rage for luxury continued until Alexander Severus, who made some improvement; but very soon after his reign, the art began rapidly to decline, as particularly evidenced in the mean and trifling character of the ornaments.

163.—The Goths and Vandals, when they overran the countries of Italy, Greece, Asia and Africa, destroyed most of the works of ancient architecture. Cultivating no art but that of war, these savage hordes could not be expected to take any interest in the beautiful forms and proportions of their habitations. From this time, architecture assumed an entirely different aspect. The celebrated styles of Greece were unappreciated and forgotten; and modern architecture took its first step on the platform of existence. The Goths, in their conquering invasions, gradually extended it over Italy, France, Spain, Portugal and Germany, into England. From the reign of Gallienus may be reckoned the total extinction of the arts among the Romans. From his time until the 6th or 7th century, architecture was almost entirely neglected. The buildings which were erected during this suspension of the arts, were very rude. Being constructed of the fragments of the edifices which had been demolished by the Visigoths in their unrestrained fury, and the builders being destitute of a proper knowledge of architecture, many sad blunders and extensive patchwork might have been seen in their construction-entablatures inverted, columns standing on their wrong ends, and other ridiculous arrangements characterized their clumsy work. The vast number of columns which the ruins around them afforded, they used as piers in the construction of arcades-which by some is thought, after having passed through various changes, to have been the origin of the plan of the Gothic cathedral. Buildings generally, which are not of the classical styles, and which were

erected after the fall of the Roman empire, have by some been indiscriminately included under the term *Gothic*. But the changes which architecture underwent during the dark ages, show that there were several distinct modes of building.

164.—Theodoric, king of the Ostrogoths, a friend of the arts, who reigned in Italy from A. D. 493 to 525, endeavoured to restore and preserve some of the ancient buildings; and erected others, the ruins of which are still seen at Verona and Ravenna. Simplicity and strength are the characteristics of the structures erected by him; they are, however, devoid of grandeur and elegance, or fine proportions. These are properly of the GOTHIC style; by some called the *old* Gothic to distinguish it from the pointed style, which is generally called *modern* Gothic.

165.-The Lombards, who ruled in Italy from A. D. 568, had no taste for architecture nor respect for antiquities. Accordingly, they pulled down the splendid monuments of classic architecture which they found standing, and erected in their stead huge buildings of stone which were greatly destitute of proportion, elegance or utility-their characteristics being scarcely any thing more than stability and immensity combined with ornaments of a puerile character. Their churches were disfigured with rows of small columns along the cornice of the pediment, small doors and windows with circular heads, roofs supported by arches having arched buttresses to resist their thrust, and a lavish display of incongruous ornaments. This kind of architecture is called, the LOMBARD style, and was employed in the 7th century in Pavia, the chief city of the Lombards; at which city, as also at many other places, a great many edifices were erected in accordance with its inelegant forms.

166.—The Byzantine architects, from Byzantium, Constantinople, erected many spacious edifices; among which are included the cathedrals of Bamberg, Worms and Mentz, and the most an cient part of the minster at Strasburg; in all of these they combined the Roman-Ionic order with the Gothic of the Lombards

This style is called the LOMBARD-BYZANTINE. To the last style there were afterwards added cupolas similar to those used in the east, together with numerous slender pillars with tasteless capitals, and the many minarets which are the characteristics of the proper Byzantine, or Oriental style.

167.-In the eighth century, when the Arabs and Moors destroyed the kingdom of the Goths, the arts and sciences were mostly in possession of the Musselmen-conquerors; at which time there were three kinds of architecture practised; viz: the Arabian, the Moorish and the modern-Gothic. The ARABIAN style was formed from Greek models, having circular arches added, and towers which terminated with globes and minarets. The MOORISH is very similar to the Arabian, being distinguished from it by arches in the form of a horse-shoe. It originated in Spain in the erection of buildings with the ruins of Roman architecture, and is seen in all its splendour in the ancient palace of the Mohammedan monarchs at Grenada, called the Alhambra, or redhouse. The MODERN-GOTHIC was originated by the Visigoths in Spain by a combination of the Arabian and Moorish styles; and introduced by Charlemagne into Germany. On account of the changes and improvements it there underwent, it was, at about the 13th or 14th century, termed the German, or romantic style. It is exhibited in great perfection in the towers of the minster of Strasburgh, the cathedral of Cologne and other edifices. The most remarkable features of this lofty and aspiring style, are the lancet or pointed arch, clustered pillars, lofty towers and flying buttresses. It was principally employed in ecclesiastical architecture, and in this capacity introduced into France, Italy, Spain, and England.

168.—The Gothic architecture of England is divided into the Norman, the Early-English, the Decorated, and the Perpendicular styles. The Norman is principally distinguished by the character of its ornaments—the chevron, or zigzag, being the most common. Buildings in this style were erected in the 12th

century. The Early-English is celebrated for the beauty of its edifices, the chaste simplicity and purity of design which they display, and the peculiarly graceful character of its foliage. This style is of the 13th century. The Decorated style, as its name implies, is characterized by a great profusion of enrichment, which consists principally of the crocket, or feathered-ornament, and ball-flower. It was mostly in use in the **15th** century. The Perpendicular style, which dates from the 15th century, is distinguished by its high towers, and parapets surmounted with spires similar in number and grouping to oriental minarets.

169.—Thus these several styles, which have been erroneously termed Gothic, were distinguished by peculiar characteristics as well as by different names. The first symptoms of a desire to return to a pure style in architecture, after the ruin caused by the Goths, was manifested in the character of the art as displayed in the church of St. Sophia at Constantinople, which was erected by Justinian in the 6th century. The church of St. Mark at Venice, which arose in the 10th or 11th century, was the work of Grecian architects, and resembles in magnificence the forms of ancient architecture. The cathedral at Pisa, a wonderful structure for the age, was erected by a Grecian architect in 1016. The marble with which the walls of this building were faced, and of which the four rows of columns that support the roof are composed, is said to be of an excellent character. The Campanile, or leaning-tower as it is usually called, was erected near the cathedral in the 12th century. Its inclination is generally supposed to have arisen from a poor foundation; although by some it is said to have been thus constructed originally, in order to inspire in the minds of the beholder sensations of sublimity and awe. In the 13th century, the science in Italy was slowly progressing; many fine churches were erected, the style of which displayed a decided advance in the progress towards pure classical architecture. In other parts of Europe, the Gothic, or pointed style, was prevalent. The cathedral at Strasburg, designed by Irwin Steinbeck, was erected

in the 13th and 14th centuries. In France and England during the 14th century, many very superior edifices were erected in this style.

170.-In the 14th and 15th centuries, and particularly in the latter, architecture in Italy was greatly revived. The masters began to study the remains of ancient Roman edifices; and many splendid buildings were erected, which displayed a purer taste in the Among others, St. Peter's of Rome, which was built science. about this time, is a lasting monument of the architectural skill of the age. Giocondo, Michael Angelo, Palladio, Vignola, and other celebrated architects, each in their turn, did much to restore the art to its former excellence. In the edifices which were erected under their direction, however, it is plainly to be seen that they studied not from the pure models of Greece, but from the remains of the deteriorated architecture of Rome. The high pedestal, the coupled columns, the rounded pediment, the many curved-and-twisted enrichments, and the convex frieze, were unknown to pure Grecian architecture. Yet their efforts were serviceable in correcting, to a good degree, the very impure taste that had prevailed since the overthrow of the Roman empire.

171.—At about this time, the Italian masters and numerous artists who had visited Italy for the purpose, spread the Roman style over various countries of Europe; which was gradually received into favor in place of the modern-Gothic. This fell into disuse; although it has of late years been again cultivated. It requires a building of great magnitude and complexity for a perfect display of its beauties. In America at the present time, the pure Grecian style is more or less studied; and perhaps the simplicity of its principles is better adapted to a republican country, than the intricacy and extent of those of the Gothic.

STYLES OF ARCHITECTURE.

172.—It is generally acknowledged that the various styles in architecture, were originated in accordance with the different pur-

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suits of the early inhabitants of the earth; and were brought by their descendants to their present state of perfection, through the propensity for imitation and desire of emulation which are found more or less among all nations. Those that followed agricultural pursuits, from being employed constantly upon the same piece of land, needed a permanent residence, and the wooden hut was the offspring of their wants; while the shepherd, who followed his flocks and was compelled to traverse large tracts of country for pasture, found the *tent* to be the most portable habitation ; again, the man devoted to hunting and fishing-an idle and vagabond way of living-is naturally supposed to have been content with the cavern as a place of shelter. The latter is said to have been the origin of the Egyptian style; while the curved roof of Chinese structures gives a strong indication of their having had the tent for their model; and the simplicity of the original style of the Greeks, (the Doric,) shows quite conclusively, as is generally conceded, that its original was of wood. The modern-Gothic, or pointed style, which was most generally confined to ecclesiastical structures, is said by some to have originated in an attempt 🌰 imitate the bower, or grove of trees, in which the ancients performed their idol-worship.

173.—There are numerous styles, or orders, in architecture; and a knowledge of the peculiarities of each, is important to the student in the art. The STYLOBATE is the substructure, or basement, upon which the columns of an order are arranged. In Roman architecture—especially in the interior of an edifice—it frequently occurs that each column has a separate substructure; this is called a *pedestal*. If possible, the pedestal should be avoided in all cases; because it gives to the column the appearance of having been originally designed for a small building, and afterwards pieced-out to make it long enough for a larger one.

174.—An ORDER, in architecture, is composed of two principal parts, viz: the column and the entablature.

175.—The COLUMN is composed of the base, shaft and capital.

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176.—The ENTABLATURE, above and supported by the columns, is horizontal; and is composed of the architrave, frieze and cornice. These principal parts are again divided into various members and mouldings. (See Sect. III.)

177.—The BASE of a column is so called from *basis*, a foundation, or footing.

178.—The SHAFT, the upright part of a column standing upon the base and crowned with the capital, is from *shafto*, to dig in the manner of a well, whose inside is not unlike the form of a column.

179.—The CAPITAL, from *kephale* or *caput*, the head, is the uppermost and crowning part of the column.

180.—The ARCHITRAVE, from *archi*, chief or principal, and *trahs*, a beam, is that part of the entablature which lies in immediate connection with the column.

181.—The FRIEZE, from *fibron*, a fringe or border, is that part of the entablature which is immediately above the architrave and preath the cornice. It was called by some of the ancients, *zophorus*, because it was usually enriched with sculptured animals.

182.—The CORNICE, from corona, to crown, is the upper and projecting part of the entablature—being also the uppermost and crowning part of the whole order.

183.—The PEDIMENT, above the entablature, is the triangular portion which is formed by the inclined edges of the roof at the end of the building. In Gothic architecture, the pediment is called, a *gable*.

184.—The TYMPANUM is the perpendicular triangular surface which is enclosed by the cornice of the pediment.

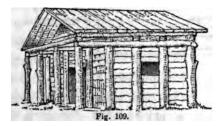
185.—The ATTIC is a small order, consisting of pilasters and entablature, raised above a larger order, instead of a pediment. An attic story is the upper story, its windows being usually square.

186.—An order, in architecture, has its several parts and members proportioned to one another by a scale of 60 equal parts, which are called minutes. If the height of buildings were always the same, the scale of equal parts would be a fixed quantity-an exact number of feet and inches. But as buildings are erected of different heights, the column and its accompaniments are required to be of different dimensions. To ascertain the scale of equal parts, it is necessary to know the height to which the whole order is to be erected. This must be divided by the number of diameters which is directed for the order under consideration. Then the quotient obtained by such division, is the length of the scale of equal parts-and is, also, the diameter of the column next above the base. For instance, in the Grecian Doric order the whole height, including column and entablature, is 8 diameters. Suppose now it were desirable to construct an example of this order, forty feet high. Then 40 feet divided by 8 gives 5 feet for the length of the scale; and this being divided b 60, the scale is completed. The upright columns of figures, marked H and P, by the side of the drawings illustrating the ord designate the height and the projection of the members. The projection of each member is reckoned from a line passing through the axis of the column, and extending above it to the top of the entablature. The figures represent minutes, or 60ths, of the major diameter of the shaft of the column.

187.—GRECIAN STYLES. The original method of building among the Greeks, was in what is called the *Doric* order: to this were afterwards added the *Ionic* and the *Corinthian*. These three were the only styles known among them. Each is distinguished from the other two, by not only a peculiarity of some one or more of its principal parts, but also by a particular destination. The character of the Doric is robust, manly and Herculean-like; that of the Ionic is more delicate, feminine, matronly; while that of the Corinthian is extremely delicate, youthful and virgin-like. However they may differ in

their general character, they are alike famous for grace and dignity, elegance and grandeur, to a high degree of perfection.

188.—The DORIC ORDER is so ancient that its origin is unknown—although some have pretended to have discovered it. But the most general opinion is, that it is an improvement upon the original log huts of the Grecians. These no doubt were very rude, and perhaps not unlike the following figure.

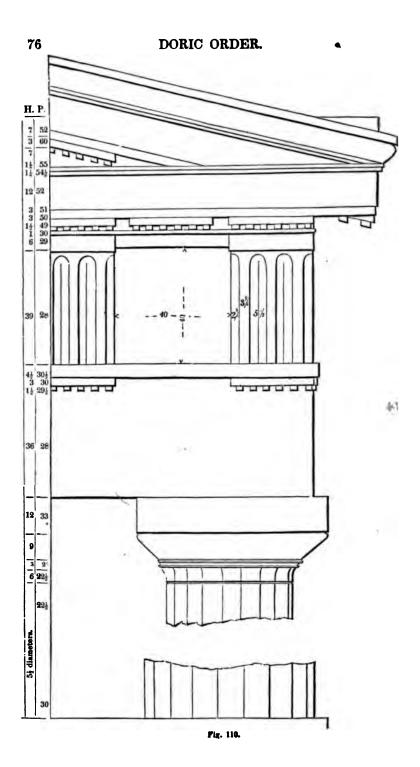


The trunks of trees, set perpendicularly to support the roof, may be taken for columns; the tree laid upon the tops of the perpendicular ones, the architrave; the ends of the cross-beams

which rest upon the architrave, the triglyphs; the tree laid on the cross-beams as a support for the ends of the rafters, the bedmoulding of the cornice; the ends of the rafters which project beyond the bed-moulding, the mutules; and perhaps the projection the roof in front, to screen the entrance from the weather, gave origin to the portico.

The peculiarities of the Doric order are the triglyphs—those parts of the frieze which have perpendicular channels cut in their surface; the absence of a base to the column—as also of fillets between the flutings of the column, and the plainness of the capital. The triglyphs are to be so disposed that the width of the metopes—the spaces between the triglyphs—shall be equal to their height.

189.—The intercolumniation, or space between the columns, is regulated by placing the centres of the columns under the centres of the triglyphs—except at the angle of the building; where, as may be seen in Fig. 110, one edge of the triglyph must be over the centre of the column. Where the columns are so disposed that one of them stands beneath every other triglyph, the arrangement is called, mono-triglyph, and is most common.



When a column is placed beneath every third triglyph, the arrangement is called *diastyle*; and when beneath every fourth, *aræostyle*. This last style is the worst, and is seldom practised.

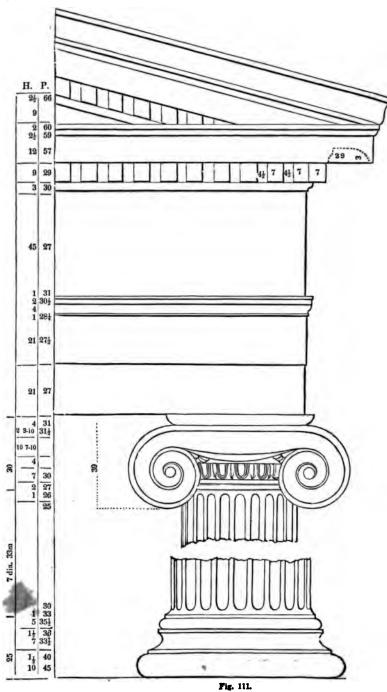
190.—The Doric order is suitable for buildings that are destined for national purposes, for banking-houses, &c. Its appearance, though massive and grand, is nevertheless rich and graceful. The Custom-House and the Union Bank, in New-York city, are good specimens of this order.

191.—The IONIC ORDER. The Doric was for some time the only order in use among the Greeks. They gave their attention to the cultivation of it, until perfection seems to have been attained. Their temples were the principal objects upon which their skill in the art was displayed; and as the Doric order seems to have been well fitted, by its massive proportions, to represent the character of their male deities rather than the female, there seems to have been a necessity for another style which should be amblematical of feminine graces, and with which they might lecorate such temples as were dedicated to the goddesses. Hence the origin of the Ionic order. This was invented, according to historians, by Hermogenes of Alabanda; and he being a native of Caria, then in the possession of the Ionians, the order was called, the Ionic.

192.—The distinguishing features of this order are the volutes, or spirals of the capital; and the *dentils* among the bed-mouldings of the cornice: although in some instances, dentils are wanting. The volutes are said to have been designed as a representation of curls of hair on the head of a matron, of whom the whole column is taken as a semblance.

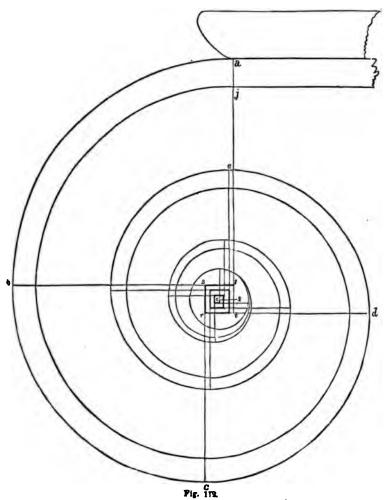
193.—The intercolumniation of this and the other orders both Roman and Grecian, with the exception of the Doric—are distinguished as follows. When the interval is one and a half ... diameters, it is called, *pycnostyle*, or columns thick-set; when. two diameters, *systyle*; when two and a quarter diameters, *eustyle*; when three diameters, *diastyle*; and when more than

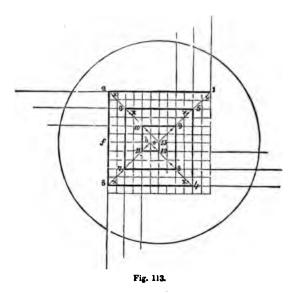




three diameters, *aræostyle*, or columns thin-set. In all the orders, when there are four columns in one row, the arrangement is called, *tetrastyle*; when there are six in a row, *hexastyle*; and when eight, *octastyle*.

194.—The Ionic order is appropriate for churches, colleges, seminaries, libraries, all edifices dedicated to literature and the arts, and all places of peace and tranquillity. The front of the Merchants' Exchange, New-York city, is a good specimen of this order.





195.—To describe the Ionic volute. Draw a perpendicular from a to s, (Fig. 112,) and make a s equal to 20 min. or to $\frac{1}{7}$ of the whole height, a c; draw s o, at right angles to s a, and equal to 1 min.; upon o, with 2_{*} min. for radius, describe the eye of the volute; about o, the centre of the eye, draw the square, r t 12, with sides equal to half the diameter of the eye, viz., 2_1 min., and divide it into 144 equal parts, as shown at Fig. 113. The several centres in rotation are at the angles formed by the heavy lines, as figured, 1, 2, 3, 4, 5, 6, &c. The position of these angles is determined by commencing at the point, 1, and making each heavy line one part less in length than the preceding one. No. 1 is the centre for the arc, a b, (Fig. 112;) 2 is the centre for the arc, b c; and so on to the last. The inside spiral line is to be described from the centres, x, x, x, &c., (Fig. 113,) being the centre of the first small square towards the middle of the eye from the centre for the outside arc. The breadth of the fillet at a j, is to be made equal to 2_{10}^3 min. This is for a spiral of three revolutions; but one of any number of revolutions, as 4 or 6,

may be drawn, by dividing o f, (Fig. 113,) into a corresponding number of equal parts. Then divide the part nearest the centre, o, into two parts, as at h; join o and 1, also o and 2; draw h 3, parallel to o 1, and h 4, parallel to o 2; then the lines, o 1, o 2, h 3, h4, will determine the length of the heavy lines, and the place of the centres. (See Art. 396.)

196.—The CORINTHIAN ORDER is in general like the Ionic, though the proportions are lighter. The Corinthian displays a more airy elegance, a richer appearance; but its distinguishing feature is its beautiful capital. This is generally supposed to have had its origin in the capitals of the columns of Egyptian temples; which, though not approaching it in elegance, have yet a similarity of form with the Corinthian. The oft-repeated story of its origin which is told by Vitruvius-an architect who flourished in Rome, in the days of Augustus Cæsar-though pretty generally considered to be fabulous, is nevertheless worthy of being again It is this: a young lady of Corinth was sick, and recited. finally died. Her nurse gathered into a deep basket, such trinkets and keepsakes as the lady had been fond of when alive, and placed them upon her grave; covering the basket with a flat stone or tile, that its contents might not be disturbed. The basket was placed accidentally upon the stem of an acanthus plant, which, shooting forth, enclosed the basket with its foliage; some of which, reaching the tile, turned gracefully over in the form of a volute.



A celebrated sculptor, Calima chus, saw the basket thus decorated, and from the hint which it suggested, conceived and constructed a capital for a column. This was called Corinthian from the fact that it was invented and first made use of at Corinth.

197.—The Corinthian being the gayest, the richest and most lovely of all the Orders, it is appropriate for edifices which are

CORINTHIAN.

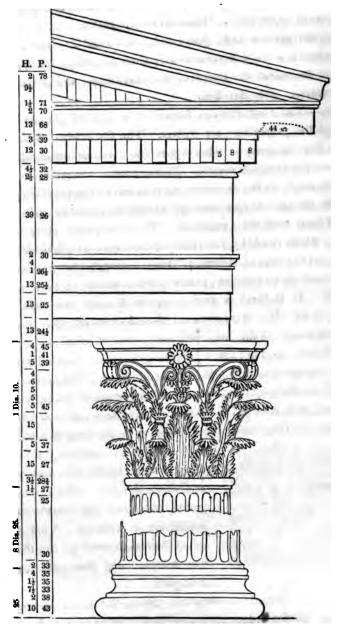


Fig. 115

dedicated to amusement, banqueting and festivity---for all places where delicacy, gayety and splendour are desirable.

198.—In addition to the three regular orders of architecture, it was sometimes customary among the Greeks—and afterwards among other nations—to employ representations of the human form, instead of columns, to support entablatures; these were called *Persians* and *Caryatides*.

199.—PERSIANS are statues of men, and are so called in commemoration of a victory gained over the Persians by Pausanias. The Persian prisoners were brought to Athens and condemned to abject slavery; and in order to represent them in the lowest state of servitude and degradation, the statues were loaded with the heaviest entablature, the Doric.

200.—CARYATIDES are statues of women dressed in long robes after the Asiatic manner. Their origin is as follows. In a war between the Greeks and the Caryans, the latter were totally vanquished, their male population extinguished, and their females carried to Athens. To perpetuate the memory of this event, statues of females, having the form and dress of the Caryans, were erected, and crowned with the Ionic or Corinthian entablature. The caryatides were generally formed of about the human size, but the persians much larger; in order to produce the greater awe and astonishment in the beholder. The entablatures were proportioned to a statue in like manner as to a column of the same height.

201.—These semblances of slavery have been in frequent use among moderns as well as ancients; and as a relief from the stateliness and formality of the regular orders, are capable of forming a thousand varieties; yet in a land of liberty such marks of human degradation ought not to be perpetuated.

202.—ROMAN STYLES. Strictly speaking, Rome had no architecture of her own—all she possessed was borrowed from other nations. Before the Romans exchanged intercourse with the Greeks, they possessed some edifices of considerable extent

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and merit, which were erected by architects from Etruria; but Rome was principally indebted to Greece for what she acquired of the art. Although there is no such thing as an architecture of Roman invention, yet no nation, perhaps, ever was so devoted to the cultivation of the art as the Roman. Whether we consider the number and extent of their structures, or the lavish richness and splendour with which they were adorned, we are compelled to yield to them our admiration and praise. At one time, under the consuls and emperors, Rome employed 400 architects. The public works-such as theatres, circuses, baths, aqueducts, &c.were, in extent and grandeur, beyond any thing attempted in Aqueducts were built to convey water from a modern times. distance of 60 miles or more. In the prosecution of this work, rocks and mountains were tunnelled, and valleys bridged. Some of the latter descended 200 feet below the level of the water; and in passing them the canals were supported by an arcade, or succession of arches. Public baths are spoken of as large as cities; being fitted up with numerous conveniences for exercise and amusement. Their decorations were most splendid; indeed, the exuberance of the ornaments alone was offensive to good taste. So overloaded with enrichments were the baths of Diocletian, that on an occasion of public festivity, great quantities of sculpture fell from the ceilings and entablatures, killing many of the people.

203.—The three orders of Greece were introduced into Rome in all the richness and elegance of their perfection. But the luxurious Romans, not satisfied with the simple elegance of their refined proportions, sought to improve upon them by lavish displays of ornament. They transformed in many instances, the true elegance of the Grecian art into a gaudy splendour, better suited to their less refined taste. The Romans remodelled each of the orders : the Doric was modified by increasing the height of the column to 8 diameters; by changing the echinus of the capital for an ovolo, or quarter-round, and adding an astragal and neck

below it; by placing the centre of the first triglyph, instead of one edge, over the centre of the column; and introducing horizontal instead of inclined mutules in the cornice. The Ionic was modified by diminishing the size of the volutes, and, in some specimens, introducing a new capital in which the volutes were diagonally arranged. This new capital has been termed modern Ionic. The favorite order at Rome and her colonies was the Corinthian. The Roman artists, in their search for novelty, subjected it to many alterations-especially in the foliage of its capi-Into the upper part of this, they introduced the modified tal. Ionic capital; thus combining the two in one. This change was dignified with the importance of an order, and received the appellation COMPOSITE, or Roman: the best specimen of which is found in the Arch of Titus. This style was not much used among the Romans themselves, and is but slightly appreciated now. Its decorations are too profuse-a standing monument of the luxury of the age in which it was invented.

204.—The TUSCAN ORDER is said to have been introduced to the Romans by the Etruscan architects, and to have been the only style used in Ita'y before the introduction of the Grecian orders. However this may be, its similarity to the Doric order gives strong indications of its having been a rude imitation of that style: this is very probable, since history informs us that the Etruscans held intercourse with the Greeks at a remote period. The rudeness of this order prevented its extensive use in Italy. All that is known concerning it is from Vitruvius—no remains of buildings in this style being found among ancient ruins.

205. For mills, factories, markets, barns, stables, &c., where utility and strength are of more importance than beauty, the improve 1 modification of this order, called the *modern* Tuscan, (*Fig.* 116,) will be useful; and its simplicity recommends it where economy is desirable.

206.—EGYPTIAN STYLE. The architecture of the ancient

TUSCAN.

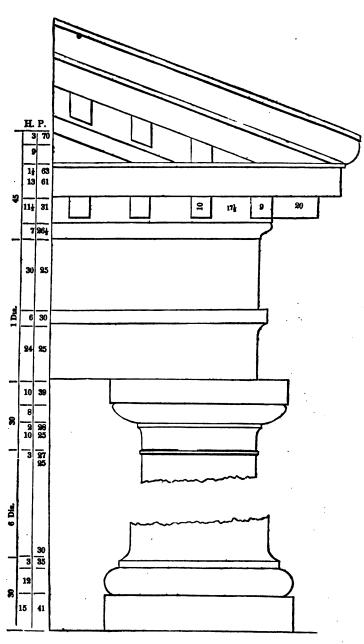


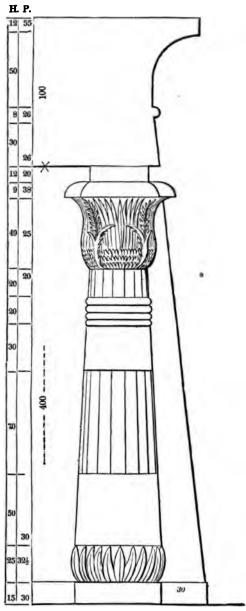
Fig. 116.

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Egyptians-to which that of the ancient Hindoos bears some resemblance-is characterized by boldness of outline, solidity and grandeur. The amazing labyrinths and extensive artificial lakes, the splendid palaces and gloomy cemeteries, the gigantic pyramids and towering obelisks, of the Egyptians, were works of immensity and durability; and their extensive remains are enduring proofs of the enlightened skill of this once-powerful, but long since extinct nation. The principal features of the Egyptian Style of architecture are-uniformity of plan, never deviating from right lines and angles; thick walls, having the outer surface slightly deviating inwardly from the perpendicular; the whole building low; roof flat, composed of stones reaching in one piece from pier to pier, these being supported by enormous columns, very short in proportion to their height; the shaft sometimes polygonal, having no base but with a great variety of handsome capitals, the foliage of these being of the palm, lotus and other leaves; entablatures having simply an architrave, crowned with a huge cavetto ornamented with sculpture; and the intercolumniation very narrow, usually $1\frac{1}{2}$ diameters and seldom exceeding $2\frac{1}{2}$. In the remains of a temple, the walls were found to be 24 feet thick; and at the gates of Thebes, the walls at the foundation were 50 feet thick and perfectly solid. The immense stones of which these, as well as Egyptian walls generally, were built, had both their inside and outside surfaces faced, and the joints throughout the body of the wall as perfectly close as upon the outer surface. For this reason, as well as that the buildings generally partake of the pyramidal form, arise their great solidity and durability. The dimensions and extent of the buildings may be judged from the temple of Jupiter at Thebes, which was 1400 feet long and 300 feet wideexclusive of the porticos, of which there was a great number.

It is estimated by Mr. Gliddon, U. S. consul in Egypt, that not less than 25,000,000 tons of hewn stone were employed in the erection of the Pyramids of Memphis alone,—or enough to construct 3,000 Bunker-Hill monuments. Some of the blocks are 40





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Fig. 117.

feet long, and polished with emery to a surprising degree. It is conjectured that the stone for these pyramids was brought, by rafts and canals, from a distance of 6 or 7 hundred miles.

207.—The general appearance of the Egyptian style of architecture is that of solemn grandeur—amounting sometimes to sepulchral gloom. For this reason it is appropriate for cemeteries, prisons, &c.; and being adopted for these purposes, it is gradually gaining favour.

A great dissimilarity exists in the proportion, form and general features of Egyptian columns. In some instances, there is no uniformity even in those of the same building, each differing from the others either in its shaft or capital. For practical use in this country, Fig. 117 may be taken as a standard of this style. The Halls of Justice in Centre-street, New-York city, is a building in general accordance with the principles of Egyptian architecture.

Buildings in General.

208.—That style of architecture is to be preferred in which utility, stability and regularity, are gracefully blended with grandeur and elegance. But as an arrangement designed for a warm country would be inappropriate for a colder climate, it would seem that the style of building ought to be modified to suit the wants of the people for whom it is designed. High roofs to resist the pressure of heavy snows, and arrangements for artificial heat, are indispensable in northern climes; while they would be regarded as entirely out of place in buildings at the equator.

209.—Among the Greeks, architecture was employed chiefly upon their temples and other large buildings; and the proportions of the orders, as determined by them, when executed to such large dimensions, have the happiest effect. But when used for small buildings, porticos, porches, &c., especially in country-places, they are rather heavy and clumsy; in such cases, more slender proportions will be found to produce a better effect. The

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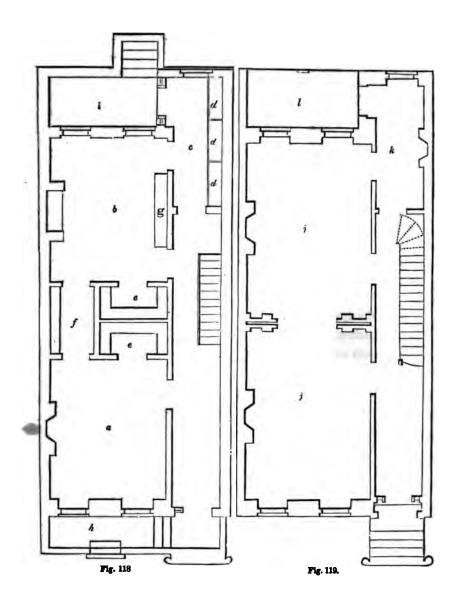
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English cottage-style is rather more appropriate, and is becoming extensively practised for small buildings in the country.

210.—Every building should bear an expression suited to its destination. If it be intended for national purposes, it should be magnificent—grand; for a private residence, neat and modest; for a banqueting-house, gay and splendid; for a monument or cemetery, gloomy—melancholy; or, if for a church, majestic and graceful. By some it has been said—"somewhat dark and gloomy, as being favourable to a devotional state of feeling;" but such impressions can only result from a misapprehension of the nature of true devotion. "Her ways are ways of *pleasantness*, and all her paths are peace." The church should rather be a type of that brighter world to which it leads.

211.—However happily the several parts of an edifice may be disposed, and however pleasing it may appear as a whole, yet much depends upon its *site*, as also upon the character and style of the structures in its immediate vicinity, and the degree of cultivation of the adjacent country. A splendid country-seat should have the out-houses and fences in the same style with itself, the trees and shrubbery heatly trimmed, and the grounds well cultivated.

212.—Europeans express surprise that so many houses in this country are built of wood. And yet, in a new country, where wood is plenty, that this should be so is no cause for wonder. Still, the practice should not be encouraged. Buildings erected with brick or stone are far preferable to those of wood; they are more durable; not so liable to injury by fire, nor to need repairs; and will be found in the end quite as economical. A wooden house is suitable for a temporary residence only; and those who would bequeath a dwelling to their children, will endeavour to build with a more durable material. Wooden cornices and gutters, attached to brick houses, are objectionable—not only on account of their frail nature, but also because they render the building liable to destruction by fire.



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213.—Dwelling houses are built of various dimensions and styles, according to their destination; and to give designs and directions for their erection, it is necessary to know their situation and object. A dwelling intended for a gardener, would require very different dimensions and arrangements from one intended for a retired gentleman—with his servants, horses, &c.; nor would a house designed for the city, be appropriate for the country. For city houses, arrangements that would be convenient for one family, might be very inconvenient for two or more. Fig. 118, 119, 120 and 121, represent the *ichnographical projection*, or groundplan, of the floors of an ordinary city house, designed to be occupied by one family only. Fig. 122 is an *elevation*, or front-view, of the same house: all these plans are drawn at the same scale which is that at the bottom of Fig. 122.

Fig. 118 is a plan of the basement.

a is the dining-room.

b-kitchen.

c-wash-room.

d, d, d,—wash-troughs.

e, e,—pantries with shelving.

f—passage having shelves, drawers, &c., on one side, and clothes-hooks on the other.

g-kitchen-dresser.

h, i,—front and rear areas.

Fig. 119-plan of the first-story.

j, j,—parlours.

k-library.

l-portico.

Fig. 120—plan of the second-story.

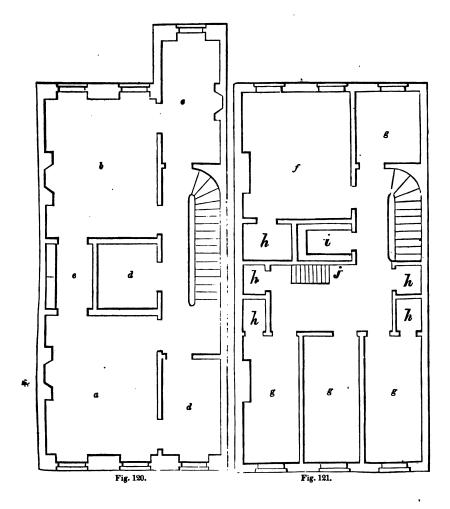
a-toilet and sitting room.

b-principal bed-chamber.

c-bath-room.

d, d,—bed-chambers.

e-passage with wardrobe and clothes-hooks.



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Fig. 121—plan of the attic-story.

f-nursery,

g, g, g, g, -bed-chambers,

h, h, h, h, h,-wardrobes,

i—pantry with shelves,

j—step-ladder leading to roof.

Fig. 122-front elevation.

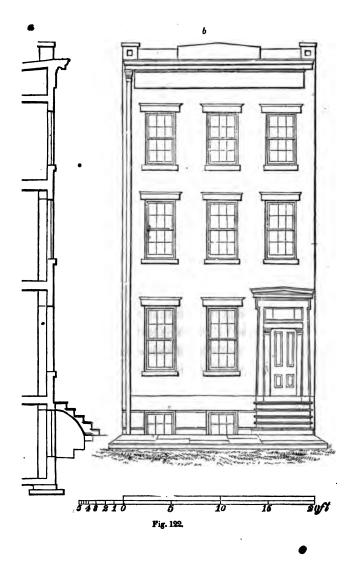
a-section,

b-front,

These are introduced to give some general ideas of the principles to be followed in designing city houses. The width of city lots is ordinarily 25 feet, but as it has become a common practice to reduce this size, on account of the enhanced value of land, the plans here given are designed for a lot only 20 feet wide-the ordinary width of many buildings of this class. In placing the chimneys, make the parlours of equal size, and set the chimneybreast in the middle of the space between the sliding-door partition and the front (and rear) walls. The basement chimneybreasts may be placed in the middle of the side of the room, as there is but one flue to pass through the chimney-breast above; but in the second-story, as there are two flues, one from the basement and one from the parlour, the breast will have to be placed nearly perpendicular over the parlour breast, so as to receive the flues within the jambs of the fire-place. As it is desirable to have the chimney-breast as near the middle of the room as possible, it may be placed a few inches towards that point from over the breast below. So in arranging those of the stories above, always make provision for the flues from below.

214.—In placing the stairs, there should be at least as much room in the passage at the side of the stairs, as upon them; and in regard to the length of the passage in the second story, there must be room for the doors which open from each of the principal rooms into the hall, and more if the stairs require it. Having assigned a position for the stairs of the second story, let the winders of

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the other stories be placed perpendicularly over and under them; and be careful to provide for head-room. To ascertain this, when it is doubtful, it is well to draw a vertical section of the whole stairs; but in ordinary cases, this is not necessary. To dispose the windows properly, the middle window of each story should be exactly in the middle of the front; but the pier between the two windows which light the parlour, should be in the centre of that room; because when chandeliers or any similar ornaments, hang from the centre-pieces of the parlour ceilings, it is important, in order to give the better effect, that the pier-glasses at the front and rear, be in a range with them. If both these objects cannot be attained, an approximation to each must be attempted. The piers should in no case be less in width than the window openings, else the blinds or shutters when thrown open will interfere with one another; in general practice, it is well to make the outside piers # of the width of one of the middle piers. When this is desirable, deduct the amount of the three openings from the width of the front, and the remainder will be the amount of the width of all the piers; divide this by 10, and the product will be 1 of a middle pier; and then, if the parlour arrangements do not interfere, give twice this amount to each corner pier, and three times the same amount to each of the middle piers.

PRINCIPLES OF ARCHITECTURE.

215.—In the construction of the first habitations of men, frail and rude as they must have been, the first and principal object was, doubtless, utility—a mere shelter from sun and rain. But as successive storms shattered the poor tenement, man was taught by experience the necessity of building with an idea to durability. And when in his walks abroad, the symmetry, proportion and beauty of nature met his admiring gaze, contrasting so strangely with the misshapen and disproportioned work of his own hands, he was led to make gradual changes; till his abode was rendered

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ARCHITECTURE.

not only commodious and durable, but pleasant in its appearance; and building became a fine-art, having utility for its basis.

216.-In all designs for buildings of importance, utility, durability and beauty, the first great principles of architecture, should be pre-eminent. In order that the edifice be useful, commodious and comfortable, the arrangement of the apartments should be such as to fit them for their several destinations; for public assemblies, oratory, state, visitors, retiring, eating, reading, sleeping, bathing, dressing, &c.—these should each have its own peculiar form and situation. To accomplish this, and at the same time to make their relative situation agreeable and pleasant, producing regularity and harmony, require in some instances much skill and sound judgment. Convenience and regularity are very important, and each should have due attention; yet when both cannot be obtained, the latter should in most cases give place to the for-A building that is neither convenient nor regular, whatever mer. other good qualities it may possess, will be sure of disapprobation.

217.—The utmost importance should be attached to such arrangements as are calculated to promote health : among these, ventilation is by no means the least. For this purpose, the ceilings of the apartments should have a respectable height; and the skylight, or any part of the roof that can be made moveable, should be arranged with cord and pullies, so as to be easily raised and lowered. Small openings near the ceiling, that may be closed at pleasure, should be made in the partitions that separate the rooms from the passages—especially for those rooms which are used for sleeping apartments. All the apartments should be so arranged as to secure their being easily kept dry and *clean*. In dwellings, suitable apartments for conveying the water.

218.—To insure stability in an edifice, it should be designed upon well-known geometrical principles : such as science has demonstrated to be necessary and sufficient for firmness and dura-

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bility. It is well, also, that it have the *appearance* of stability as well as the *reality*; for should it seem tottering and unsafe, the sensation of fear, rather than those of admiration and pleasure, will be excited in the beholder. To secure certainty and accuracy in the application of those principles, a knowledge of the strength and other properties of the materials used, is indispensable; and in order that the whole design be so made as to be capable of execution, a practical knowledge of the requisite mechanical operations is quite important.

219.—The elegance of an architectural design, although chiefly depending upon a just proportion and harmony of the parts, will be promoted by the introduction of ornaments-provided this be judiciously performed. For enrichments should not only be of a proper character to suit the style of the building, but should also have their true position, and be bestowed in proper quantity. The most common fault, and one which is prominent in Roman architecture, is an excess of enrichment: an error which is carefully to be guarded against. But those who take the Grecian models for their standard, will not be liable to go to that extreme. In ornamenting a cornice, or any other assemblage of mouldings, at least every alternate member should be left plain; and those that are near the eye should be more finished than those which are dis-Although the characteristics of good architecture are utilitant. ty and elegance, in connection with durability, yet some buildings are designed expressly for use, and others again for ornament : in the former, utility, and in the latter, beauty, should be the governing principle.

220.—The builder should be intimately acquainted with the principles upon which the essential, elementary parts of a building are founded. A scientific knowledge of these will insure certainly and security, and enable the mechanic to erect the most extensive and lofty edifices with confidence. The more important parts are the foundation, the column, the wall, the lintel, the arch, the vault, the dome and the roof. A separate description of the

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peculiarities of each, would seem to be necessary; and cannot perhaps be better expressed than in the following language of a modern writer on this subject.

221.—"In laying the FOUNDATION of any building, it is necessary to dig to a certain depth in the earth, to secure a solid basis, below the reach of frost and common accidents. The most solid basis is rock, or gravel which has not been moved. Next to these are clay and sand, provided no other excavations have been made in the immediate neighbourhood. From this basis a stone wall is carried up to the surface of the ground, and constitutes the foundation. Where it is intended that the superstructure shall press unequally, as at its piers, chimneys, or columns, it is sometimes of use to occupy the space between the points of pressure by an inverted arch. This distributes the pressure equally, and prevents the foundation from springing between the different points. In loose or muddy situations, it is always unsafe to build, unless we can reach the solid bottom below. In salt marshes and flats, this is done by depositing timbers, or driving wooden piles into the earth, and raising walls upon them. The preservative quality of the salt will keep these timbers unimpaired for a great length of time, and makes the foundation equally secure with one of brick or stone.

222.—The simplest member in any building, though by no means an essential one to all, is the COLUMN, or *pillar*. This is a perpendicular part, commonly of equal breadth and thickness, not intended for the purpose of enclosure, but simply for the support of some part of the superstructure. The principal force which a column has to resist, is that of perpendicular pressure. In its shape, the shaft of a column should not be exactly cylindrical, but, since the lower part must support the weight of the superior part, in addition to the weight which presses equally on the whole column, the thickness should gradually decrease from bottom to top. The outline of columns should be a little curved, so as to represent a portion of a very long spheroid, or paraboloid,

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rather than of a cone. This figure is the joint result of two calculations, independent of beauty of appearance. One of these is, that the form best adapted for stability of base is that of a cone; the other is, that the figure, which would be of equal strength throughout for supporting a superincumbent weight, would be generated by the revolution of two parabolas round the axis of the column, the vertices of the curves being at its extremities. The swell of the shafts of columns was called the entasis by the ancients. It has been lately found, that the columns of the Parthenon, at Athens, which have been commonly supposed straight, deviate about an inch from a straight line, and that their greatest swell is at about one third of their height. Columns in the antique orders are usually made to diminish one sixth or one seventh of their diameter, and sometimes even one The Gothic pillar is commonly of equal thickness fourth. throughout.

223.—The WALL, another elementary part of a building, may be considered as the lateral continuation of the column, answering the purpose both of enclosure and support. A wall must diminish as it rises, for the same reasons, and in the same proportion, as the column. It must diminish still more rapidly if it extends through several stories, supporting weights at different heights. A wall, to possess the greatest strength, must also consist of pieces, the upper and lower surfaces of which are horizontal and regular, not rounded nor oblique. The walls of most of the ancient structures which have stood to the present time, are constructed in this manner, and frequently have their stones bound together with bolts and cramps of iron. The same method is adopted in such modern structures as are intended to possess great strength and durability, and, in some cases, the stones are even dove-tailed together, as in the light-houses at Eddystone and Bell Rock. But many of our modern stone walls, for the sake of cheapness, have only one face of the stones squared, the inner half of the wall being completed with brick; so that they can,

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in reality, be considered only as brick walls faced with stone. Such walls are said to be liable to become convex outwardly, from the difference in the shrinking of the cement. *Rubble* walls are made of rough, irregular stones, laid in mortar. The stones should be broken, if possible, so as to produce horizontal surfaces. The *coffer* walls of the ancient Romans were made by enclosing successive portions of the intended wall in a box, and filling it with stones, sand, and mortar, promiscuously. This kind of structure must have been extremely insecure. The Pantheon, and various other Roman buildings, are surrounded with a double brick wall, having its vacancy filled up with loose bricks and cement. The whole has gradually consolidated into a mass of great firmness.

The reticulated walls of the Romans, having bricks with oblique surfaces, would, at the present day, be thought highly unphilosophical. Indeed, they could not long have stood, had it not been for the great strength of their cement. Modern brick walls are laid with great precision, and depend for firmness more upon their position than upon the strength of their cement. The bricks being laid in horizontal courses, and continually overlaying each other, or breaking joints, the whole mass is strongly interwoven, and bound together. Wooden walls, composed of timbers covered with boards, are a common, but more perishable kind. They require to be constantly covered with a coating of a foreign substance, as paint or plaster, to preserve them from spontaneous decomposition. In some parts of France, and elsewhere, a kind of wall is made of earth, rendered compact by ramming it in moulds or cases. This method is called building in pisé, and is much more durable than the nature of the material would lead us to suppose. Walls of all kinds are greatly strengthened by angles and curves, also by projections, such as pilasters, chimneys and buttresses. These projections serve to increase the breadth of the foundation, and are always to be made use of in large buildings, and in walls of considerable length.

224.—The LINTEL, or *beam*, extends in a right line over a vacant space, from one column or wall to another. The strength of the lintel will be greater in proportion as its transverse vertical diameter exceeds the horizontal, the strength being always as the square of the depth. The *floor* is the lateral continuation or connection of beams by means of a covering of boards.

225.—The ARCH is a transverse member of a building, answering the same purpose as the lintel, but vastly exceeding it in strength. The arch, unlike the lintel, may consist of any number of constituent pieces, without impairing its strength. It is, however, necessary that all the pieces should possess a uniform shape,---the shape of a portion of a wedge_--and that the joints, formed by the contact of their surfaces, should point towards a common centre. In this case, no one portion of the arch can be displaced or forced inward; and the arch cannot be broken by any force which is not sufficient to crush the materials of which it is made. In arches made of common bricks, the sides of which are parallel, any one of the bricks might be forced inward, were it not for the adhesion of the cement. Any two of the bricks, however, by the disposition of their mortar, cannot collectively be forced inward. An arch of the proper form, when complete, is rendered stronger, instead of weaker, by the pressure of a considerable weight, provided this pressure be uniform. While building, however, it requires to be supported by a centring of the shape of its internal surface, until it is complete. The upper stone of an arch is called the key-stone, but is not more essential than any other. In regard to the shape of the arch, its most simple form is that of the semi-circle. It is, however, very frequently a smaller arc of a circle, and, still more frequently, a portion of an ellipse. The simplest theory of an arch supporting itself only, is that of Dr. Hooke. The arch, when it has only its own weight to bear, may be considered as the inversion of a chain, suspended at each end. The chain hangs in such a form, that the weight of each link or portion is held in equilibrium by

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the result of two forces acting at its extremities; and these forces, or tensions, are produced, the one by the weight of the portion of the chain below the link, the other by the same weight increased by that of the link itself, both of them acting originally in a vertical direction. Now, supposing the chain inverted, so as to constitute an arch of the same form and weight, the relative situations of the forces will be the same, only they will act in contrary directions, so that they are compounded in a similar manner, and balance each other on the same conditions.

The arch thus formed is denominated a catenary arch. In common cases, it differs but little from a circular arch of the extent of about one third of a whole circle, and rising from the abutments with an obliquity of about 30 degrees from a perpendicu-But though the catenary arch is the best form for supportlar. ing its own weight, and also all additional weight which presses in a vertical direction, it is not the best form to resist lateral pressure, or pressure like that of fluids, acting equally in all direc-Thus the arches of bridges and similar structures, when tions. covered with loose stones and earth, are pressed sideways, as well as vertically, in the same manner as if they supported a weight of fluid. In this case, it is necessary that the arch should arise more perpendicularly from the abutment, and that its general figure should be that of the longitudinal segment of an ellipse. In small arches, in common buildings, where the disturbing force is not great, it is of little consequence what is the shape of the curve. The outlines may even be perfectly straight, as in the tier of bricks which we frequently see over a window. This is, strictly speaking, a real arch, provided the surfaces of the bricks tend towards a common centre. It is the weakest kind of arch, and a part of it is necessarily superfluous, since no greater portion can act in supporting a weight above it, than can be included between two curved or arched lines.

Besides the arches already mentioned, various others are in use. The *acute* or *lancet* arch, much used in Gothic architecture, is

described usually from two centres outside the arch. It is a strong arch for supporting vertical pressure. The rampant arch is one in which the two ends spring from unequal heights. The horse-shoe or Moorish arch is described from one or more centres placed above the base line. In this arch, the lower parts are in danger of being forced inward. The ogee arch is concavo-convex, and therefore fit only for ornament. In describing arches, the upper surface is called the extrados, and the inner, the intrados. The springing lines are those where the intrados meets the abutments, or supporting walls. The span is the distance from one springing line to the other. The wedge-shaped stones, which form an arch, are sometimes called *voussoirs*, the uppermost being the key-stone. The part of a pier from which an arch springs is called the *impost*, and the curve formed by the upper side of the voussoirs, the archivolt. It is necessary that the walls, abutments and piers, on which arches are supported, should be so firm as to resist the lateral thrust, as well as vertical pressure, of the arch. It will at once be seen, that the lateral or sideway pressure of an arch is very considerable, when we recollect that every stone, or portion of the arch, is a wedge, a part of whose force acts to separate the abutments. For want of attention to this circumstance, important mistakes have been committed, the strength of buildings materially impaired, and their ruin accelerated. In some cases, the want of lateral firmness in the walls is compensated by a bar of iron stretched across the span of the arch, and connecting the abutments, like the tie-beam of a roof. This is the case in the cathedral of Milan and some other Gothic buildings.

In an arcade, or continuation of arches, it is only necessary that the outer supports of the terminal arches should be strong enough to resist horizontal pressure. In the intermediate arches, the lateral force of each arch is counteracted by the opposing lateral force of the one contiguous to it. In bridges, however, where individual arches are liable to be destroyed by accident, it is desi-

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rable that each of the piers should possess sufficient horizontal strength to resist the lateral pressure of the adjoining arches.

226.—The VAULT is the lateral continuation of an arch, serving to cover an area or passage, and bearing the same relation to the arch that the wall does to the column. A simple vault is constructed on the principles of the arch, and distributes its pressure equally along the walls or abutments. A complex or groined vault is made by two vaults intersecting each other, in which case the pressure is thrown upon springing points, and is greatly increased at those points. The groined vault is common in Gothic architecture.

227.—The Dome, sometimes called cupola, is a concave covering to a building, or part of it, and may be either a segment of a sphere, of a spheroid, or of any similar figure. When built of stone, it is a very strong kind of structure, even more so than the arch, since the tendency of each part to fall is counteracted, not only by those above and below it, but also by those on each side. It is only necessary that the constituent pieces should have a common form, and that this form should be somewhat like the frustum of a pyramid, so that, when placed in its situation, its four angles may point toward the centre, or axis, of the dome. During the erection of a dome, it is not necessary that it should be supported by a centring, until complete, as is done in the arch. Each circle of stones, when laid, is capable of supporting itself without aid from those above it. It follows that the dome may be left open at top, without a key-stone, and yet be perfectly secure in this respect, being the reverse of the arch. The dome of the Pantheon, at Rome, has been always open at top, and yet has stood unimpaired for nearly 2000 years. The upper circle of stones, though apparently the weakest, is nevertheless often made to support the additional weight of a lantern or tower above it. In several of the largest cathedrals, there are two domes, one within the other, which contribute their joint support to the lantern, which rests upon the top. In these buildings, the dome

rests upon a circular wall, which is supported, in its turn, by arches upon massive pillars or piers. This construction is called building upon pendentives, and gives open space and room for passage beneath the dome. The remarks which have been made in regard to the abutments of the arch, apply equally to the walls immediately supporting a dome. They must be of sufficient thickness and solidity to resist the lateral pressure of the dome, which is very great. The walls of the Roman Pantheon are of great depth and solidity. In order that a dome in itself should be perfectly secure, its lower parts must not be too nearly vertical, since, in this case, they partake of the nature of perpendicular walls, and are acted upon by the spreading force of the parts above them. The dome of St. Paul's church, in London, and some others of similar construction, are bound with chains or hoops of iron, to prevent them from spreading at bottom. Domes which are made of wood depend, in part, for their strength, on their internal carpentry. The Halle du Bled, in Paris, had originally a wooden dome more than 200 feet in diameter, and only one foot in thickness. This has since been replaced by a dome of iron. (See Art. 303.)

228.—The Roof is the most common and cheap method of covering buildings, to protect them from rain and other effects of the weather. It is sometimes flat, but more frequently oblique, in its shape. The flat or platform-roof is the least advantageous for shedding rain, and is seldom used in northern countries. The pent roof, consisting of two oblique sides meeting at top, is the most common form. These roofs are made steepest in cold climates, where they are liable to be loaded with snow. Where the four sides of the roof are all oblique, it is denominated a hipped roof, and where there are two portions to the roof, of different obliquity, it is a curb, or mansard roof. In modern times, roofs are made almost exclusively of wood, though frequently covered with incombustible materials. The internal structure or carpentry of roofs is a subject of considerable mechanical contrivance.

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The roof is supported by rafters, which abut on the walls on each side, like the extremities of an arch. If no other timbers existed, except the rafters, they would exert a strong lateral pressure on the walls, tending to separate and overthrow them. To counteract this lateral force, a tie-beam, as it is called, extends across, receiving the ends of the rafters, and protecting the wall from their horizontal thrust. To prevent the tie-beam from sagging, or bending downward with its own weight, a kingpost is erected from this beam, to the upper angle of the rafters, serving to connect the whole, and to suspend the weight of the beam. This is called *trussing*. Queen-posts are sometimes added, parallel to the king-post, in large roofs; also various other connecting timbers. In Gothic buildings, where the vaults do not admit of the use of a tie-beam, the rafters are prevented from spreading, as in an arch, by the strength of the buttresses.

In comparing the lateral pressure of a high roof with that of a low one, the length of the tie-beam being the same, it will be seen that a high roof, from its containing most materials, may produce the greatest pressure, as far as weight is concerned. On the other hand, if the weight of both be equal, then the low roof will exert the greater pressure; and this will increase in proportion to the distance of the point at which perpendiculars, drawn from the end of each rafter, would meet. In roofs, as well as in wooden domes and bridges, the materials are subjected to an internal strain, to resist which, the cohesive strength of the material is relied on. On this account, beams should, when possible, be of one piece. Where this cannot be effected, two or more beams are connected together by splicing. Spliced beams are never so strong as whole ones, yet they may be made to approach the same strength, by affixing lateral pieces, or by making the ends overlay each other, and connecting them with bolts and straps of iron. The tendency to separate is also resisted, by letting the two pieces into each other by the process called scarfing. Mortices, in-

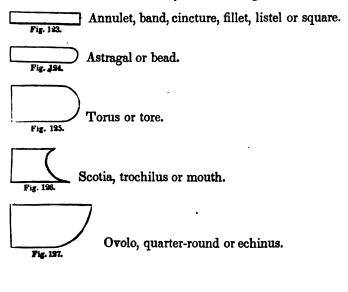
tended to *truss* or suspend one piece by another, should be formed upon similar principles.

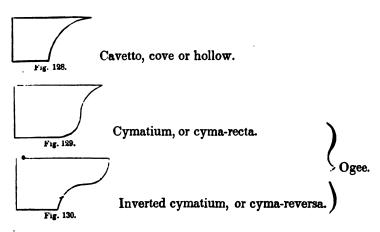
Roofs in the United States, after being boarded, receive a secondary covering of shingles. When intended to be incombustible, they are covered with slates or earthern tiles, or with sheets of lead, copper or tinned iron. Slates are preferable to tiles, being lighter, and absorbing less moisture. Metallic sheets are chiefly used for flat roofs, wooden domes, and curved and angular surfaces, which require a flexible material to cover them, or have not a sufficient pitch to shed the rain from slates or shingles. Various artificial compositions are occasionally used to cover roofs, the most common of which are mixtures of tar with lime, and sometimes with sand and gravel."—*Ency. Am.* (See *Art.* 285.)

SECTION III.-MOULDINGS, CORNICES, &c.

MOULDINGS.

229.—A moulding is so called, because of its being of the same determinate shape along its whole length, as though the whole of it had been cast in the same mould or form. The regular mouldings, as found in remains of ancient architecture, are eight in number; and are known by the following names:





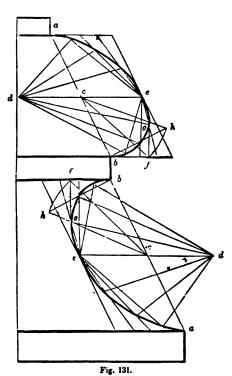
Some of the terms are derived thus: fillet, from the French word *fil*, thread. Astragal, from *astragalos*, a bone of the heel —or the curvature of the heel. Bead, because this moulding, when properly carved, resembles a string of beads. Torus, or tore, the Greek for *rope*, which it resembles, when on the base of a column. Scotia, from *shotia*, darkness, because of the strong shadow which its depth produces, and which is increased by the projection of the torus above it. Ovolo, from *ovum*, an egg, which this member resembles, when carved, as in the Ionic capital. Cavetto, from *cavus*, hollow. Cymatium, from *kumaton*, a wave.

230.—Neither of these mouldings is peculiar to any one of the orders of architecture, but each one is common to all; and although each has its appropriate use, yet it is by no means confined to any certain position in an assemblage of mouldings. The use of the fillet is to bind the parts, as also that of the astragal and torus, which resemble ropes. The ovolo and cyma-reversa are strong at their upper extremities, and are therefore used to support projecting parts above them. The cyma-recta and cavetto, being weak at their upper extremities, are not used as supporters, but are placed uppermost to cover and shelter the other parts. The scotia is introduced in the base of a column, to separate the upper and lower torus, and to produce a pleasing variety and relief. The form of the bead, and that of the torus, is the same; the reasons for giving distinct names to them are, that the torus, in every order, is always considerably larger than the bead, and is placed among the base mouldings, whereas the bead is never placed there, but on the capital or entablature; the torus, also, is never carved, whereas the bead is; and while the torus among the Greeks is frequently elliptical in its form, the bead retains its circular shape. While the scotia is the reverse of the torus, the cavetto is the reverse of the ovolo, and the cymarecta and cyma-reversa are combinations of the ovolo and cavetto.

231.—The curves of mouldings, in Roman architecture, were most generally composed of parts of circles; while those of the Greeks were almost always elliptical, or of some one of the conic sections, but rarely circular, except in the case of the bead, which was always, among both Greeks and Romans, of the form of a semi-circle. Sections of the cone afford a greater variety of forms than those of the sphere; and perhaps this is one reason why the Grecian architecture so much excels the Roman. The quick turnings of the ovolo and cyma-reversa, in particular, when exposed to a bright sun, cause those narrow, well-defined streaks of light, which give life and splendour to the whole.

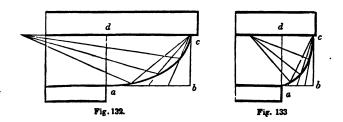
232.—A profile is an assemblage of essential parts and mouldings. That profile produces the happiest effect which is composed of but few members, varied in form and size, and arranged so that the plane and the curved surfaces succeed each other alternately.

233.—To describe the Grecian torus and scotia. Join the extremities, a and b, (Fig. 131;) and from f, the given projection of the moulding, draw f o, at right angles to the fillets; from b, draw b h, at right angles to a b; bisect a b in c; join f and c, and upon c, with the radius, c f, describe the arc, f h, cutting b h in h; through c, draw d e, parallel with the fillets; make d c and c s, each equal to b h; then d e and a b will be conjugate diame-

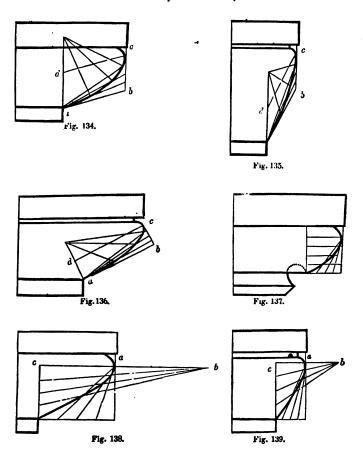


ters of the required ellipse. To describe the curve by intersection of lines, proceed as directed at Art. 118 and note; by a trammel, see Art. 125; and to find the foci, in order to describe it

with a string, see Art. 115.

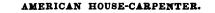


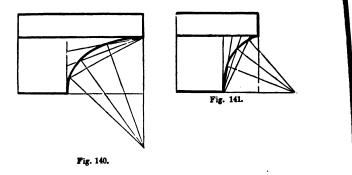
234.—Fig. 132 to 139 exhibit various modifications of the Grecian ovolo, sometimes called echinus. Fig. 132 to 136 are



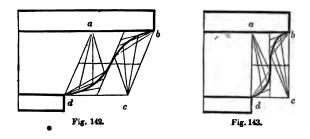
elliptical, a b and b c being given tangents to the curve; parallel to which, the semi-conjugate diameters, a d and d c, are drawn. In Fig. 132 and 133, the lines, a d and d c, are semi-axes, the tangents, a b and b c, being at right angles to each other. To draw the curve, see Art. 118. In Fig. 137, the curve is parabolical, and is drawn according to Art. 127. In Fig. 138 and 139, the curve is hyperbolical, being described according to Art. 128. The length of the transverse axis, a b, being taken at pleasure, in order to flatten the curve, a b should be made short in proportion to a c.

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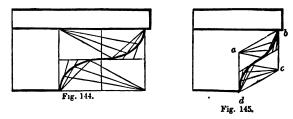




235.— To describe the Grecian cavetto, (Fig. 140 and 141,) having the height and projection given, see Art. 118.



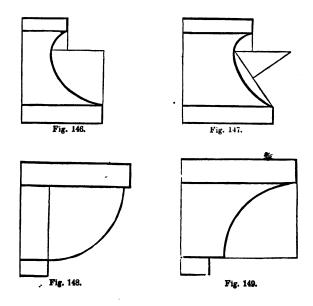
236.— To describe the Grecian cyma-recta. When the projection is more than the height, as at Fig. 142, make $a \ b$ equal to the height, and divide $a \ b \ c \ d$ into 4 equal parallelograms; then proceed as directed in note to Art. 118. When the projection is less than the height, draw $d \ a$, (Fig. 143,) at right angles to $a \ b$; complete the rectangle, $a \ b \ c \ d$; divide this into 4 equal rectangles, and proceed according to Art. 118.



237.—To describe the Grecian cyma-reversa. When the

projection is more than the height, as at Fig. 144, proceed as directed for the last figure; the curve being the same as that, the position only being changed. When the projection is less than the height, draw a d, (Fig. 145,) at right angles to the fillet; make a d equal to the projection of the moulding: then proceed as directed for Fig. 142.

238.—Roman mouldings are composed of parts of circles, and have, therefore, less beauty of form than the Grecian. The bead and torus are of the form of the semi-circle, and the scotia, also, in some instances; but the latter is often composed of two quadrants, having different radii, as at Fig. 146 and 147, which resemble the elliptical curve. The ovolo and cavetto are generally a quadrant, but often less. When they are less, as at Fig. 150, the centre is found thus: join the extremities, a and b, and bisect a b in c; from c, and at right angles to a b, draw c d, cutting a level line drawn from a in d; then d will be the centre. This moulding projects less than its height. When the projection is more than the height, as at Fig. 152, extend the line from c until



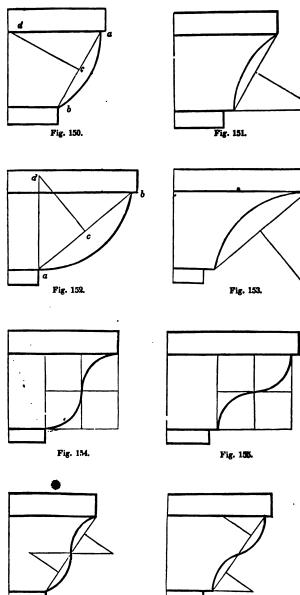
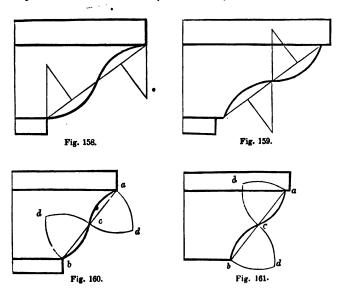


Fig. 157.

Fig. 156.

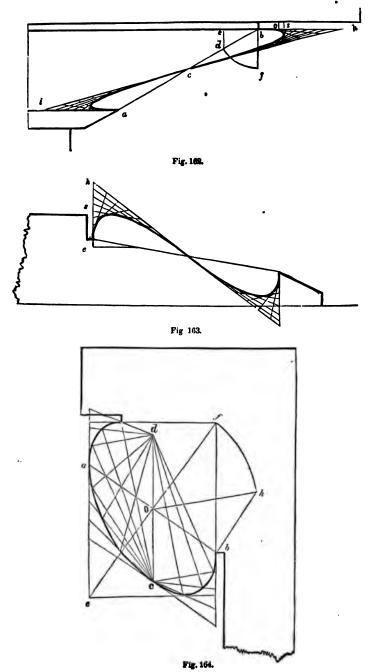
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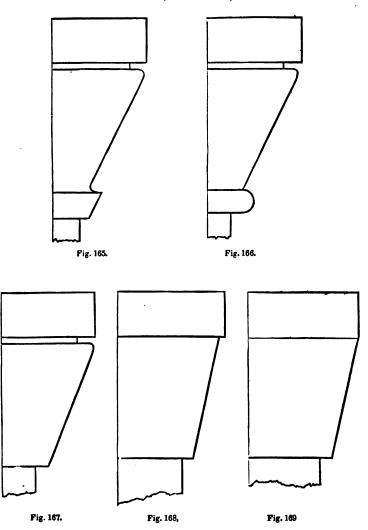


it cuts a perpendicular drawn from a, as at d; and that will be the centre of the curve. In a similar manner, the centres are found for the mouldings at *Fig.* 147, 151, 153, 156, 157, 158 and 159. The centres for the curves at *Fig.* 160 and 161, are found thus: bisect the line, a b, at c; upon a, c and b, successively, with a c or c b for radius, describe arcs intersecting at d and d; then those intersections will be the centres.

239.—Fig. 162 to 169 represent mouldings of modern invention. They have been quite extensively and successfully used in inside finishing. Fig. 162 is appropriate for a bed-moulding under a low, projecting shelf, and is frequently used under mantle-shelves. The tangent, i h, is found thus: bisect the line, a b, at c_i and b c at d; from d, draw d e, at right angles to e b; from b, draw b f; parallel to e d; upon b, with b d for radius, describe the arc, d f; divide this arc into 7 equal parts, and set one of the parts from s, the limit of the projection, to o; make o h equal to o e; from h, through c, draw the tangent, h i; divide b h, h c, c iand i a, each into a like number of equal parts, and draw the in-

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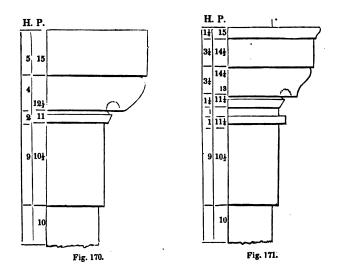




tersecting lines as directed at Art. 89. If a bolder form is desired, draw the tangent, *i h*, nearer horizontal, and describe an elliptic curve as shown in *Fig.* 131, 164, 175 and 176. *Fig.* 163 is much used on base, or skirting of rooms, and in deep panelling. The curve is found in the same manner as that of *Fig.* 162. In this case, however, where the moulding has so little projection

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in comparison with its height, the point, e, being found as in the last figure, $h \ s$ may be made equal to $s \ e$, instead of $o \ e$ as in the last figure. Fig. 164 is appropriate for a crown moulding of a cornice. In this figure the height and projection are given; the direction of the diameter, $a \ b$, drawn through the middle of the diagonal, $e \ f$, is taken at pleasure; and $d \ c$ is parallel to $a \ e$. To find the length of $d \ c$, draw $b \ h$, at right angles to $a \ b$; upon o, with $o \ f$ for radius, describe the arc, $f \ h$, cutting $b \ h$ in h; then make $o \ c$ and $o \ d$, each equal to $b \ h$.*. To draw the curve, see note to Art. 118. Fig. 165 to 169 are peculiarly distinct from ancient mouldings, being composed principally of straight lines; the few curves they possess are quite short and quick.

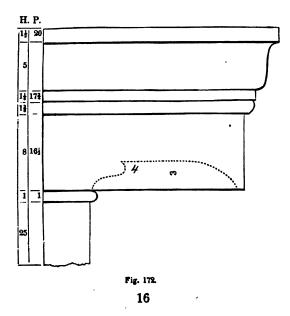


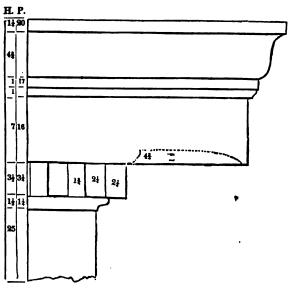
240.-Fig. 170 and 171 are designs for antæ caps. The

* The manner of ascertaining the length of the conjugate diameter, dc, in this figure, and also in Fig. 131, 175 and 176, is new, and is important in this application. It is founded upon well-known mathematical principles, viz: All the parallelograms that may be circumscribed about an ellipsis are equal to one another, and consequently any one is equal to the rectangle of the two axes. And again : the sum of the squares of every pair of conjugate diameters is equal to the sum of the squares of the two axes. diameter of the antæ is divided into 20 equal parts, and the height and projection of the members, are regulated in accordance with those parts, as denoted under H and P, height and projection. The projection is measured from the middle of the antæ. These will be found appropriate for porticos, door-ways, mantle-pieces, door and window trimmings, &c. The height of the antæ for mantle-pieces, should be from 5 to 6 diameters, having an entablature of from 2 to 24 diameters. This is a good proportion, it being similar to the Doric order. But for a portico these proportions are much too heavy; an antæ, 15 diameters high, and an entablature of 3 diameters, will have a better appearance.

CORNICES.

241.—Fig. 172, 173 and 174, are designs for eave cornices, and Fig. 175 and 176, for stucco cornices for the inside finish of rooms. The projection of the uppermost member from the facia, is divided into 20 equal parts, and the various members are proportioned according to those parts, as figured under H and P.







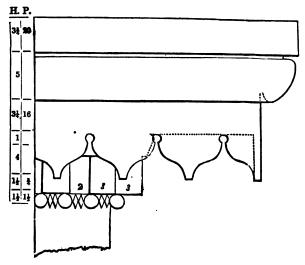
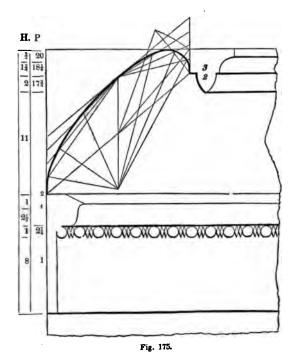


Fig. 174

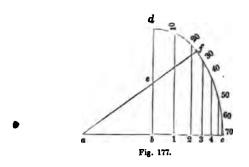
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H. P. 84 |20 14 |10 7 14 |22 64 |1 1

Fig. 176.

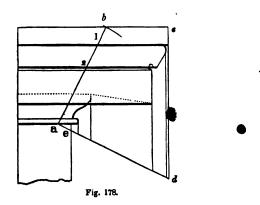
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242.— To proportion an eave cornice in accordance with the height of the building. Draw the line, a c, (Fig. 177,) and make b c and b a, each equal to 18 inches; from b, draw b d, at right angles to a c, and equal in length to $\frac{2}{3}$ of a c; bisect b d in e, and from a, through e, draw a f; upon a, with a c for radius, describe the arc, c f, and upon e, with e f for radius, describe the arc, f d; divide the curve, df c, into 7 equal parts, as at 10, 20, 30, &c., and from these points of division, draw lines to b c, parallel to d b; then the distance, b 1, is the projection of a cornice for a building 10 feet high; b 2, the projection at 20 feet high; b 3, the projection at 30 feet, &c. If the projection of a cornice for a building 34 feet high, is required, divide the arc between 30 and 40 into 10 equal parts, and from the fourth point from 30, draw a line to the base, b c, parallel with b d; then the distance of the point, at which that line cuts the base, from b, will be the projection required. So proceed for a cornice of any height within 70 feet. The above is based on the supposition that 18 inches is the proper projection for a cornice 70 feet high. This, for general purposes, will be found correct; still, the length of the line, b c, may be varied to suit the judgment of those who think differently.

Having obtained the projection of a cornice, divide it into 20 equal parts, and apportion the several members according to its destination—as is shown at Fig. 172, 173 and 174.

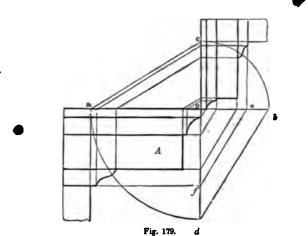
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243.-- To proportion a cornice according to a smaller given one. Let the cornice at Fig. 178 be the given one. Upon any point in the lowest line of the lowest member, as at a, with the height of the required cornice for radius, describe an intersecting arc across the uppermost line, as at b; join a and b; then b 1 will be the perpendicular height of the upper fillet for the proposed cornice, 1 2 the height of the crown moulding—and so of all the members requiring to be enlarged to the sizes indicated on this line. For the projection of the proposed cornice, draw a d, at right angles to a b, and c d, at right angles to b c; parallel with c d, draw lines from each projection of the given cornice to the line, a d; then e d will be the required projection for the proposed cornice, and the perpendicular lines falling upon e d will indicate the proper projection for the members.

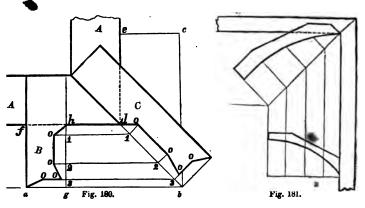
244.—To proportion a cornice according to a larger given one. Let A, (Fig. 179,) be the given cornice. Extend $a \ o \ to \ b$, and draw $c \ d$, at right angles to $a \ b$; extend the horizontal lines of the cornice, A, until they touch $o \ d$; place the height of the proposed cornice from o to e, and join f and e; upon o, with the projection of the given cornice, $o \ a$, for radius, describe the quadrant, $a \ d$; from d, draw $d \ b$, parallel to $f \ e$; upon o, with $o \ b$ for radius, describe the quadrant, $b \ c$; then $o \ c$ will be the proper projection for the proposed cornice. Join $a \ and \ c$; draw lines from the

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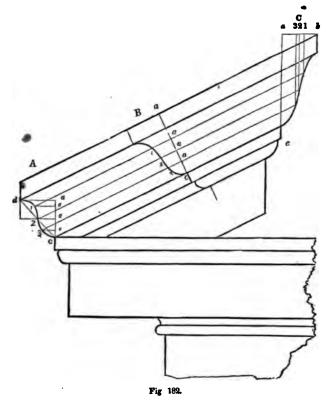
projection of the different members of the given cornice to a o, parallel to od; from these divisions on the line, a o, draw lines to the line, o c, parallel to a c; from the divisions on the line, o f, draw lines to the line, o e, parallel to the line, f e; then the divisions on the lines, o e and o c, will indicate the proper height and projection for the different members of the proposed cornice. In this process, we have assumed the height, o e, of the proposed cornice to be given; but if the projection, o c, alone be given, we can obtain the same result by a different process. Thus: upon o. with o c for radius, describe the quadrant, c b; upon o, with o afor radius, describe the quadrant, a d; join d and b; from f, draw f e, parallel to d b; then o e will be the proper height for the proposed cornice, and the height and projection of the different members can be obtained by the above directions. By this problem, a cornice can be proportioned according to a smaller given one as well as to a larger ; but the method described in the previous article is much more simple for that purpose.

245.—To find the angle-bracket for a cornice. Let A, (Fig. 180,) be the wall of the building, and B the given bracket, which, for the present purpose, is turned down horizontally. The angle-bracket, C, is obtained thus: through the extremity, a, and paral-



with the wall, f d, draw the line, a b; make e c equal a f, 1 through c, draw c b, parallel with e d; join d and b, and from several angular points in B, draw ordinates to cut d b in 1, 2 1 3; at those points erect lines perpendicular to d b; from h, w h g, parallel to f a; take the ordinates, 1 o, 2 o, &c., at B, 1 transfer them to C, and the angle-bracket, C, will be defined. the same manner, the angle-bracket for an internal cornice, or angle-rib of a coved ceiling, or of groins, as at Fig. 181, can jound.

246.—A level crown moulding being given, to find the raking ulding and a level return at the top. Let A, (Fig. 182,) be given moulding, and A b the rake of the roof. Divide the ve of the given moulding into any number of parts, equal or squal, as at 1, 2, and 3; from these points, draw horizontal s to a perpendicular erected from c; at any convenient place the rake, as at B, draw a c, at right angles to A b; also, from lraw the horizontal line, b a; place the thickness, d a, of the ulding at A, from b to a, and from a, draw the perpendicular , a e; from the points, 1, 2, 3, at A, draw lines to C, parallel 4 b; make a 1, a 2 and a 3, at B and at C, equal to a 1, &c., 1; through the points, 1, 2 and 3, at B, trace the curve—this 1 be the proper form for the raking moulding. From 1, 2 and



3, at C, drop perpendiculars to the corresponding ordinates fr 1, 2 and 3, at A; through the points of intersection, trace curve—this will be the proper form for the *return* at the top.

SECTION IV.—FRAMING.

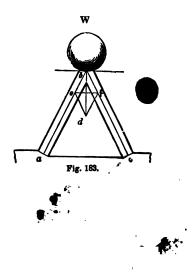
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247.-This subject is, to the carpenter, of the highest impor-Ance; and deserves more attention and a larger place in a volume this kind, than is generally allotted to it. Something, indeed, as been said upon the geometrical principles, by which the seve-Al lines for the joints and the lengths of timber, may be ascerined; yet, besides this, there is much to be learned. For how-•ver precise or workmanlike the joints may be made, what will t avail, should the system of framing, from an erroneous position If its timbers, &c., change its form, or become incapable of susaining even its own weight? Hence the necessity for a knowedge of the laws of pressure and the strength of timber. These being once understood, we can with confidence determine the best position and dimensions for the several timbers which compose a loor or a roof, a partition or a bridge. As systems of framing re more or less exposed to heavy weights and strains, and, in case of failure, cause not only a loss of labour and material, but frequently that of the itself, it is very important that the materials employed be of the proper quantity and quality to serve their destination. And, on the other hand, any superfluous material is not only useless, but a positive injury, it being an unnecessary load upon the points of support. It is necessary, therefore, to know

the *least* quantity of timber that will suffice for strength. The greatest fault in framing is that of using an excess of material. Economy, at least, would seem to require that this evil be abated.

Before proceeding to consider the principles upon which a system of framing should be constructed, let us attend to a few of the elementary laws in *Mechanics*, which will be found to be of great value in determining those principles.

248.—LAWS OF PRESSURE. (1.) A heavy body always exerts a pressure equal to its own weight in a vertical direction. Example: Suppose an iron ball, weighing 100 lbs., be supported upon the top of a perpendicular post, (Fig. 196;) then the pressure exerted upon that post will be equal to the weight of the ball; viz., 100 lbs. (2.) But if two inclined posts, (Fig. 183,) be substituted for the perpendicular support, the united pressures upon these posts will be more than equal to the weight, and will be in proportion to their position. The farther apart their feet are spread the greater will be the pressure, and vice versa. Hence tremendous strains may be exerted by a comparatively small weight. And it follows, therefore, that a piece of timber intended for a strut or post, should be so placed that its axis may coincide, as near as possible, with the direction of the pressure. The direction of the pressure of the weight, W, (Fig. 183,) is in the vertical line, b d; and the weight, W, would fall in that line, if the two posts were removed, hence the best position for a support



for the weight would be in that line. But, as it rarely occurs in systems of framing that weights can be supported by any single resistance, they requiring generally two or more supports, (as in the case of a roof supported by its rafters,) it becomes important, therefore, to know the exact amount of pressure any certain weight is capable of exerting upon oblique supports. This can be ascertained by the following process.

Let a b and b c, (Fig. 183,) represent the axes of two sticks of timber supporting the weight, W; and let the weight, W, be equal to 6 tons. Make the vertical line, b d, equal to 6 inches; from d, draw df, parallel to ab, and de, parallel to cb; then the line, b e, will be found to be $3\frac{1}{2}$ inches long, which is equal to the number of tons that the weight, W, exerts upon the post, a b. The pressure upon the other post is represented by b f, which in this case is of the same length as b e. The posts being inclined at equal angles to the vertical line, b d, the pressure upon them is equal. Thus it will be found that the weight, which weighs only 6 tons, exerts a pressure of 7 tons; the amount being increased because of the oblique position of the supports. The lines, e b, b f, f d and d e, compose what is called the parallelogram of forces. The oblique strains exerted by any one force, therefore, may always be ascertained, by making b d equal, (upon any scale of equal parts,) to the number of lbs., cwts., or tons contained in the weight, W, and b e will then represent the number of lbs., cwts., or tons with which the timber, a b, is pressed, and b f that exerted upon b c.

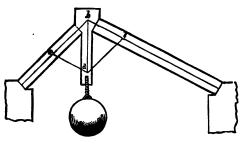
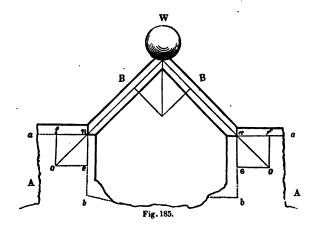


Fig. 184

Correct ideas of the comparative pressure exerted upon timbers according to their position, will be readily formed by drawing various designs of framing, and estimating the several strains in accordance with these principles. In Fig. 184, the struts are framed into a third piece, and the weight suspended from that. The struts are placed at a different angle to show the diverse pressures. The *length* of the timber used as struts, does not alter the amount of the pressure. But it may be observed that long timbers are not so capable of resistance as short ones.

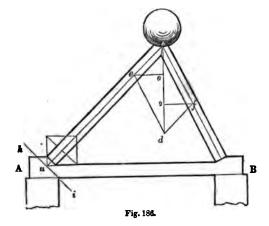


249.—In Fig. 185, the weight, W, exerts a pressure on the struts in the direction of their length; their feet, n, n, have, therefore, a tendency to move in the direction, n o, and would so move, were they not opposed by a sufficient resistance from the blocks, A and A. If a piece of each block be cut off at the horizontal line, a n, the feet of the struts would slide away from each other along that line, in the direction, n a; but if, instead of these, two pieces were cut off at the vertical line, n b, then the struts would descend vertically. To estimate the horizontal and the vertical pressures exerted by the struts, let n o be made equal (upon any scale of equal parts) to the number of tons (or pounds) with which the strut is pressed; construct the parallelogram of forces

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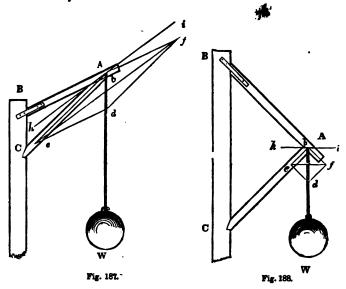
by drawing e e parallel to a n, and o f parallel to b n; then n f, (by the same scale,) shows the number of tons (or pounds) pressure that is exerted by the strut in the direction, n a, and n eshows the amount exerted in the direction, n b. By constructing designs similar to this, giving various and dissimilar positions to the struts, and then estimating the pressures, it will be found in every case that the horizontal pressure of one strut is exactly equal to that of the other, however much one strut may be inclined more than the other; and also, that the united vertical pressure of the two struts is exactly equal to the weight, W. (In this calculation, the weight of the timbers is not taken into consideration.)

250.—Suppose that the two struts, B and B, (Fig. 185,) were rafters of a roof, and that instead of the blocks, A and A, the walls of a building were the supports : then, to prevent the walls from being thrown over by the thrust of B and B, it would be desirable to remove the horizontal pressure. This may be done by uniting the feet of the rafters with a rope, iron rod, or piece of timber, as in Fig. 186. This figure is similar to the truss of a roof.



The horizontal strains on the tie-beam, tending to pull it asunder in the direction of its length, may be measured at the foot of the

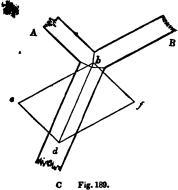
rafter, as was shown at Fig. 185; but it can be more readily and as accurately measured, by drawing from f and e horizontal lines to the vertical line, b d, meeting it in o and o; then f o will be the horizontal thrust at B, and e o at A; these will be found to equal one another. When the rafters of a roof are thus connected, all tendency to thrust the walls horizontally is removed, the only pressure on them is in a vertical direction, being equal to the weight of the roof and whatever it has to support. This pressure is beneficial rather than otherwise, as a roof thus formed tends to steady the walls.



251.—Fig. 187 and 188 exhibit methods of framing for supporting the equal weights, W and W. Suppose it be required to measure and compare the strains produced on the pieces, AB and AC. Construct the parallelogram of forces, $e \ b \ f \ d$, according to Art. 248. Then $b \ f$ will show the strain on AB, and $b \ e$ the strain on AC. By comparing the figures, $b \ d$ being equal in each, it will be seen that the strains in Fig. 187 are about three

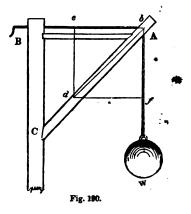
times as great as those in *Fig.* 188: the position of the pieces, *A B* and *A C*, in *Fig.* 188, is therefore far preferable.

This and the preceding examples exemplify, in a measure, the resolution of forces; viz., the finding of two or more forces, which, acting in differ the directions, shall exactly balance the pressure of any given single force. Thus, in Fig. 185, supposing the weight, W, to be the greatest force that the two timbers, in their present position, are capable of sustaining, then the weight, W, is the given force, and the timbers are the two forces just equal to the given force.



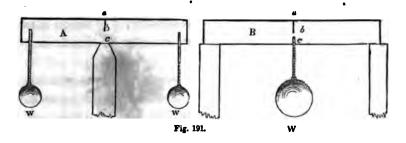
252.—The composition of forces consists in ascertaining the direction and amount of one force, which shall be just capable of balancing two or more given forces, acting in different directions. This is only the reverse of the resolution of forces, and the two are founded on one and the same principle, and may be solved in the same manner. For example; let A and B, (Fig. 189,) be two pieces of timber, pressed in the direction of their length towards b—A by a force equal to 6 tons weight, and B equal to 9. To find the direction and amount of pressure they would unitedly exert, draw the lines, b e and b f, in a line with the axes of the timbers, and make b e equal to the pressure exerted by B, viz., 9; also make b f equal to the pressure on A, viz., 6, and complete the parallelogram of forces, e b f d; then b d, the diagonal of the

parallelogram, will be the *direction*, and its length will be the *amount*, of the united pressures of A and of B. The line, b d, is termed the *resultant* of the two forces, b f and be. If A and B are to be supported by one post, C, the best position **that** post will be in the direction of the diagonal, b d; and **instant** require to be sufficiently strong to support the united pressures of A and of B.



253.—Another example: let Fig. 190 represent a piece of framing commonly called a crane, which is used for hoisting heavy weights by means of the rope, B b f, which passes over a pulley at b. This is similar to Fig. 187 and 188, yet it is materially different. In those figures, the strain is in one direction only, viz., from b to d, but in this there are two strains, from A to B and from A to \overline{W} . The strain in the direction, A B, is evidently equal to that in the direction, A W. To ascertain the best position for the strut, A C, make b e equal to b f, and complete the parallelogram of forces, $e \ b \ f \ d$; then draw the diagonal, $b \ d$, and it will be the position required. Should the foot, C, of the strut be placed either higher or lower, the strain on A C would be increased. In constructing cranes, it is advisable, in order that the piece, B A, may be under a gentle pressure, to place the foot of the strut a trifle lower than where the diagonal, b d, would indicate, but never higher

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254.—*Ties and Struts.* Timbers in a state of tension are called *ties*, while such as are in a state of compression are termed *struts.* This subject can be illustrated in the following manner.

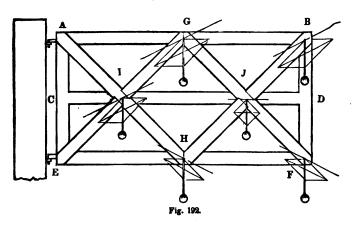
Let A and B, (Fig. 191,) represent beams of timber supporting the weights, W, W and W; A having but one support, which is in the middle of its length, and B two, one at each end. To show the nature of the strains, let each beam be sawed in the middle from a to b. The effects are obvious: the cut in the beam, A, will open, whereas that in B will close. If the weights are heavy enough, the beam, A, will break at b; while the cut in B will be closed perfectly tight at a, and the beam be very little injured by it. But if, on the other hand, the cuts be made in the bottom edge of the timbers, from c to b, B will be seriously injured, while A will scarcely be affected. By this it appears evident that, in a piece of timber subject to a pressure across the direction of its length, the fibres are exposed to contrary strains. If the timber is supported at both ends, as at B, those from the top edge down to the middle are compressed in the direction of their length, while those from the middle to the bottom edge are in a state of tension; but if the beam is supported as at A, the contrary effect is produced; while the fibres at the middle of either beam are not at all strained. The strains in a framed truss are of the same nature as those in a single beam. The truss for a roof, being supported at each end, has its tie-beam in a state of tension, while its rafters are compressed in the direction of their length. By this, it appears highly important that pieces in a state of tension should be distinguished

from such as are compressed, in order that the former may be preserved continuous. A strut may be constructed of two or more pieces; yet, where there are many joints, it will not resist compression so firmly.

255.—To distinguish ties from struts. This may be done by the following rule. In Fig. 183, the timbers, a b and b c, are the sustaining forces, and the weight, W, is the straining force; and, if the support be removed, the straining force would move from the point of support, b, towards d. Let it be required to ascertain whether the sustaining forces are stretched or pressed by the straining force. Rule: upon the direction of the straining force, b d, as a diagonal, construct a parallelogram, e b f d, whose sides shall be parallel with the direction of the sustaining forces, a band c b; through the point, b, draw a line, parallel to the diagonal, e f; this may then be called the dividing line between ties and struts. Because all those supports which are on that side of the dividing line, which the straining force would occupy if unresisted, are compressed, while those on the other side of the dividing line are stretched.

In Fig. 183, the supports are both compressed, being on that side of the dividing line which the straining force would occupy if unresisted. In Fig. 187 and 188, in which $A \ B$ and $A \ C$ are the sustaining forces, $A \ C$ is compressed, whereas $A \ B$ is in a state of tension; $A \ C$ being on that side of the line, $h \ i$, which the straining force would occupy if unresisted, and $A \ B$ on the opposite side. The place of the latter might be supplied by a chain or rope. In Fig. 186, the foot of the rafter at A is sustained by two forces, the wall and the tie-beam, one perpendicular and the other horizontal : the direction of the straining force is indicated by the line, $b \ a$. The dividing line, $h \ i$, ascertained by the rule, shows that the wall is pressed and the tie-beam stretched.

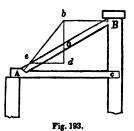
256.—Another example : let $E \land B F$, (Fig. 192,) represent a gate, supported by hinges at A and E. In this case, the *strain*-



ing force is the weight of the materials, and the direction of course vertical. Ascertain the dividing line at the several points, G, B, I, J, H and F. It will then appear that the force at G is sustained by A G and G E, and the dividing line shows that the former is stretched and the latter compressed. The force at H is supported by A H and HE—the former stretched and the latter compressed. The force at B is opposed by H B and A B, one pressed—the other stretched. The force at F is sustained by GF and FE, GF being stretched and FE pressed. By this it appears that A B is in a state of tension, and E F, of compression; also, that A H and G F are stretched, while B H and GE are compressed: which shows the necessity of having A Hand G F, each in one whole length, while B H and G E may be, as they are shown, each in two pieces. The force at J is sustained by G J and J H, the former stretched and the latter compressed. The piece, C D, is neither stretched nor pressed, and could be dispensed with if the joinings at J and I could be made as effectually without it. In case AB should fail, then CDwould be in a state of tension.

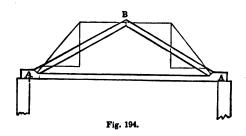
257.—The pressure of inclined beams. The centre of gravity of a uniform prism or cylinder, is in its axis, at the middle of its length. In irregular bodies with plain sides, the centre of

gravity may be found by balancing them upon the edge of a prism in two positions, making a line each time upon the body in a line with the edge of the prism, and the intersection of those lines will indicate the point required.

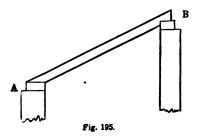


An inclined post or strut, supporting some heavy pressure applied at its upper end, as at Fig. 186, exerts a pressure at its foot in the direction of its length, or nearly so. But when such a beam is loaded uniformly over its whole length, as the rafter of a roof, the pressure at its foot varies considerably from the direction of its length. For example, let A B, (Fig. 193,) be a beam leaning against the wall, B c, and supported at its foot by the abutment, A, in the beam, Ac, and let o be the centre of gravity of the Through o, draw the vertical line, b d, and from B, draw beam. the horizontal line, Bb, cutting bd in b; join b and A, and bAwill be the *direction* of the thrust. To prevent the beam from loosing its footing, the joint at A should be made at right angles to b A. The amount of pressure will be found thus: let b d, (by any scale of equal parts,) equal the number of tons, cwts., or pounds weight upon the beam, A B; draw d e, parallel to Bb; then b e, (by the same scale,) equals the pressure in the direction, b A; and e d, the pressure against the wall at B—and also the horizontal thrust at A, as these are always equal in a construction of this kind. Fig. 194 represents two equal beams, supported at their feet by the abutments in the tie-beam. This case is similar to the last; for it is obvious that each beam is in precisely the position of the beam in Fig. 193. The horizontal

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pressures at B, being equal and opposite, balance one another; and their horizontal thrusts at the tie-beam are also equal. (See Art. 250—Fig. 186.) When the inclination of a roof, (Fig. 194,) is one-fourth of the span, or of a shed, (Fig. 193,) is one-half the span, the horizontal thrust of a rafter, whose centre of gravity is at the middle of its length, is exactly equal to the weight distributed uniformly over its surface. The inclination, in a rafter uniformly loaded, which will produce the least oblique pressure, (b e, Fig. 193,) is 35 degrees and 16 minutes.

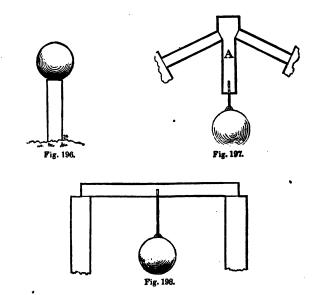


258.—In shed, or *lean-to* roofs, as *Fig.* 193, the horizontal pressure will be entirely removed, if the bearings of the rafters, as A, B, (Fig. 195), are made horizontal—provided, however, that the rafters and other framing do not bend between the points of support. If a beam or rafter have a natural curve, the convex or rounding edge should be laid uppermost.

259.—A beam laid horizontally, supported at each end and uniformly loaded, is subject to the greatest strain at the middle

of its length. The amount of pressure at that point is equal to half of the whole load sustained. The greatest strain coming upon the middle of such a beam, mortices, large knots and other defects, should be kept as far as possible from that point; and, in resting a load upon a beam, as a partition upon a floor beam, the weight should be so adjusted that it will bear at or near the ends. (See Art. 282.)

260.—The resistance of timber. When the stress that a given load exerts in any particular direction, has been ascertained, before the proper size of the timber can be determined for the resistance of that pressure, the strength of the kind of timber to be used must be known. The following rules for calculating the resistance of timber, are based upon the supposition that the timber used be of what is called "merchantable" quality—that is, strait-grained, seasoned, and free from large knots, splits, decay, &c.



The strength of a piece of timber, is to be considered in accordance with the direction in which the strain is applied upon

it. When it is compressed in the direction of its length, as in **Fig.** 196, its strength is termed the resistance to compression. When the force tends to pull it as under in the direction of its length, (A, Fig. 197,) it is termed the resistance to tension. And when strained by a force tending to break it crosswise, as at **Fig.** 198, its strength is called the resistance to cross strains.

261.—Resistance to compression. When the height of a piece of timber exceeds about 10 times its diameter if round, or 10 times its thickness if rectangular, it will bend before crushing. The first of the following cases, therefore, refers to such posts as would be *crushed* if overloaded, and the other two to such as would before crushing. In estimating the strength of timber for this kind of resistance, it is provided in the following rules that the pressure be exactly in a line with the axis of the post.

Case 1.—To find the area of a post that will safely bear a given weight—when the height of the post is less than 10 times its least thickness. **Rule.**—Divide the given weight in pounds by 1000 for pine and 1400 for oak, and the quotient will be the least area of the post in inches. This rule requires that the area of the *abutting surface* be equal to the result: should there be, therefore, a tenon on the end of the post, this quotient will be too small. **Example.**—What should be the least area of a pine post that will safely sustain 48,000 pounds? 48,000, divided by 1000, gives 48—the required area in inches. Such a post may be 6×8 inches, and will bear to be of any length within 10 times 6 inches, its least thickness.

Case 2.—To find the area of a rectangular post that will safely bear a given weight—when its height is 10 times its least thickness or more. Rule.—Multiply the given weight or pressure in pounds by the square of the length in feet; and multiply this product by the decimal, 0015, for oak, 0021, for pitch pine and 0016 for white pine; then divide this product by the breadth in inches, and the cube-root of the quotient will be the

thickness in inches. *Example.*—What should be the thickness of a pine post, 8 feet high and 8 inches wide, in order to support a weight of 12 tons, or 26,880 pounds? The square of the length is 64 feet; this, multiplied by the weight in pounds, gives 1,730,320; this product, multiplied by the decimal, 0016, gives 2768.512; and this again, divided by the breadth in inches, gives 346.064; by reference to the table of cube-roots in the appendix, the cube-root of this number will be found to be 7 inches large which is the thickness required. The stiffest rectangular post is that in which the sides are as 10 to 6.

Case 3.—To find the area of a round, or cylindrical, post, that will safely bear a given weight—when its height is 10 times its least diameter or more. Rule.—Multiply the given weight or pressure in pounds by 1.7, and the product by 0015 for oak, 0021 for pitch pine and 0016 for white pine; then multiply the squareroot of this product by the height in feet, and the square-root of the last product will be the diameter required, in inches. Example.—What should be the diameter of a cylindrical oak post, 8 feet high, in order to support a weight of 12 tons, or 26,880 pounds? This weight in pounds, multiplied by 1.7, gives 45,696; and this, by 0015, gives 68.544; the square-root of this product is (by the table in the appendix) 8.28, nearly—which, multiplied by 8, gives 66.24; the square-root of this number is 8.14, nearly; therefore, 8.14 inches is the diameter required.

Experiments have shown that the pressure should never be more than 1000 pounds per square inch on a joint in yellow pine —when the end of the grain of one piece is pressed against the side of the grain of the other.

262.—Resistance to tension. A bar of oak of an inch square, pulled in the direction of its length, has been torn as under by a weight of ______ - ____ - 11,500 lbs.

	-		~		-		11,000 10
Of white pine		-		-		-	11,000
Of pitch pine	-		Ŧ		-		10,000

Therefore, when the strain is applied in a line with the axis of the piece, the following rule must be observed.

To find the area of a piece of timber to resist a given strain in the direction of its length. *Rule.*—Divide the given weight to be sustained, by the weight that will tear asunder a bar an inch square of the same kind of wood, (as above,) and the product will be the area in inches of a piece that will just sustain the given weight; but the area should be at least 4 times this, to safely sustain a constant load of the given weight. *Example.*—What should be the area of a stick of pitch pine timber, which is required to sustain safely a constant load of 60,000 pounds? 60,000, divided by 10,000, (as above,) gives 6, and this, multiplied by 4, give 24 inches—the answer.

263.—Resistance to cross strains. To find the scantling of a piece of timber to sustain a given weight, when such piece is supported at the ends in a horizontal position.

Case 1.—When the breadth is given. Rule.—Multiply the square of the length in feet by the weight in pounds, and this product by the decimal, 009, for oak, 011 for white pine and 016 for pitch pine; divide the product by the breadth in inches, and the cube-root of the quotient will be the depth required in inches. *Example.*—What should be the depth of a beam of white pine, having a bearing of 24 feet and a breadth of 6 inches, in order to support 900 pounds? The square of 24 is 576, and this, multiplied by 900, gives 518 400; and this again, by 011, gives 5702 400; this, divided by 6, gives 950 400; the cube-root of which is 9.83 inches—the depth required.

Case 2.—When the depth is given. Rule.—Multiply the square of the length in feet by the weight in pounds, and multiply this product by the decimal, 009, for oak, 011 for white pine and 016 for pitch pine; divide the last product by the cube of the depth in inches, and the quotient will be the breadth in inches required. Example.—What should be the breadth of a beam of oak, having a bearing of 16 feet and a depth of 12 inches, in

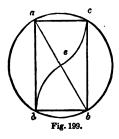
order to support a weight of 4000 pounds? The square of 16 is 256, which, multiplied by 4000, gives 1,024,000; this, multiplied by 009, gives 9216; and this again, divided by 1728, the cube of 12, gives $5\frac{1}{2}$ inches—which is the breadth required.

Case 3.—When the breadth bears a certain proportion to the depth. When neither the breadth nor depth is given, it will be best to fix on some proportion which the breadth should have to the depth; for instance, suppose it be convenient to make the breadth to the depth as 0.6 is to 1, then the rule would become as follows: Rule.--Multiply the weight in pounds by the decimal, .009, for oak, .011 for white pine and .016 for pitch pine; divide the product by 0.6, and extract the square-root; multiply this root by the length in feet, and extract the square-root a second time, which will be the depth in inches required. The breadth is equal to the depth multiplied by the decimal, 0.6. It is obvious that any other proportion of the breadth and depth may be obtained by merely changing the decimal, 0.6, in the rule. Example.—What should be the depth and breadth of a beam of pitch pine, having a proportion to one another as 0.6 to 1, and a bearing of 22 feet, in order to sustain a ton weight, or 2240 pounds? This, multiplied by .016, gives 35.84, which, divided by 0.6, gives 59.73; the square-root of this is 7.7, which, multiplied by 22, the length, gives 169.4; the square-root of this is 13-which is the depth required. Then 13, multiplied by 0.6, gives 7.8 inches-the required breadth.

Case 4.—When the beam is inclined, as A B, Fig. 193. Rule.—Multiply together the weight in pounds, the length of the beam in feet, the horizontal distance, A c, between the supports, in feet, and the decimal, 009, for oak, 011 for white pine, and 016 for pitch pine; divide this product by 0.6, and the fourth root of the quotient will give the depth in inches. The breadth is equal to the depth multiplied by the decimal, 0.6. Example.— What should be the size of an oak beam, the sides to bear a proportion to one another as 0.6 to 1, in order to support a ton weight



or 2240 pounds, the beam being inclined so that, its length being 20 feet, its horizontal distance between the points of support will be 16 feet? 2240, multiplied by 20, gives 44,800, which, multiplied by 16, gives 716,800; and this again, by the decimal, \cdot 009, gives 6451.2; this last, divided by 0.6, gives 10,752, the fourth root of which is 10.18, nearly; and this, multiplied by 0.6, gives 6.1; therefore, the size of the beam should be 10.18 inches by 6.1 inches.



264.—To ascertain the scantling of the stiffest beam that can be cut from a cylinder. Let $d \ a \ c \ b$, (Fig. 199,) be the section, and e the centre, of a given cylinder. Draw the diameter, $a \ b$; upon a and b, with the radius of the section, describe the arcs, $d \ e$ and $e \ c$; join d and a, a and c, c and b, and b and d; then the rectangle, $d \ a \ c \ b$, will be a section of the beam required.

265.—The greater the depth of a beam in proportion to the thickness, the greater the strength. But when the difference between the depth and the breadth is great, the beam must be stayed, (as at Fig. 202,) to prevent its falling over and breaking sideways. Their shrinking is another objection to deep beams; but where these evils can be remedied, the advantage of increasing the depth is considerable. The following rule is, to find the strongest form for a beam out of a given quantity of timber. Rule.—Multiply the length in feet by the decimal, 0.6, and divide the given area in inches by the product; and the square of the quotient will give the depth in inches. Example.—What is the strongest form for a beam whose given area of section is 48

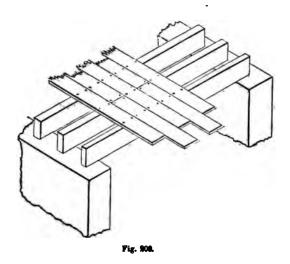
inches, and length of bearing 20 feet? The length in feet, 20, multiplied by the decimal, 0.6, gives 12; the given area in inches, 48, divided by 12, gives a quotient of 4, the square of which is 16—this is the depth in inches; and the breadth must be 3 inches. A beam 16 inches by 3 would bear twice as much as a square beam of the same area of section; which shows how important it is to make beams deep and thin. In many old buildings, and even in new ones, in country places, the very reverse of this has been practised; the principal beams being oftener laid on the broad side than on the narrower one.

266.—Systems of Framing. In the various parts of framing known as floors, partitions, roofs, bridges, &c., each has a specific object; and, in all designs for such constructions, this object should be kept clearly in view; the various parts being so disposed as to serve the design with the least quantity of material. The simplest form is the best, not only because it is the most economical, but for many other reasons. The great number of joints, in a complex design, render the construction liable to derangement by multiplied compressions, shrinkage, and, in consequence, highly increased oblique strains; by which its stability and durability are greatly lessened.

FLOORS.

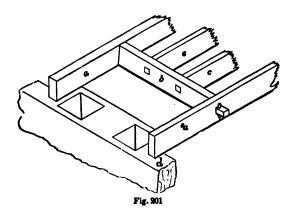
267.—Floors have been constructed in various ways, and are known as single-joisted, double, and framed. In a singlejoisted floor, the timbers, or floor-joists, are disposed as is shown in Fig. 200. Where strength is the principal object, this manner of disposing the floor-joists is far preferable; as experiments have proved that, with the same quantity of material, single-joisted floors are much stronger than either double or framed floors. To obtain the greatest strength, the joists should be thin and deep.

268.—To find the depth of a joist, the length of bearing and thickness being given, when the distance from centres is



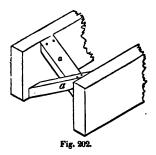
12 inches. Rule.—Divide the square of the length in feet, by the breadth in inches; and the cube-root of the quotient, multiplied by 2.2 for pine, or 2.3 for oak, will give the depth in inches. *Example.*—What should be the depth of floor-joists, having a bearing of 12 feet and a thickness of 3 inches, when said joists are of pine and placed 12 inches from centres? The square of 12 is 144, which, divided by 3, gives 48; the cube-root of this number is 3.63, which, multiplied by 2.2, gives 7.986 inches, the depth required; or 8 inches will be found near enough for practice.

269.—Where chimneys, flues, stairs, &c., occur to interrupt the bearing, the joists are framed into a piece, (b, Fig. 201,)called a *trimmer*. The beams, *a*, *a*, into which the trimmer is framed, are called *trimming-beams*, *trimming-joists*, or *carriage-beams*. They need to be stronger than the common joists, in proportion to the number of beams, *c*, *c*, which they support. The trimmers have to be made strong enough to support half the weight which the joists, *c*, *c*, support, (the wall, or another trimmer, at the other end supporting the other half,) and the *carriage*-



beams must each be strong enough to support half the weight which the trimmer supports. In calculating for the dimensions of floor-timbers, regard must be had to the fact that the weight which they generally support—such as persons of 150 pounds moving over the floor—exerts a much greater influence than equal weights at rest. When the trimmer, b, is not more distant from the bearing, d, than is necessary for ordinary hearths, &c., it will be sufficient to add $\frac{1}{6}$ of an inch to the thickness of the carriage-beam for every joist, c, that is supported. Thus, if the thickness of c is 3 inches, and the number of joists supported be 6, add 6 eighths, or $\frac{3}{4}$ of an inch, making the carriage-beams $3\frac{3}{4}$ inches thick. It is generally the practice in dwellings to make the carriage-beam, in all situations, one inch thicker than the common joists. But it is well to have a rule for determining the size more accurately in extreme cases.

270.—When the bearing exceeds 8 feet, there should be *struts*, as a and a, (*Fig.* 202,) well nailed between the joists. These will prevent the turning or twisting of the floor-joists, and will greatly stiffen the floor. For, in the event of a heavy weight resting upon one of the joists, these struts will prevent that joist from settling below the others, to the injury of the plastering

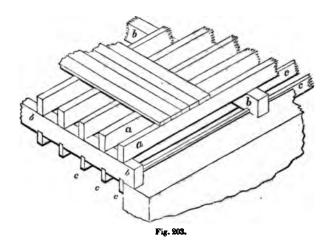


upon the underside. When the length of bearing is great, struts should be inserted at about every 4 feet.

271.—Single-joisted floors may be constructed for as great a length of bearing as timber of sufficient depth can be obtained; but, in such cases, where perfect ceilings are desirable, either double or framed floors are considered necessary. Yet the ceilings under a single-joisted floor may be rendered more durable by cross-furring, as it is termed—which consists of nailing a series of narrow strips of board on the under edge of the beams and at right angles to them. To these, instead of the beams, the laths are nailed. The strips should be not over 2 inches wide—enough to join the laths upon is all that is wanted in width—and not more than 12 inches apart. It is necessary that all furring for plastering be narrow, in order that the mortar may have a sufficient clinch.

When it is desirable to prevent the passage of sound, the openings between the beams, at about 3 inches from the upper edge, are closed by short pieces of boards, which rest on cleets nailed to the beam along its whole length. This forms a floor upon which mortar is laid to the depth of about 2 inches, leaving but about half an inch from its upper surface to the under side of the floor-plank.

272.—Double floors. A double floor consists, as at Fig. 203, of three tiers of joists or timbers; viz., bridging-joists, a, a, binding-joists, b, b, and ceiling-joists, c, c. The binding-joists



are the principal support, and of course reach from wall to wall. The bridging-joists, which support the floor-plank, are laid upon the binding-joists, to which they are nailed; sometimes they are notched into the binding-joists, but they are sufficiently firm when well nailed. The ceiling-joists are notched into the under side of the binders, and nailed; they are the support of the lath and plastering.

273.—Binders are laid 6 feet apart. At this distance the following rules will give the scantling.

Case 1.—To find the depth of a binding-joist, the length and breadth being given. Rule.—Divide the square of the length in feet, by the breadth in inches; and the cube-root of the quotient, multiplied by 3.42 for pine, or by 3.53 for oak, will give the depth in inches. Example.—What should be the depth of a bindingjoist, having a length of 12 feet and a breadth of 6 inches, when the kind of timber is pine? The square of 12 is 144, which, divided by 6, gives 24; the cube-root of this is 2.88, which, multiplied by 3.42, gives 9.85, the depth in inches.

Case 2.—To find the breadth, when the depth and length are given. Rule.—Divide the square of the length in feet, by the

cube of the depth in inches; and multiply the quotient by 40 for pine, or by 44 for oak, which will give the breadth in inches. *Example.*—What should be the breadth of a binding-joist, having a length of 12 feet and a depth of 10 inches, when the kind of wood is pine? The cube of 10 is 1000; the square of 12 is 144; this, divided by 1000, gives a quotient of 144; and this quotient; multiplied by 40, gives 5.76, the breadth in inches.

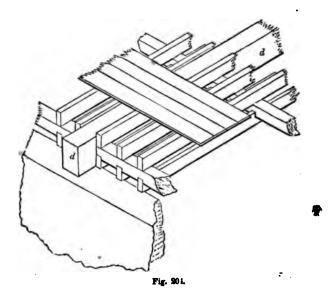
274.—Bridging-joists are laid from 12 to 20 inches apart. The scantling may be found by the rule at Art. 268.

275.—Ceiling-joists are generally placed 12 inches apart from centres. They are arranged to suit the length of the lath; this being, in most cases, 4 feet long. What is said at Art. 271, in regard to the width of furring for plastering, will apply to the thickness of ceiling-joists.

To find the depth of a ceiling-joist, when the length of bearing and thickness are given. *Rule.*—Divide the length in feet by the cube-root of the breadth in inches; and multiply the quotient by 0.64 for pine, or by 0.67 for oak, which will give the depth in inches. *Example.*—What should be the depth of a ceiling-joist of pine, when the length of bearing is 6 feet and the thickness 2 inches? The length in feet, 6, divided by the cube-root of the breadth in inches, 1.26, gives a quotient of 4.76, which, being multiplied by the decimal, 0.64, gives 3 inches, the depth required.

When the thickness of a ceiling-joist is 2 inches, the depth in inches will be equal to half the length of bearing in feet. Thus, if the bearing is 6 feet, the depth will be 3 inches; bearing 8 feet, depth 4 inches, &c.

276.—Framed floors. When a good ceiling is required, and the distance of bearing is great, the binding-joists, instead of reaching from wall to wall, are framed into girders. These are heavy timbers, as d, (Fig. 204,) which reach from wall to wall, being the chief support of the floor. Such an arrangement is termed a framed floor. The binding, the bridging and the ceil-



ing-joists in these, are the same as those in double floors just described. The distinctive feature of this kind of floor is the girder.

277.—Girders should be made as deep as the timber will allow: if their being increased in size should reduce the height of a story a few inches, it would be better than to have a house suffer from defective ceilings and insecure floors. In the following rules for the scantling of girders, they are supposed to be placed at 10 feet apart.

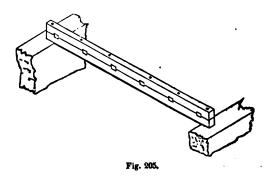
Case 1.—To find the depth, when the breadth of the girder and the length of bearing are given. *Rule.*—Divide the square of the length in feet, by the breadth in inches; and the cube-root of the quotient, multiplied by 4.2 for pine, or by 4.3 for oak, will give the depth required in inches. *Example.*—What should be the depth of a pine girder, having a length of 20 feet and a breadth of 13 inches? The square of 20 is 400, which, divided by 13, gives 30.77; the cube-root of this is 3.12, which, multiplied by 4.2, gives 13 inches, the depth required.

Case 2.—To find the breadth, when the length of bearing and depth are given. *Rule.*—Divide the square of the length in feet, by the cube of the depth in inches; and the quotient, multiplied by 74 for pine, or by 82 for oak, will give the breadth in inches. *Example.*—What should be the breadth of a pine girder, having a length of 18 feet and a depth of 14 inches? The square of the length in feet, 324, divided by the cube of the depth in inches, 2744, gives 118; and this, multiplied by 74, gives 8.73 inches, the breadth required.

278.—When the breadth of a girder is more than about 12 inches, it is recommended to divide it by sawing from end to end, vertically through the middle, and then to bolt it together with the sawn sides outwards. This is not to strengthen the girder, as some have supposed, but to reduce the size of the timber, in order that it may dry sooner. The operation affords also an opportunity to examine the heart of the stick-a necessary precaution; as large trees are frequently in a state of decay at the heart, although outwardly they are seemingly sound. When the halves are bolted together, thin slips of wood should be inserted between. them at the several points at which they are bolted, in order to leave sufficient space for the air to circulate between. This tends to prevent decay; which will be found first at such parts as are not exactly tight, nor yet far enough apart to permit the escape of moisture.

279.—When girders are required for a long bearing, it is usual to truss them; that is, to insert between the halves two pieces of oak which are inclined towards each other, and which meet at the centre of the length of the girder, like the rafters of a rooftruss, though nearly if not quite concealed within the girder. This, and many similar methods, though extensively practised, are generally worse than useless; since it has been ascertained that, in nearly all such cases, the operation has positively *weakened* the girder.

A girder may be strengthened by mechanical contrivance, when



its depth is required to be greater than any one piece of timber Fig. 205 shows a very simple yet scientific method will allow. of doing this. The two pieces of which the girder is composed are bolted, or pinned, together, having keys inserted between to prevent the pieces from sliding. The keys should be of hard wood, well seasoned. The two pieces should be about equal in depth, in order that the joint between them may be in the neutral (See Art, 254.) The thickness of the keys should be line. about half their breadth, and the amount of their united thicknesses should be equal to a trifle over the depth and one-third of the depth of the girder. Instead of bolts or pins, iron hoops are sometimes used; and when they can be procured, they are far preferable. In this case, the girder is diminished at the ends, and the hoops driven from each end towards the middle.

280.—Beams may be spliced, if none of a sufficient length can be obtained, though not at or near the middle, if it can be avoided. (See Art. 259 and 332.) Girders should rest from 9 to 12 inches on the wall, and a space should be left for the air to circulate around the ends, that the dampness may evaporate. Floor-timbers are supported at their ends by walls of considerable height. They should not be permitted to rest upon intervening partitions, which are not likely to settle as much as the walls; otherwise the unequal settlements will derange the level of the floor. As all floors, however well-constructed, settle in some degree, it is advisable to

frame the joists a little higher at the middle of the room than at its sides,—as also the ceiling-joists and cross-furring, when either are used. In single-joisted floors, for the same reason, the rounded edge of the stick, if it have one, should be placed uppermost.

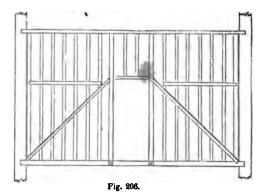
If the floor-plank are laid down temporarily at first, and left to season a few months before they are finally driven together and secured, the joints will remain much closer. But if the edges of the plank are planed after the first laying, they will shrink again ; as it is the nature of wood to shrink after *every* planing however dry it may have been before.

PARTITIONS.

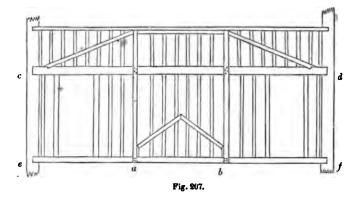
281.—Too little attention has been given to the construction of this part of the frame-work of a house. The settling of floors and the cracking of ceilings and walls, which disfigure to so great an extent the apartments of even our most costly houses, may be attributed almost solely to this negligence. A square of partitioning weighs about half a ton, a greater weight, when added to its customary load, such as furniture, storage, &c., than any ordinary floor is calculated to sustain. Hence the timbers bend, the ceilings and cornices crack, and the whole interior part of the house settles; showing the necessity for providing adequate supports independent of the floor-timbers. A partition should, if practicable, be supported by the walls with which it is connected, in order, if the walls settle, that it may settle with them. This would prevent the separation of the plastering at the angles of rooms. For the same reason, a firm connection with the ceiling is an important object in the construction of a partition.

282.—The joists in a partition should be so placed as to discharge the weight upon the points of support. All oblique pieces in a partition, that tend not to this object, are much better omitted. Fig. 206 represents a partition having a door in the middle. Its

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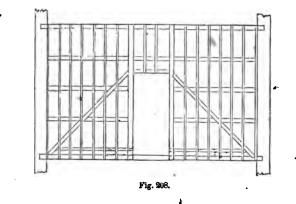




construction is simple but effective. Fig. 207 shows the manner of constructing a partition having doors near the ends. The true is formed above the door-heads, and the lower parts are suspended from it. The posts, a and b, are halved, and nailed to the tie, cd, and the sill, ef. The braces in a trussed partition should be placed so as to form, as near as possible, an angle of 40 degrees with the horizon. In partitions that are intended to support only their own weight, the principal timbers may be 3×4 inches for a 20 feet span, $3\frac{1}{2}\times5$ for 30 feet, and 4×6 for 40. The thickness of the filling-in stuff may be regulated according to what is said at *Art.* 271, in regard to the width of furring for plastering. The

filling-in pieces should be stiffened at about every three feet by short struts between.

All superfluous timber, besides being an unnecessary load upon the points of support, tends to injure the stability of the plastering; for, as the strength of the plastering depends, in a great measure, upon its clinch, formed by pressing the mortar through the space between the laths, the narrower the surface, therefore, upon which the laths are nailed, the less will be the quantity of plastering unclinched, and hence its greater security from fractures. For this reason, the principal timbers of the partition should have their edges reduced, by chamfering off the corners.



283.—When the principal timbers of a partition require to be large for the purpose of greater strength, it is a good plan to omit the upright filling-in pieces, and in their stead, to place a few horizontal pieces; in order, upon these and the principal timbers, to nail upright battens at the proper distances for lathing, as in *Fig.* 208. A partition thus constructed requires a little more space than others; but it has the advantage of insuring greater stability to the plastering, and also of preventing to a good degree the conversation of one room from being heard in the other. When a partition is required to support, in addition to its own weight, that of a floor or some other burden resting upon it, the dimensions of

the timbers may be ascertained, by applying the principles which regulate the laws of pressure and those of the resistance of timber, as explained at the first part of this section. The following data, however, may assist in calculating the amount of pressure upon partitions:

284.—The weight of a square, (that is, a hundred square feet,) of partitioning may be estimated at from 1500 to 2000 lbs.; a square of single-joisted flooring, at from 1200 to 2000 lbs.; a square of framed flooring, at from 2700 to 4500 lbs.; and the weight of a square of *deafening*, (as described at the latter part of Art. 271,) at about 1500 lbs.

When a floor is supported at two opposite extremities, and by a partition introduced midway, one-half of the weight of the whole floor will then be supported by the partition. As the settling of partitions and floors, which is so disastrous to plastering, is frequently owing to the shrinking of the timber and to ill-made joints, it is very important that the timber be seasoned and the work well executed.

ROOFS.*

285.—In ancient buildings, the Norman and the Gothic, the walls and buttresses were erected so massive and firm, that it was customary to construct their roofs without a tie-beam; the walls being abundantly capable of resisting the lateral pressure exerted by the rafters. But in modern buildings, the walls are so slightly built as to be incapable of resisting scarcely any oblique pressure; and hence the necessity of constructing the roof so that all oblique and lateral strains may be removed; as, also, that instead of having a tendency to separate the walls, the roof may contribute to bind and steady them.

286.—In estimating the pressures upon any certain roof, for the purpose of ascertaining the proper sizes for the timbers, calculation must be made for the pressure exerted by the wind, and, if

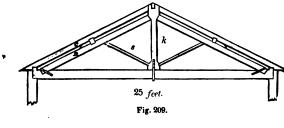
* See also Art. 228.

in a cold climate, for the weight of snow, in addition to the weight of the materials of which the roof is composed. The force of wind may be calculated at 40 lbs. on a square foot. The weight of snow will be of course according to the depth it acquires. (See weight of materials, in Appendix.) In a severe climate, roofs ought to be constructed steeper than in a milder one; in order that the snow may have a tendency to slide off before it becomes of sufficient weight to endanger the safety of the roof. The inclination should be regulated in accordance with the qualities of the material with which the roof is to be covered. The following table may be useful in determining the inclination, and in estimating the weight of the various kinds of covering:

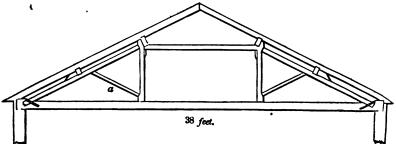
MATERIAL.	INCLINATION.				WEIGHT UPON A SQUARE FOOT		
Tin,	Rise	1	inch to	a foot.	$\frac{5}{8}$ to $1\frac{1}{4}$ lbs.		
Copper, -	"	1	"	"	1 to 14 "		
Lead, -	"	2	inches	"	4 to 7 "		
Zinc,	"	3	"	"	11 to 2. "		
Short pine shingles,	"	5	"	"	$1\frac{1}{2}$ to $2\frac{1}{2}$ "		
Long cypress shingles,	"	6	"	"	4 to 5 "		
Slate,	"	6	"	"	5 to 9 "		

The weight of the covering, as above estimated, is that of the material only, added to the weight of whatever is used to fix it to the roof, such as nails, &c.; what the material is laid on, such as plank, boards or lath, is not included.

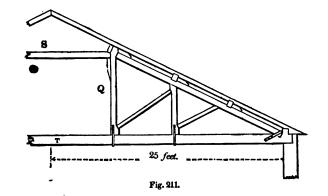
287.—Fig. 209 to 212 give a general idea of the usual manner of constructing trusses for roofs: c, (Fig. 209,) is a common

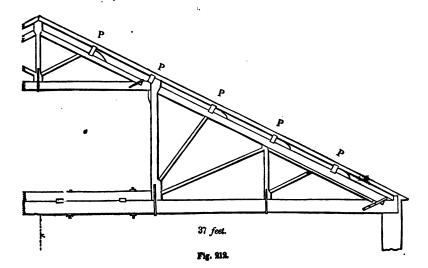


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rafter; R is a principal rafter; k is a king-post; s is a strut; S, (*Fig.* 211,) is a straining-beam; Q is a queen-post; T is a tiebeam; and P, P, (*Fig.* 212,) are purlins. In constructing a roof of importance, the trusses should be placed not over 10 feet apart, the principal rafter supported by a strut at every purlin, the purlin *notched on* instead of being framed into the principal rafters, and the tie-beam supported at proper distances, according to the weight of the ceiling or whatever else it is required to support.

288.—The dimensions of the timbers may be found in accordance with the principles explained at the first part of this section; but for general purposes, the following rules, deduced from the experience of practical builders and from scientific principles, may be found useful: these rules give the dimensions of the piece at its smallest part.

289.—To find the dimensions of a king-post. Rule.—Multiply the length of the post in feet by the span in feet. Then multiply this product by the decimal, 0.12, for pine, or by 0.13 for oak, which will give the area of the king-post in inches; and divide this area by the breadth, and it will give the thickness; or by the thickness for the breadth. *Example.*—What should be the dimensions of a pine king-post, 8 feet long, for a roof having a span of 25 feet? 8 times 25 is 200; this, multiplied by the decimal, 0.12, gives 24 inches for the area; 4×6 , therefore, would be a good size at the smallest part.

290.—To find the dimensions of a queen-post. Rule.—Multiply the length in feet, of the queen-post or suspending-piece, by that part of the length of the tie-beam it supports, also in feet. This product, multiplied by the decimal, 0.27, for pine, or by 0.32 for oak, will give the area of the post in inches; and dividing this area by the thickness will give the breadth. *Example.*— The queen-posts in *Fig.* 210 support each $\frac{1}{3}$ of the tie-beam, which is 12 $\frac{3}{3}$ feet. To make them of pine, 6 feet long, what should be their dimensions? 12 $\frac{3}{3}$, multiplied by 6, gives 76,

which, multiplied by 0.27, gives 20.52; which indicates a size of about 4×54 .

291.—To find the dimensions of a tie-beam, that is required to support a ceiling only. Rule.—Divide the length of the longest unsupported part by the cube-root of the breadth; and the quotient, multiplied by 1.47 for pine, or by 1.52 for oak, will give the depth in inches. Example.—The length of the longest unsupported part of the tie-beam in Fig. 210 is 123 feet. What should be the depth of the tie-beam, the breadth being 6 inches, and the kind of wood, pine? The cube-root of 6 is 1.82, and 123, divided by 1.82, gives a quotient of 6.956; this, multiplied by 1.47, gives 10.225. The size of the tie-beam, therefore, may be 6×103 . When there are rooms in the roof, the dimensions for the tie-beam can be found by the rule for girders, (Art. 277.)

292.—To find the dimensions of a principal rafter when there is a king-post in the middle. Rule.—Multiply the square of the length of the rafter in feet, by the span in feet; and divide the product by the cube of the thickness in inches. For pine, multiply the quotient by '096, which will give the depth in inches. Example.—What should be the depth of a rafter of pine, 22:36 feet long, and 6 inches thick, the roof having a span of 40 feet? The square of 22:36 is 500 nearly, this, multiplied by 40, gives 20000; and this, divided by 216, the cube of the thickness, gives 92:59; which, multiplied by .096, equals 8:888. The size of the rafter should, therefore, be $6 \times 8\frac{2}{5}$.

293.—To find the dimensions of a principal rafter when two queen-posts are used instead of a king-post. Rule.—The same as the last, except that the decimal, 0.155, must be used instead of 0.096. Example.—What should be the dimensions of a principal rafter, having a length of 14 feet, (as in Fig. 210,) and a thickness of 6 inches, when the span of the roof is 38 feet and the wood is pine? The square of 14 is 196, which, multiplied by 38, gives 7448; this, divided by 216, the cube of 6, gives

31:48, which, multiplied by 0:155, gives 5:34. The size of the rafter should, therefore, be $6 \times 5_{\overline{s}}^3$.

294.—To find the dimensions of a straining-beam. In order that this beam may be the strongest possible, its depth should be to its thickness as 10 is to 7. Rule.--Multiply the square-root of the span in feet, by the length of the straining-beam in feet, and extract the square-root of the product. Multiply this root by 0.9 for pine, which will give the depth in inches To find the thickness, multiply the depth by the decimal, 0.7. Example.---What should be the dimensions of a pine straining-beam, 12 feet ng, for a span of 38 feet? The square-root of the span is 6.164, which, multiplied by 12, gives 73.968; the square-root of this is nearly 8.60, which, multiplied by 0.9, gives 7.74-the depth. This, multiplied by 0.7, gives 5.418—the thickness. Therefore, the beam should be $5\frac{3}{4} \times 7\frac{3}{4}$, or $5\frac{1}{4} \times 8$.

295.—To find the dimensions of struts and braces. Rule.— Multiply the square-root of the length supported in feet, by the length of the brace or strut in feet; and the square-root of the product, multiplied by 0.8 for pine, will give the depth in inches; and the depth, multiplied by the decimal, 0.6, will give the thickness in inches. *Example.*—In *Fig.* 210, the part supported by the brace or strut, *a*, is equal to half the length of the principal rafter, or 7 feet; and the length of the brace is 6 feet: what should be the size of a pine brace? The square-root of 7 is 2.65, which, multiplied by 0.8, gives 3.192—the depth. This, multiplied by 0.6, gives 1.9152, the thickness. Therefore, the brace should be 2×3 inches.

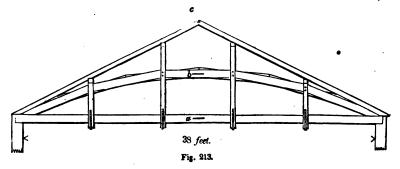
It is customary to make the principal rafters, tie-beam, posts and braces, all of the same thickness, that the whole truss may be of the same thickness throughout.

296.—To find the dimensions of purlins. Rule.—Multiply the cube of the length of the purlin in feet, by the distance the purlins are apart in feet; and the fourth root of the product for pine will give the depth in inches; or multiply by 1.04 to obtain

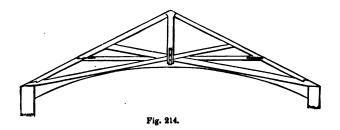
the depth for oak; and the depth, multiplied by the decimal, 0.6, will give the thickness. *Example.*—What should be the dimensions of pine purlins, 9 feet long and 6 feet apart? The cube of 9 is 729, which, multiplied by 6, gives 4374; the fourth root of this is 8.13—the required depth. This, multiplied by 0.6, gives 4.878—the thickness. A proper size for them would be about 5×8 inches. Purlins should be long enough to extend over two, three or more trusses.

297.—To find the dimensions of common rafters. The following rule is for slate roofs, having the rafters placed 12 inches apart. Shingle roofs may have rafters placed 2 feet apart. The dimensions of rafters for other kinds of covering may be found by reference to the table at Art. 286, and the laws of pressure at the first part of this section. Rule.—Divide the length of bearing in feet, by the cube-root of the breadth in inches; and the quotient, multiplied by 0.72 for pine, or 0.74 for oak, will give the depth in inches. Example.—What should be the depth of a pine rafter, 7 feet long and 2 inches thick? 7 feet, divided by 1.26, the cubefoot of 2, gives 5.55, which, multiplied by 0.72, gives nearly 4 inches—the depth required.

298.—If, instead of framing the principal rafters and strainingbeam into the king and the queen posts, they be permitted to abut against each other, and the king and the queen posts be made in halves, notched on and bolted, or strapped to each other and to the tie-beam, much of the ill effects of shrinking in the heads of the king and the queen posts will be avoided. (See Art. 339 and 340.)

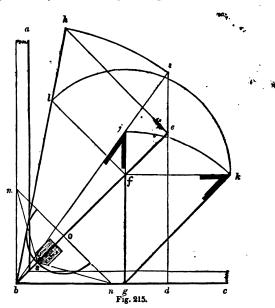


299.—Fig. 213 shows a method of constructing a truss having a built-rib in the place of principal rafters. The proper form for the curve is that of a parabola, (Art. 127.) This curve, when as flat as is described in the figure, approximates so near to that of the circle, that the latter may be used in its stead. The height, a b, is just half of a c, the curve to pass through the middle of the rib. The rib is composed of two series of abutting pieces, bolted together. These pieces should be as long as the dimensions of the timber will admit, in order that there may be but few joints. The suspending pieces are in halves, notched and bolted to the tie-beam and rib, and a purlin is framed upon the upper end of each. A truss of this construction needs, for ordinary roofs, no diagonal braces between the suspending pieces, but if extra strength is required the braces may be added. The best place for the suspending pieces is at the joints of the rib. A rib of this kind will be sufficiently strong, if the area of its section contain about one-fourth more timber, than is required for that of a straining-beam for a roof of the same size. The proportion of the depth to the thickness should be about as 10 is to 7.



300.—Some writers have given designs for roofs similar to Fig. 214, having the tie-beam omitted for the accommodation of an arch in the ceiling. This and all similar designs are seriously objectionable, and should always be avoided; as the small height gained by the omission of the tie-beam can never compensate for the powerful lateral strains, which are exerted by the oblique position of the supports, tending to separate the walls. Where an arch

is required in the ceiling, the best plan is to carry up the walls as high as the top of the arch. Then, by using a horizontal tiebeam, the oblique strains will be entirely removed. Many a public building in this place and vicinity, has been all but ruined by the settling of the roof, consequent upon a defective plan in the formation of the truss in this respect. It is very necessary, therefore, that the horizontal tie-beam be used, except where the walls are made so strong and firm by abutments, or other support, as to prevent a possibility of their separating.



301.—Fig. 215 is a method of obtaining the proper lengths and bevils for rafters in a hip-roof, $a \ b$ and $b \ c$ are walls at the angle of the building; $b \ e$ is the seat of the hip-rafter and $g \ f$ of a jack or cripple rafter. Draw $e \ h$, at right angles to $b \ e$, and **make** it equal to the rise of the roof; join b and h, and $h \ b$ will be the length of the hip-rafter. Through e, draw $d \ i$, at right angles to $b \ c$; upon b, with the radius, $b \ h$, describe the arc, $h \ i$, cutting $d \ i$ in i; join b and i, and extend $g \ f$ to meet $b \ i$ in j; then $g \ j$ will

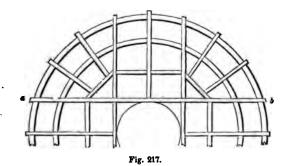
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be the length of the jack-rafter. The length of each jack-rafter is found in the same manner-by extending its seat to cut the line, b i. From f, draw f k, at right angles to f g, also f l, at right angles to be; make fk equal to fl by the arc, lk, or make gkequal to g j by the arc, j k; then the angle at j will be the topbevil of the jack-rafters, and the one at k will be the down-bevil.

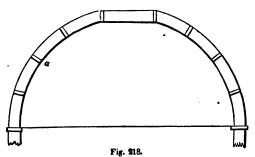
392.-To find the backing of the hip-rafter. At any convenient place in b e, (Fig. 215,) as o, draw m n, at right angles to b e; from o, tangical to b h, describe a semi-circle, cutting b e in s; join m and s and n and s; then these lines will form at s the proper angle for beviling the top of the hip-rafter.

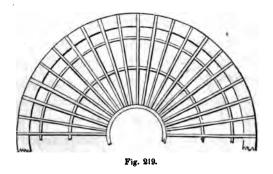
> DOMES. Fig. 216.



* The lengths and bevils of rafters for roof-valleys can also be found by the above process † See also Art. 227 22

303.—The most usual form for domes is that of the sphere, the base being circular. When the interior dome does not rise to high, a horizontal tie may be thrown across, by which any degree of strength required may be obtained. Fig. 216 shows a section, and Fig. 217 the plan, of a dome of this kind, a b being the tie-beam in both. Two trusses of this kind, (Fig. 216,) parallel to each other, are to be placed one on each side of the opening in the top of the dome. Upon these the whole framework is to depend for support, and their strength must be calculated accordingly. (See the first part of this section, and Art. 286.) If the dome is large and of importance, two other trusses may be introduced at right angles to the foregoing, the tie-beams being preserved in one continuous length by framing them high enough to pass over the others.





304.—When the interior dome rises too high to admit of a level

b-beam, the framing may be composed of a succession of ribs anding upon a continuous circular curb of timber, as seen at **ig**. 218 and 219,—the latter being a plan and the former a secon. This curb must be well secured, as it serves in the place **f** a tie-beam to resist the lateral thrust of the ribs. In small iomes, these ribs may be easily cut from wide plank; but, where **n** extensive structure is required, they must be built in two hicknesses so as to break joints, in the same manner as is described for a roof at Art. 299. They should be placed at about two eet apart at the base, and strutted as at a in Fig. 218.

305.—The scantling of each thickness of the rib may be as follows:

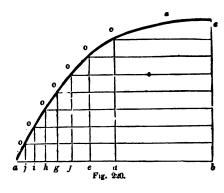
For domes of 24 feet diameter, 1×8 inches.

"	"	36	"	$1\frac{1}{2} \times 10$	"
"	"	60	"	2×13	"
"	"	9 0	"	21×13	"
"	"	108	"	3×13	"

306.—Although the outer and the inner surfaces of a dome may be finished to any curve that may be desired, yet the framing should be constructed of such a form, as to insure that the curve of equilibrium will pass through the middle of the depth of the framing. The nature of this curve is such that, if an arch or dome be constructed in accordance with it, no one part of the structure will be less capable than another of resisting the strains and pressures to which the whole fabric may be exposed. The curve of equilibrium for an arched vault or a roof, where the load is equally diffused over the whole surface, is that of a parabola, (Art. 127;) for a dome, having no lantern, tower or cupola above it, a cubic parabola, (Fig. 220;) and for one having a tower, &c., above it, a curve approaching that of an hyperbola must be adopted, as the greatest strength is required at its upper parts. If the curve of a dome be circular, (as in the vertical section, Fig. 218,) the pressure will have a tendency to burst the dome outwards at about one-third of its height. Therefore, when this form is used

in the construction of an extensive dome, an iron band should be placed around the framework at that height; and whatever may be the form of the curve, a band or tie of some kind is necessary around or across the base.

If the framing be of a form less convex than the curve of equilibrium, the weight will have a tendency to crush the ribs inwards, but this pressure may be effectually overcome by strutting between the ribs; and hence it is important that the struts be so placed as to form continuous horizontal circles.

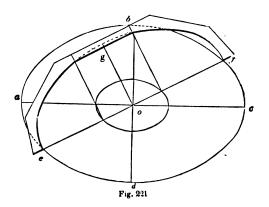


307.—To describe a cubic parabola. Let a b, (Fig. 220,) be the base and b c the height. Bisect a b at d, and divide a d into 100 equal parts; of these give d e 26, e f 181, f g 141, g h 121, h i 101, i j 91, and the balance, 81, to j a; divide b c into 8 equal parts, and, from the points of division, draw lines parallel to $a b_7$ to meet perpendiculars from the several points of division in $a b_7$ at the points, o, o, o, &c. Then a curve traced through these points will be the one required.

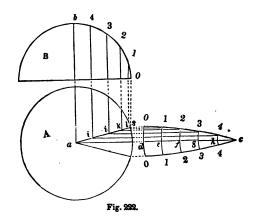
308.—Small domes to light stairways, &c., are frequently made elliptical in both plan and section; and as no two of the ribs in one quarter of the dome are alike in form, a method for obtaining the curves is necessary.

309.-To find the curves for the ribs of an elliptical dome. Let a b c d, (Fig. 221,) be the plan of a dome, and e f the seat

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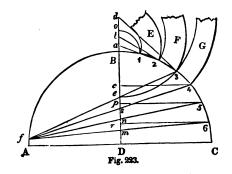


of one of the ribs. Then take e f for the transverse *axis* and twice the rise, o g, of the dome for the conjugate, and describe, (according to *Art.* 115, 116, &c.,) the semi-ellipse, e g f, which will be the curve required for the rib, e g f. The other ribs are found in the same manner.



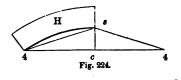
310.—To find the shape of the covering for a spherical dome. Let A, (Fig. 222,) be the plan and B the section of a given dome. From a, draw a c, at right angles to a b; find the stretch-out, (Art. 92,) of o b, and make d c equal to it; divide the arc, o b, and the line, d c, each into a like number of equal parts,

as 5, (a large number will insure greater accuracy than a small one;) upon c, through the several points of division in c d, describe the arcs, o d o, 1 e 1, 2 f 2, &c.; make d o equal to half the width of one of the boards, and draw o s, parallel to a c; join s and a, and from the points of division in the arc, o b, drop perpendiculars, meeting a s in ij k l; from these points, draw i 4, j 3, &c., parallel to a c; make d o, e 1, &c., on the lower side of a c, equal to d o, e 1, &c., on the upper side; trace a curve through the points, o, 1, 2, 3, 4, c, on each side of d c; then o c o will be the proper shape for the board. By dividing the circumference of the base, A, into equal parts, and making the bottom, o d o, of the board of a size equal to one of those parts, every board may be made of the same size. In the same manner as the above, the shape of the covering for sections of another form may be found, such as an ogee, cove, &c.

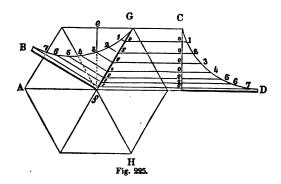


311.—To find the curve of the boards when laid in horizontal courses. Let $A \ B \ C$, (Fig. 223,) be the section of a given dome, and $D \ B$ its axis. Divide $B \ C$ into as many parts as there are to be courses of boards, in the points, 1, 2, 3, &cc.; through 1 and 2, draw a line to meet the axis extended at a; then a will be the centre for describing the edges of the board, E. Through 3 and 2, draw 3 b; then b will be the centre for describing F. Through 4 and 3, draw 4 d; then d will be the centre for G. B is the centre for the arc, 1 o. If this method is taken to find

the centres for the boards at the base of the dome, they would occur so distant as to make it impracticable : the following method is preferable for this purpose. G being the last board obtained by the above method, extend the curve of its inner edge until it meets the axis, DB, in e; from 3, through e, draw 3 f, meeting the arc, AB, in f; join f and 4, f and 5 and f and 6, cutting the axis, DB, in s, n and m; from 4, 5 and 6, draw lines parallel to AC and cutting the axis in c, p and r; make c 4, (Fig. 224,)



equal to c 4 in the previous figure, and c s equal to c s also in the previous figure; then describe the inner edge of the board, H, according to Art. 87: the outer edge can be obtained by gauging from the inner edge. In like manner proceed to obtain the next board—taking p 5 for half the chord and p n for the height of the segment. Should the segment be too large to be described easily, reduce it by finding intermediate points in the curve, as at Art. 86.

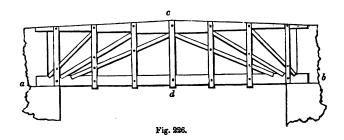


312.— To find the shape of the angle-rib for a polygonal dome. Let $A \in H$, (Fig. 225,) be the plan of a given dome, and

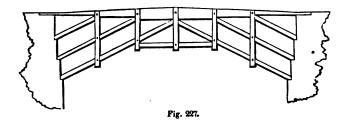
C D a vertical section taken at the line, ef. From 1, 2, 3, &c., in the arc, C D, draw ordinates, parallel to A D, to meet f G; from the points of intersection on f G, draw ordinates at rightangles to f G; make s 1 equal to o 1, s 2 equal to o 2, &c.; then G f B, obtained in this way, will be the angle-rib required. The best position for the sheathing-boards for a dome of this kind is horizontal, but if they are required to be bent from the base to the vertex, their shape may be found in a similar manner to that shown at Fig. 222.

BRIDGES.

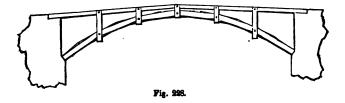
313.—Various plans have been adopted for the construction of bridges, of which perhaps the following are the most useful. *Fig.* 226 shows a method of constructing wooden bridges, where the banks of the river are high enough to permit the use of the tie-beam, a b. The upright pieces, c d, are notched and bolted on in pairs, for the support of the tie-beam. A bridge of this construction exerts no lateral pressure upon the abutments. This method may be employed even where the banks of the river are low, by letting the timbers for the roadway rest immediately upon the tie-beam. In this case, the framework above will serve the purpose of a railing.



314.-Fig. 227 exhibits a wooden bridge without a tie-beam. Where staunch buttresses can be obtained, this method may be recommended; but if there is any doubt of their stability, it



should not be attempted, as it is evident that such a system of framing is capable of a tremendous lateral thrust.

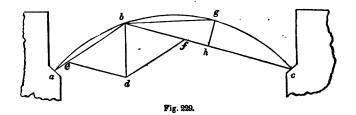


315.—Fig. 228 represents a wooden bridge in which a built-rib, (see Art. 299,) is introduced as a chief support. The curve of equilibrium will not differ much from that of a parabola: this, therefore, may be used—especially if the rib is made gradually a little stronger as it approaches the buttresses. As it is desirable that a bridge be kept low, the following table is given to show the least rise that may be given to the rib.

Span in feet.	Least rise in feet.	Span in feet.	Least rise in feet.	Span in feet.	Least rise in feet.
30	0.5	120	7	280	24
40	0.8	140	8	300	28
50	1.4	160	10	320	32
60	2	180	11	350	39
70	2 1	200	12	380	47
80	3	220	14	400	53
90	4	240	17		
100	5	260	20		

The rise should never be made less than this, but in all cases . 23

greater if practicable; as a small rise requires a greater quantity of timber to make the bridge equally strong. The greatest uniform weight with which a bridge is likely to be loaded is, probably, that of a dense crowd of people. This may be estimated at 120 pounds per square foot, and the framing and gravelled roadway at 180 pounds more; which amounts to 300 pounds on a square foot. The following rule, based upon this estimate, may be useful in determining the area of the ribs. Rule.--Multiply the width of the bridge by the square of half the span, both in feet; and divide this product by the rise in feet, multiplied by the number of ribs; the quotient, multiplied by the decimal, 0.0011, will give the area of each rib in feet. When the roadway is only planked, use the decimal, 0.0007, instead of 0.0011. Example.—What should be the area of the ribs for a bridge of 200 feet span, to rise 15 feet, and be 30 feet wide, with 3 curved ribs? The half of the span is 100 and its square is 10,000; this, multiplied by 30, gives 300,000, and 15, multiplied by 3, gives 45; then 300,000, divided by 45, gives 6666; which, multiplied by 0.0011, gives 7.333 feet, or 1056 inches for the area of each rib. Such a rib may be 24 inches thick by 44 inches deep, and composed of 6 pieces, 2 in width and 3 in depth.



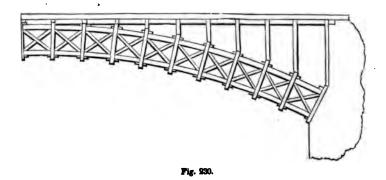
316.—The above rule gives the area of a rib, that would be requisite to support the greatest possible *uniform* load. But in large bridges, a *variable* load, such as a heavy wagon, is capable of exerting much greater strains; in such cases, therefore, the rib should be made larger. The greatest concentrated load a

bridge will be likely to encounter, may be estimated at from about 20 to 50 thousand pounds, according to the size of the bridge. This is capable of exerting the greatest strain, when placed at about one-third of the span from one of the abutments, as at b, (*Fig.* 229.) The weakest point of the segment, b g c, is at g, the most distant point from the chord line. The pressure exerted at b by the above weight, may be considered to be in the direction of the chord lines, b a and b c; then, by constructing the parallelogram of forces, e b f d, according to Art. 248, b f will show the pressure in the direction, b c. Then the scantling for the rib may be found by the following rule.

Rule.—Multiply the pressure in pounds in the direction, b c, by the decimal, 0.0016, for white pine, 0.0021 for pitch pine, and 0.0015 for oak, and the product by the decimal representing the sine of the angle, $g \ b \ h$, to a radius of unity. Divide this product by the united breadth in inches of the several ribs, and the cube-root of the quotient, multiplied by the distance, b c, in feet, will give the depth of the rib. Example.-In a bridge of 200 feet span, 15 feet rise, having 3 ribs each 24 inches thick, or 72 inches whole thickness, the pressure in the direction, b c, is found to be 166,000 lbs., and the sine of the angle, $g \ b \ h$, is 0.1—what should be the depth of the rib for white pine? 166,000, multiplied by 0.0016, gives 265.6, which, multiplied by 0.1, gives 26.56; this, divided by 72, gives 0.3689. The cube-root of the last sum is 0.717 nearly, and the distance, b c, is 135 feet: then, 0.717, multiplied by 135, gives 963 inches, the depth required. By this, each rib will require to be 24×97 inches, in order to encounter without injury the greatest possible load.

317.—In constructing these ribs, if the span be not over 50 feet, each rib may be made in two or three thicknesses of timber, (three thicknesses is preferable,) of convenient lengths bolted together; but, in larger spans, where the rib will be such as to render it difficult to procure timber of sufficient breadth, they may be constructed by bending the pieces to the proper curve,

and bolting them together. In this case, where timber of sufficient length to span the opening cannot be obtained, and scarfing is necessary, such joints must be made as will resist both tension and compression, (see Fig. 238.) To ascertain the greatest depth for the pieces which compose the rib, so that the process of bend. ing may not injure their elasticity, multiply the radius of curvature in feet by the decimal, 0.05, and the product will be the depth in Example.—Suppose the curve of the rib to be described inches. with a radius of 100 feet, then what should be the depth? The radius in feet, 100, multiplied by 0.05, gives a product of 5 inches. White pine or oak timber, 5 inches thick, would freely bend to the above curve; and, if the required depth of such a rib be 20 inches, it would have to be composed of at least 4 pieces. Pitch pine is not quite so elastic as white pine or oak-its thickness may be found by using the decimal, 0.046, instead of 0.05.



318.—When the span is over 250 feet, a *framed* rib, formed as in *Fig.* 230, would be preferable to the foregoing. Of this, the upper and the lower edges are formed as just described, by bending the timber to the proper curve. The pieces that tend to the centre of the curve, called *radials*, are notched and bolted on in pairs, and the cross-braces are halved together in the middle, and abut end to end between the radials. The distance between the ribs of a bridge should not exceed about 8 feet. The roadway

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should be supported by vertical standards bolted to the ribs at about every 10 to 15 feet. At the place where they rest on the ribs, a double, horizontal tie should be notched and bolted on the back of the ribs, and also another on the under side; and diagonal braces should be framed between the standards, over the space between the ribs, to prevent lateral motion. The timbers for the roadway may be as light as their situation will admit, as all useless timber is only an unnecessary load upon the arch.

319.-It is found that if a roadway be 18 feet wide, two carriages can pass one another without inconvenience. Its width, therefore, should be either 9, 18, 27 or 36 feet, according to the The width of the foot-path should be 2 feet amount of travel. When a stream of water has a rapid current, for every person. as few piers as practicable should be allowed to obstruct its course; otherwise the bridge will be liable to be swept away by freshets. When the span is not over 300 feet, and the banks of the river are of sufficient height to admit of it, only one arch should be employed. The rise of the arch is limited by the form of the roadway, and by the height of the banks of the river (See Art. 315.) The rise of the roadway should not exceed one in 24 feet, but, as the framing settles about one in 72, the roadway should be framed to rise one in 18, that it may be one in 24 after settling. The commencement of the arch at the abutments-the spring, as it is termed, should not be below high-water mark : and the bridge should be placed at right angles with the course of the current.

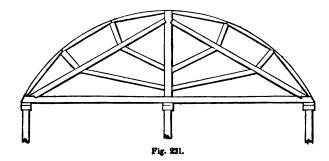
320.—The best material for the abutments and piers of a bridge, is stone; and, if possible, stone should be procured for the purpose. The following rule is to determine the extent of the abutments, they being rectangular, and built with stone weighing 120 lbs. to a cubic-foot. *Rule.*—Multiply the square of the height of the abutment by 160, and divide this product by the weight of a square foot of the arch, and by the rise of the arch; add unity to the quotient, and extract the square-root. Diminish the square-root by unity, and multiply the root, so diminished, by

half the span of the arch, and by the weight of a square-foot of the arch. Divide the last product by 120 times the height of the abutment, and the quotient will be the thickness of the abutment. *Example.*—Let the height of the abutment from the base to the springing of the arch be 20 feet, half the span 100 feet, the weight of a square foot of the arch, including the greatest possible load upon it, 300 pounds, and the rise of the arch 18 feet—what should be its thickness? The square of the height of the abutment, 400, multiplied by 160, gives 64,000, and 300 by 18, gives 5400; 64,000, divided by 5400, gives a quotient of 11.852, one added to this makes 12.852, the square-root of which is 3.6; this, less one, is 2.6; this, multiplied by 100, gives 260, and this again by 300, gives 78,000; this, divided by 120 times the height of the abutment, 2400, gives 32 feet 6 inches, the thickness required.

The dimensions of a pier will be found by the same rule. For, although the thrust of an arch may be balanced by an adjoining arch, when the bridge is finished, and while it remains uninjured; yet, during the erection, and in the event of one arch being destroyed, the pier should be capable of sustaining the entire thrust of the other.

321.—Piers are sometimes constructed of timber, their principal strength depending on piles driven into the earth, but such piers should never be adopted where it is possible to avoid them; for, being alternately wet and dry, they decay much sooner than the upper parts of the bridge. Spruce and elm are considered good for piles. Where the height from the bottom of the river to the roadway is great, it is a good plan to cut them off at a little below low-water mark, cap them with a horizontal tie, and upon this erect the posts for the support of the roadway. This method cuts off the part that is continually wet from that which is only occasionally so, and thus affords an opportunity for replacing the upper part. The pieces which are immersed will last a great length of time, especially when of elm; for it is a well-established fact, that timber is less durable when subject to

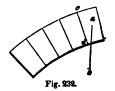
alternate dryness and moisture, than when it is either continually wet or continually dry. It has been ascertained that the piles under London bridge, after having been driven about 600 years, were not materially decayed. These piles are chiefly of elm, and vholly immersed.



322.—Centres for stone bridges. Fig. 231 is a design for a centre for a stone bridge where intermediate supports, as piles driven into the bed of the river, are practicable. Its timbers are so distributed as to sustain the weight of the arch-stones as they are being laid, without destroying the original form of the centre; and also to prevent its destruction or settlement, should any of the piles be swept away. The most usual error in badly-constructed centres is, that the timbers are disposed so as to cause the framing to rise at the crown, during the laying of the arch-stones up the sides. To remedy this evil, some have loaded the crown with heavy stones; but a centre properly constructed will need no such precaution.

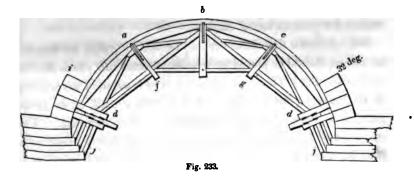
Experiments have shown that an arch-stone does not press upon the centring, until its bed is inclined to the horizon at an angle of from 30 to 45 degrees, according to the hardness of the stone, and whether it is laid in mortar or not. For general purposes, the point at which the pressure commences, may be considered to be at that joint which forms an angle of 32 degrees with the horizon. At this point, the pressure is inconsiderable,

but gradually increases towards the crown. At an angle of 45 degrees, the pressure equals about one-quarter the weight of the stone; at 57 degrees, half the weight; and when a vertical line, as a b, (*Fig.* 232,) passing through the centre of gravity of



the arch-stone, does not fall within its bed, c d, the pressure may be considered equal to the whole weight of the stone. This will be the case at about 60 degrees, when the depth of the stone is double its breadth. The direction of these pressures is considered in a line with the radius of the curve. The weight upon a centre being known, the pressure may be estimated and the timber calculated accordingly. But it must be remembered that the whole weight is never placed upon the framing at once-as seems to have been the idea had in view by the designers of some cen-In building the arch, it should be commenced at each buttres. tress at the same time, (as is generally the case,) and each side should progress equally towards the crown. In designing the framing, the effect produced by each successive layer of stone should be considered. The pressure of the stones upon one side should, by the arrangement of the struts, be counterpoised by that of the stones upon the other side.

323.—Over a river whose stream is rapid, or where it is necessary to preserve an uninterrupted passage for the purposes of navigation, the centre must be constructed without intermediate supports, and without a continued horizontal tie at the base; such a centre is shown at Fig. 233. In laying the stones from the base up to a and c, the pieces, b d and b d, act as ties to prevent any rising at b. After this, while the stones are being laid from a and from c to b, they act as struts: the piece, f g, is added for



additional-security. Upon this plan, with some variation to suit circumstances, centres may be constructed for any span usual in stone-bridge building.

324.—In bridge centres, the principal timbers should abut, and not be intercepted by a suspension or radial piece between. These should be in halves, notched on each side and bolted. The timbers should intersect as little as possible, for the more joints the greater is the settling; and halving them together is a bad practice, as it destroys nearly one-half the strength of the timber. Ties should be introduced across, especially where many timbers meet; and as the centre is to serve but a temporary purpose, the whole should be designed with a view to employ the timber afterwards for other uses. For this reason, all unnecessary cutting should be avoided.

325.—Centres should be sufficiently strong to preserve a staunch and steady form during the whole process of building; for any shaking or trembling will have a tendency to prevent the mortar or cement from *setting*. For this purpose, also, the centre should be lowered a trifle immediately after the key-stone is laid, in order that the stones may take their bearing before the mortar is set; otherwise the joints will open on the under side. The trusses, in centring, are placed at the distance of from 4 to 6 feet apart, according to their strength and the weight of the

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arch. Between every two trusses, diagonal braces should be introduced to prevent lateral motion. TELI

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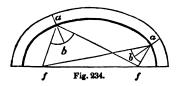
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326.—In order that the centre may be easily lowered, the frames, or trusses, should be placed upon wedge-formed sills; as is shown at d, (Fig. 233.) These are contrived so as to admit of the settling of the frame by driving the wedge, d, with a maul, or, in large centres, a piece of timber mounted as a battering-ram. The operation of lowering a centre should be very slowly performed, in order that the parts of the arch may take their bearing uniformly. The wedge pieces, instead of being placed parallel with the truss, are sometimes made sufficiently long and laid through the arch, in a direction at right angles to that shown at Fig. 233. This method obviates the necessity of stationing men beneath the arch during the process of lowering; and was originally adopted with success soon after the occurrence of an accident, in lowering a centre, by which nine men were killed.

327.—To give some idea of the manner of estimating the pressures, in order to select timber of the proper scantling, calculate the pressure of the arch-stones from i to b, (Fig. 233,) and suppose half this pressure concentrated at a_{1} and acting in the direction, a f. Then, by reference to the laws of pressure and the resistance of timber at Art. 248, 260, &c., the scantlings of the several pieces composing the frame, b d a, may be computed. Again, calculate the pressure of that portion of the arch included between a and c, and consider half of it collected at b, and acting in a vertical direction; then the amount of pressure on the beams, b d and b d, may be found by reference to the first part of this section, as above. Add the pressure of that portion of the arch which is included between i and b to half the weight of the centre, and consider this amount concentrated at d, and acting in a vertical direction; then, by constructing the parallelogram of forces, the pressure upon dj may be ascertained.

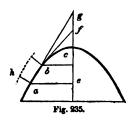
328.—As a short rule for calculating the scantlings of the timbers, let every strut be sufficiently braced, so that it will yield to crushing before it will bend under the pressure—(Art. 261.) Then divide the pressure in pounds by 1000, and the quotient will be the area of the strut in inches. For example, let the pressure upon a strut, in the direction of its axis, be 60,000 lbs. This, divided by 1000, gives 60, the area of the strut in inches; the size of the strut, therefore, might be 6×10 . This rule is based upon experiments by which it has been ascertained, that 1000 pounds is the greatest load that can be trusted upon a square inch of timber, without more indentation than would be compatible with the stability of the framing. The area ascertained by the rule, therefore, must have reference to the actual amount of surface upon which the load bears; and should the strut have a tenon on the end, the area of the shoulders, instead of a section of the whole piece, must be equal to the amount given by the rule.

329.—In the construction of arches, the *voussoirs*, or archstones, are so shaped that the joints between them are perpendicular to the curve of the arch, or to its tangent at the point at which the joint intersects the curve. In a circular arch, the ioints tend toward the centre of the circle: in an elliptical arch, the joints may be found by the following process:

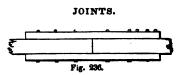


330.—To find the direction of the joints for an elliptical arch. A joint being wanted at a, (Fig. 234) draw lines from that point to the foci, f and f; bisect the angle, f a f, with the line, a b; then a b will be the direction of the joint.

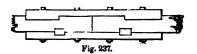
331.— To find the direction of the joints for a parabolic arch. A joint being wanted at a, (Fig. 235,) draw a e, at right angles to the axis, e g; make c g equal to c e, and join a and g; draw ah, at right angles to a g; then ah will be the direction of the joint.



The direction of the joint from b is found in the same manner. The lines, a g and b f, are tangents to the curve at those points respectively; and any number of joints in the curve may be obtained, by first ascertaining the tangents, and then drawing lines at right angles to them.



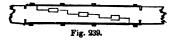
332.—*Fig.* 236 shows a simple and quite strong method of lengthening a tie-beam; but the strength consists wholly in the bolts, and in the friction of the parts produced by screwing the pieces firmly together. Should the timber shrink to even a small degree, the strength would depend altogether on the bolts. It would be made much stronger by indenting the pieces together; as at the upper edge of the tie-beam in *Fig.* 237; or by placing



keys in the joints, as at the lower edge in the same figure. This process, however, weakens the beam in proportion to the depth of the indents.

333.—Fig. 238 shows a method of scarfing, or splicing, a tiebeam without bolts. The keys are to be of well-seasoned, hard

wood, and, if possible, very cross-grained. The addition of bolts would make this a very strong splice, or even white-oak pins would add materially to its strength.



334.—Fig. 239 shows about as strong a splice, perhaps, as can well be made. It is to be recommended for its simplicity; as, on account of their being no oblique joints in it, it can be readily and accurately executed. A complicated joint is the worst that can be adopted; still, some have proposed joints that seem to have little else besides complication to recommend them.

335.—In proportioning the parts of these scarfs, the depths of all the indents taken together should be equal to one-third of the depth of the beam. In oak, ash or elm, the whole length of the scarf should be six times the depth, or thickness, of the beam, when there are no bolts; but, if bolts instead of indents are used, then three times the breadth; and, when both methods are combined, twice the depth of the beam. The length of the scarf in pine and similar soft woods, depending wholly on indents, should be about 12 times the thickness, or depth, of the beam; when depending wholly on bolts, 6 times the breadth; and, when both methods are combined, 4 times the depth.

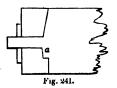


336.—Sometimes beams have to be pieced that are required to resist cross strains—such as a girder, or the tie-beam of a roof when supporting the ceiling. In such beams, the fibres of the

wood in the upper part are compressed; and therefore a simple butt joint at that place, (as in Fig. 240,) is far preferable to any other. In such case, an oblique joint is the very worst. The under side of the beam being in a state of tension, it must be indented or bolted, or both; and an iron plate under the heads of the bolts, gives a great addition of strength.

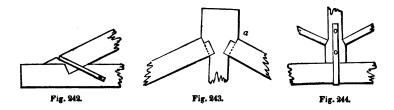
Scarfing requires accuracy and care, as all the indents should bear equally; otherwise, one being strained more than another, there would be a tendency to splinter off the parts. Hence the simplest form that will attain the object, is by far the best. In all beams that are compressed endwise, abutting joints, formed at right angles to the direction of their length, are at once the simplest and the best. For a temporary purpose, *Fig.* 236 would do very well; it would be improved, however, by having a piece bolted on all four sides. *Fig.* 237, and indeed each of the others, since they have no oblique joints, would resist compression well.

337.—In framing one beam into another for bearing purposes, such as a floor-beam into a trimmer, the best place to make the mortice in the trimmer, is in the neutral line, (see Art. 254,) which is in the middle of its depth. Some have thought that, as the fibres of the upper edge are compressed, a mortice migh *t* be made there, and the tenon be driven in tight enough to make the parts as capable of resisting the compression, as they would be without it; and they have therefore concluded that plan to be the best. This could not be the case, even if the tenon would not shrink; for a joint between two pieces cannot possibly be made to resist compression, so well as a solid piece without joints. The proper place, therefore, for the mortice, is at the middle of the depth of the beam; but the best place for the tenon, in the floor-beam, is at its bottom edge. For the nearer this is placed to the upper edge, the greater is the liability for it to splinter off; if the joint is formed, therefore, as at Fig. 241, it will combine all the advantages that can be obtained. Double tenons are objectionable, because the piece framed into is needlessly weakened,



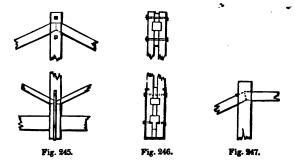
and the tenons are seldom so accurately made as to bear equally. For this reason, unless the tusk at a in the figure fits exactly, so as to bear equally with the tenon, it had better be omitted. And in sawing the shoulders, care should be taken not to saw into the tenon in the least, as it would wound the beam in the place least able to bear it.

338.—Thus it will be seen that framing weakens both pieces, more or less. It should, therefore, be avoided as much as possible; and where it is practicable one piece should rest *upon* the other, rather than be framed into it. This remark applies to the bridging-joists in a framed floor, to the purlins and jack-rafters of a roof, &c.

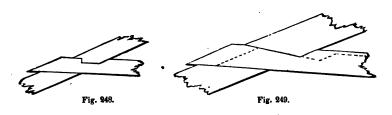


339.—In a framed truss for a roof, bridge, partition, &c., the joints should be so constructed as to direct the pressures through the axes of the several pieces, and also to avoid every tendency of the parts to slide. To attain this object, the abutting surface on the end of a strut should be at right angles to the direction of the pressure; as at the joint shown in *Fig.* 242 for the foot of a rafter, (see *Art.* 257,) in *Fig.* 243 for the head of a rafter, and in *Fig.* 244 for the foot of a strut or brace. The joint at *Fig.* 242 is not cut completely across the tie-beam, but a narrow lip is left

standing in the middle, and a corresponding indent is made in the rafter, to prevent the parts from separating sideways. The abutting surface should be made as large as the attainment of other necessary objects will admit. The iron strap is added to prevent the rafter from sliding out, should the end of the tie-beam, by decay or otherwise, splinter off. In making the joint shown at Fig. 243, it should be left a little open at a, so as to bring the parts to a fair bearing at the settling of the truss, which must necessarily take place from the shrinking of the king-post and other parts. If the joint is made fair at first, when the truss settles it will cause it to open at the under side of the rafter, thus throwing the whole pressure upon the sharp edge at a. This will cause an indentation in the king-post, by which the truss will be made to settle further; and this pressure not being in the axis of the rafter, it will be greatly increased, thereby rendering the rafter liable to split and break.



340.—If the rafters and struts were made to abut end to end, as in Fig. 245, 246 and 247, and the king or queen post notched on in halves and bolted, the ill effects of shrinking would be avoided. This method has been practised with success, in some of the most celebrated bridges and roofs in Europe; and, were its use adopted in this country, the unseemly sight of a *hogged* ridge would seldom be met with. A plate of cast iron between the abutting surfaces, will equalize the pressure.



341.—Fig. 248 is a proper joint for a collar-beam in a small roof: the principle shown here should characterize all tie-joints. The dovetail joint, although extensively practised in the above and similar cases, is the very worst that can be employed. The shrinking of the timber, if only to a small degree, permits the tie to withdraw—as is shown at Fig. 249. The dotted line shows the position of the tie after it has shrunk.

342.—Locust and white-oak pins are great additions to the strength of a joint. In many cases, they would supply the place of iron bolts; and, on account of their small cost, they should be used in preference wherever the strength of iron is not requisite. In small framing, good cut nails are of great service at the joints; but they should not be trusted to bear any considerable pressure, as they are apt to be brittle. Iron straps are seldom necessary, as all the joinings in carpentry may be made without them. They can be used to advantage, however, at the foot of suspending-pieces, and for the rafter at the end of the tie-beam. In roofs for ordinary purposes, the iron straps for suspending-pieces may be as follows: When the longest unsupported part of the tie-beam is

10 feet	, the stra	ap may be	1 inch	wide by	18 t	hick.
15	"	"	$1\frac{1}{2}$	"	4	"
20	"	"	2	"	1 .	"

In fastening a strap, its hold on the suspending-piece will be much increased, by turning its ends into the wood. Iron straps should be protected from rust; for thin plates of iron decay very soon,

especially when exposed to dampness. For this purpose, as soon as the strap is made, let it be heated to about a blue heat, and, while it is hot, pour over its entire surface raw linseed oil, or rub it with beeswax. Either of these will give it a coating which dampness will not penetrate.

SECTION V.—DOORS, WINDOWS, &c.

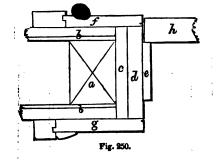
DOORS.

343.---Among the several architectural arrangements of an edifice, the door is by no means the least in importance; and, if properly constructed, it is not only an article of use, but also of ornament, adding materially to the regularity and elegance of the apartments. The dimensions and style of finish of a door, should be in accordance with the size and style of the building, or the apartment for which it is designed. As regards the utility of doors, the principal door to a public building should be of sufficient width to admit of a free passage for a crowd of people; while that of a private apartment will be wide enough, if it permit one person to pass without being incommoded. Experience has determined that the least width allowable for this is 2 feet 8 inches; although doors leading to inferior and unimportant rooms may, if circumstances require it, be as narrow as 2 feet 6 inches; and doors for closets, where an entrance is seldom required, may be but 2 feet wide. The width of the principal door to a public building may be from 6 to 12 feet, according to the size of the building; and the width of doors for a dwelling may be from 2 feet 8 inches, to 3 feet 6 inches. If the importance of an apartment in a dwelling be such as to require a door of greater width

than 3 feet 6 inches, the opening should be closed with two doors, or a door in two folds; generally, in such cases, where the opening is from 5 to 8 feet, folding or sliding doors are adopted. As to the height of a door, it should no case be less than about 6 feet 3 inches; and generally not less than 6 feet 8 inches.

344.—The proportion between the width and height of single doors, for a dwelling, should be as 2 is to 5; and, for entrancedoors to public buildings, as 1 is to 2. If the width is given and the height required of a door for a dwelling, multiply the width by 5, and divide the product by 2; but, if the height is given and the width required, divide by 5, and multiply by 2. Where two or more doors of different widths show in the same room, it is well to proportion the dimensions of the more important by the above rule, and make the narrower doors of the same height as the wider ones; as all the doors in a suit of apartments, except the folding or sliding doors, have the best appearance when of one height. The proportions for folding or sliding doors should be such that the width may be equal to $\frac{4}{5}$ of the height; yet this rule needs some qualification : for, if the width of the opening be greater than one-half the width of the room, there will not be a sufficient space left for opening the doors; also, the height should be about one-tenth greater than that of the adjacent single doors.

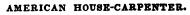
345.—Where doors have but two panels in width, let the stiles and muntins be each $\frac{1}{7}$ of the width; or, whatever number of panels there may be, let the united widths of the stiles and the muntins, or the whole width of the solid, be equal to $\frac{3}{7}$ of the width of the door. Thus: in a door, 35 inches wide, containing two panels in width, the stiles should be 5 inches wide; and in a door, 3 feet 6 inches wide, the stiles should be 6 inches. If a door, 3 feet 6 inches wide, is to have 3 panels in width, the stiles and muntins should be each $4\frac{1}{2}$ inches wide, each panel being 8 inches. The bottom rail and the lock rail ought to be each equal in width to $\frac{1}{10}$ of the height of the door; and the top rail, and all others, of the same width as the stiles. The moulding on the panel should be equal in width to $\frac{1}{4}$ of the width of the stile.

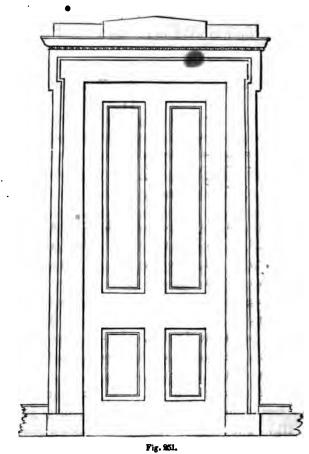


346.—Fig. 250 shows an approved method of trimming doors: a is the door stud; b, the lath and plaster; c, the ground; d, the jamb; e, the stop; f and g, architrave casings; and h, the door stile. It is customary in ordinary work to form the stop for the door by rebating the jamb. But, when the door is thick and heavy, a better plan is to nail on a piece as at e in the figure. This piece can be fitted to the door, and put on after the door is hung; so, should the door be a trifle winding, this will correct the evil, and the door be made to shut solid.

347.—Fig. 251 is an elevation of a door and trimmings suitable for the best rooms of a dwelling. (For trimmings generally, see Sect. III.) 'The number of panels into which a door should be divided, is adjusted at pleasure; yet the present style of finishing requires, that the number be as small as a proper regard for strength will admit. In some of our best dwellings, doors have been made having only two upright panels. A few years experience, however, has proved that the omission of the lock rail is at the expense of the strength and durability of the door; a four-panel door, therefore, is the best that can be made.

348.—The doors of a dwelling should all be hung so as to open into the principal rooms; and, in general, no door should be hung to open into the hall, or passage. As to the proper edge of the door on which to affix the hinges, no general rule can be assigned.





It may be observed, however, that a bed-room door should be hung so that, when half open, it will screen the bed; and a door leading from a hall, or passage, to a principal room, should screen the fire.

WINDOWS.

349.—A window should be of such dimensions, and in such a position, as to admit a sufficiency of light to that part of the apartment for which it is designed. No definite rule for the size

DOORS, WINDOWS, &C.

can well be given, that will answer in all cases; yet, as an approximation, the following has been used for general purposes. Multiply together the length and the breadth in feet of the apartment to be lighted, and product by the height in feet; then the square-root of this product will show the required number of square feet of glass.

350.—To ascertain the dimensions of window frames, add $4\frac{1}{2}$ inches to the width of the glass for their width, and $6\frac{1}{2}$ inches to the height of the glass for their height. These give the dimensions, in the clear, of ordinary frames for 12-light windows; the height being taken at the inside edge of the sill. In a brick wall, the width of the opening is 8 inches more than the width of the glass.— $4\frac{1}{2}$ for the stiles of the sash, and $3\frac{1}{2}$ for hanging stiles—and the height between the stone sill and lintel is about $10\frac{1}{2}$ inches more than the height of the glass, it being varied according to the thickness of the sill of the frame.

351.-In hanging inside shutters to fold into boxes, it is necessary to have the box shutter about one inch wider than the flap, in order that the flap may not interfere when both are folded into the box. The usual margin shown between the face of the shutter when folded into the box and the quirk of the stop bead, or edge of the casing, is half an inch; and, in the usual method of letting the whole of the thickness of the butt hinge into the edge of the box shutter, it is necessary to make allowance for the throw of the hinge. This may, in general, be estimated at $\frac{1}{2}$ of an inch at each hinging; which being added to the margin, the entire width of the shutters will be 11 inches more than the width of the frame in the clear. Then, to ascertain the width of the box shutter, add 11 inches to the width of the frame in the clear, between the pulley stiles; divide this product by 4, and add half an inch to the quotient; and the last product will be the required width. For example, suppose the window to have 3 lights in width, 11 inches each. Then, 3 times 11 is 33, and 41 added for the wood of the sash, gives $37\frac{1}{2}$ ----- $37\frac{1}{2}$ and $1\frac{1}{2}$ is 39,

and 39, divided by 4, gives $9\frac{3}{4}$; to which add half an inch, and the result will be 10 $\frac{1}{4}$ inches, the width required for the box shutter.

352.—In disposing and proportioning windows for the walls of a building, the rules of architectural three require that they be of different heights in different stories, but of the same width. The windows of the upper stories should all range perpendicularly over those of the first, or principal, story; and they should be disposed so as to exhibit a balance of parts throughout the front of the building. To aid in this, it is always proper to place the front door in the middle of the front of the building; and, where the size of the house will admit of it, this plan should be adopted. (See the latter part of Art. 214.) The proportion that the height should bear to the width, may be, in accordance with general usage, as follows :

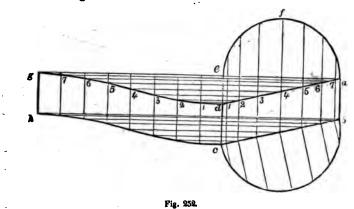
The height of basement windows, 11 of the width.

"	"	principal-story	"	2¦	u .	
"	"	second-story	"	17	Ľ	
"	"	third-story	"	13	Ľ	
"	u	fourth-story	"	1‡	"	
ĸ	u	attic-story	"	the sa	me as the width.	,

But, in determining the height of the windows for the several stories, it is necessary to take into consideration the height of the story in which the window is to be placed. For, in addition to the height from the floor, which is generally required to be from 28 to 30 inches, room is wanted above the head of the window for the window-trimming and the cornice of the room, besides some respectable space which there ought to be between these.

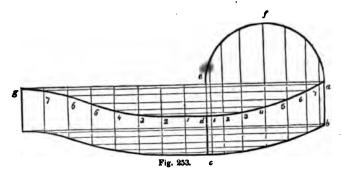
353.—'The present style of finish requires the heads of windows in general to be horizontal, or *square-headed*; yet, it is well to be possessed of information for trimming circular-headed windows, as repairs of these are occasionally needed. If the jambs of a door or window be placed at right angles to the face of the wall, the edges of the *soffit*, or surface of the head, would be straight, and its length be found by getting the stretch-out of the

circle, (Art. 92;) but, when the jambs are placed obliquely to the face of the wall, occasioned by the demand for light in an oblique direction, the form of the soffit will be obtained as in the following article: and, when the face of the wall is circular, as in the succeeding one.



354.—To find the form of the soffit for circular windowheads, when the light is received in an oblique direction. Let a b c d, (Fig. 252,) be the ground-plan of a given window, and efa, a vertical section taken at right angles to the face of the jambs. From a, through e, draw ag, at right angles to a b; obtain the stretch-out of ef a, and make eg equal to it; divide eg and ef a, each into a like number of equal parts, and drop perpendiculars from the points of division in each; from the points of intersection, 1, 2, 3, &c., in the line, ad, draw horizontal lines to meet corresponding perpendiculars from eg; then those points of intersection will give the curve line, dg, which will be the one required for the edge of the soffit. The other edge, ch, is found in the same manner.

355.—To find the form of the soffit for circular windowheads, when the face of the wall is curved. Let a b c d, (Fig. 253,) be the ground-plan of a given window, and e f a, a vertical section of the head taken at right angles to the face of the jambs.



Proceed as in the foregoing article to obtain the line, d g; then that will be the curve required for the edge of the soffit; the other edge being found in the same manner.

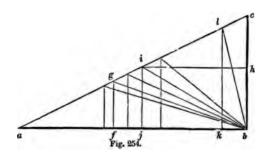
If the given vertical section be taken in a line with the face of the wall, instead of at right angles to the face of the jambs, place it upon the line, $c \ b$, (*Fig.* 252;) and, having drawn ordinates at right angles to $c \ b$, transfer them to $e \ f \ a \ ;$ in this way, a section at right angles to the jambs can be obtained.

SECTION VI.—STAIRS.

356.—The STAIRS is that mechanical arrangement in a building by which access is obtained from one story to another. Their position, form and finish, when determined with discriminating taste, add greatly to the comfort and elegance of a structure. As regards their position, the first object should be to have them near the middle of the building, in order that an equally easy access may be obtained from all the rooms and passages. Next in importance is light; to obtain which they would seem to be best situated near an outer wall, in which windows might be constructed for the purpose; yet a sky-light, or opening in the roof, would not only provide light, and so secure a central position for the stairs, but may be made, also, to assist materially as an ornament to the building, and, what is of more importance, afford an opportunity for better ventilation.

357.—It would seem that the length of the raking side of the *pitch-board*, or the distance from the top of one riser to the top of the next, should be about the same in all cases; for, whether stairs be intended for large buildings or for small, for public or for private, the accommodation of men of the same stature is to be consulted in every instance. But it is evident that, with the same effort, a longer step can be taken on level than on rising ground;

and that, although the tread and rise cannot be proportioned merely in accordance with the style and importance of the building, yet this may be done according to the angle at which the flight rises. If it is required to ascend gradually and easy, the length from the top of one rise to that of another, or the hypothenuse of the pitch-board, may be long; but, if the flight is steep, the length must be shorter. Upon this data the following problem is constructed.



358.—To proportion the rise and tread to one another. Make the line, a b, (Fig. 254,) equal to 24 inches; from b, erect b c, at right angles to a b, and make b c equal to 12 inches; join σ and c, and the triangle, a b c, will form a scale upon which t σ graduate the sides of the pitch-board. For example, suppose a very easy stairs is required, and the tread is fixed at 14 inches. Place it from b to f, and from f; draw f g, at right angles to a b; then the length of fg will be found to be 5 inches, which is a proper rise for 14 inches tread, and the angle, f b g, will show the degree of inclination at which the flight will ascend. But, in a majority of instances, the height of a story is fixed, while the length of tread, or the space that the stairs occupy on the lower floor, is optional. The height of a story being determined, the height of each rise will of course depend upon the number into which the whole height is divided; the angle of ascent being more easy if the number be great, than if it be smaller. By dividing

the whole height of a story into a certain number of rises, suppose the length of each is found to be 6 inches. Place this length from b to h, and draw h i, parallel to a b; then h i, or b j will be the proper tread for that rise, and j b i will show the angle of ascent. On the other hand, if the angle of ascent be given, as a b l, (b l being $10\frac{1}{2}$ inches, the proper length of run for a stepladder,) drop the perpendicular, l k, from l to k; then l k b will be the proper proportion for the sides of a pitch-board for that run.

359.—The angle of ascent will vary according to circumstances. The following treads will determine about the right inclination for the different classes of buildings specified.

In public edifices,	tread about	14	inches.
In first-class dwellings	"	12]	"
In second-class "	**	11	"
In third-class " and cotta	iges "	9	"

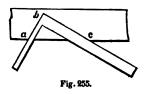
Step-ladders to ascend to scuttles, &c., should have from 10 to 11 inches *run* on the rake of the string. (See notes at Art. 103.)

360.—The length of the steps is regulated according to the extent and importance of the building in which they are placed, varying from 3 to 12 feet, and sometimes longer. Where two persons are expected to pass each other conveniently, the shortest length that will admit of it is 3 feet; still, in crowded cities where land is so valuable, the space allowed for passages being very small, they are frequently executed at $2\frac{1}{2}$ feet.

361.—To find the dimensions of the pitch-board. The first thing in commencing to build a stairs, is to make the pitch-board; this is done in the following manner. Obtain very accurately, in feet and inches, the perpendicular height of the story in which the stairs are to be placed. This must be taken from the top of the floor in the lower story to the top of the floor in the upper story. Then, to obtain the number of rises, the height in inches thus obtained must be divided by 5, 6, 7, 8, or 9, according to the quality and style of the building in which the stairs are to be

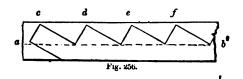
built. For instance, suppose the building to be a first-class dwelling, and the height ascertained is 13 feet 4 inches, or 160 inches. The proper rise for a stairs in a house of this class is about 6 inches. Then, 160 divided by 6, gives 261 inches. This being nearer 27 than 26, the number of risers, should be 27. Then divide the height, 160 inches, by 27, and the quotient will give the height of one rise. On performing this operation, the quotient will be found to be 5 inches, $\frac{1}{16}$ and $\frac{1}{16}$ of an inch.

Then, if the space for the extension of the stairs is not limited, the tread can be found as at Art. 358. But, if the contrary is the case, the whole distance given for the treads must be divided by the number of treads required. On account of the upper floor forming a step for the last riser, the number of treads is always one less than the number of risers. Having obtained this rise and tread, the pitch-board may be made in the following manner. Upon a piece of well-seasoned board about $\frac{5}{4}$ of an inch thick, having one edge jointed straight and square, lay the corner of a carpenters'-square, as shown at Fig. 255. Make *a b*

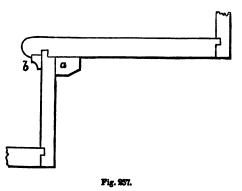


equal to the rise, and b c equal to the tread; mark along those edges with a knife, and cut it out by the marks, making the edges perfectly square. The grain of the wood must run in the direction indicated in the figure, because, if it shrinks a trifle, the rise and the tread will be equally affected by it. When a pitch-board is first made, the dimensions of the rise and tread should be preserved in figures, in order that, should the first shrink, a second could be made.

362.—To lay out the string. The space required for timber



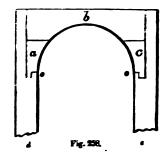
and plastering under the steps, is about 5 inches for ordinary stairs; set a gauge, therefore, at 5 inches, and run it on the lower edge of the plank, as $a \ b$, (Fig. 256.) Commencing at one end, lay the longest side of the pitch-board against the gauge-mark, ab, as at c, and draw by the edges the lines for the first rise and tread; then place it successively as at d, e and f, until the required number of risers shall be laid down.



363.—Fig. 257 represents a section of a step and riser, joined after the most approved method. In this, a represents the end of a block about 2 inches long, two of which are glued in the corner in the length of the step. The cove at b is planed up square, glued in, and *stuck* after the glue is set.

PLATFORM STAIRS.

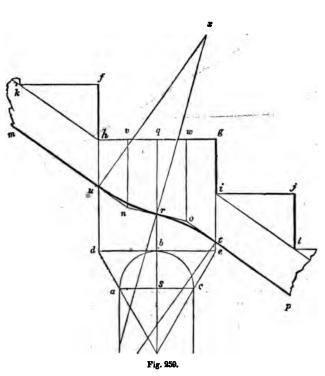
364.—A platform stairs ascends from one story to another in two or more flights, having platforms between for resting and to change their direction. This kind of stairs is the most easily constructed, and is therefore the most common. The cylin-



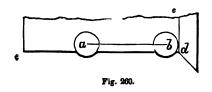
der is generally of small diameter, in most cases about 6 inches. It may be worked out of one solid piece, but a better way is to glue together three pieces, as in Fig. 258; in which the pieces, a, b and c, compose the cylinder, and d and e represent parts of the strings. The strings, after being glued to the cylinder, are secured with screws. The joining at o and o is the most proper for that kind of joint.

365.—To obtain the form of the lower edge of the cylinder. Find the stretch-out, de, (Fig. 259,) of the face of the cylinder, a b c, according to Art. 92; from d and e, draw d f and e g, at right angles to d e; draw h g, parallel to d e, and make h f and g i, each equal to one rise; from i and f, draw i j and f k, parallel to hg; place the tread of the pitch-board at these last lines, and draw by the lower edge the lines, k h and i l; parallel to these, draw m n and o p, at the requisite distance for the dimensions of the string; from s, the centre of the plan, draw s q, parallel to df; divide hq and qg, each into 2 equal parts, as at v and w; from v and w, draw v n and w o, parallel to f d; join nand o, cutting $q s ext{ in } r$; then the angles, u n r and r o t, being eased off according to Art. 89, will give the proper curve for the bottom edge of the cylinder. A centre may be found upon which to describe these curves thus : from u, draw u x, at right angles to mn; from r, draw rx, at right angles to no; then x will be the centre for the curve, u r. The centre for the curve, r t, is found in the same manner.

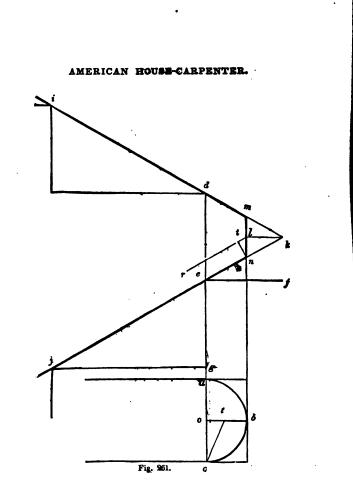




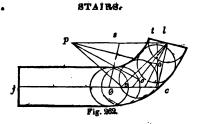
366.—To find the position for the balusters. Place the centre of the first baluster, $(b. Fig. 260,) \frac{1}{2}$ its diameter from the face of the riser, c d, and $\frac{1}{2}$ its diameter from the end of the step, e d; and place the centre of the other baluster, a, half the tread from the centre of the first. The centre of the rail must be placed over the centre of the balusters. Their usual length is 2 feet 5 inches, and 2 feet 9 inches, for the short and the long balusters respectively.







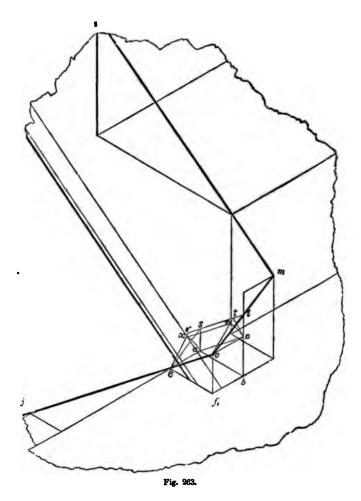
367.— To find the face-mould for a round hand-rail to platform stairs. CASE 1.— When the cylinder is small. In Fig. 261, j and e represent a vertical section of the last two steps of the first flight, and d and i the first two steps of the second flight, of a platform stairs, the line, e f, being the platform; and a b c is the plan of a line passing through the centre of the rail around the cylinder. Through i and d, draw i k, and through j and e, draw j k; from k, draw k l, parallel to f e; from b, draw b m, parallel to g d; from l, draw l r, parallel to k j; from n, draw nt, at right angles to j k; on the line, o b, make o t equal to n t; join c and t: on the line, j c, (Fig. 262,) make e c equal to e n at Fig. 261; from c, draw c t, at right angles to j c, and make c t



equal to c t at Fig. 261; through t, draw p l, parallel to j c, and make t l equal to t l at Fig. 261; join l and c, and complete the parallelogram, e c l s; find the points, o, o, o, according to Art. 118; upon e, o, o, o, and l, successively, with a radius equal to half the width of the rail, describe the circles shown in the figure; then a curve traced on both sides of these circles and just touching them, will give the proper form for the mould. The joint at l is drawn at right angles to c l.

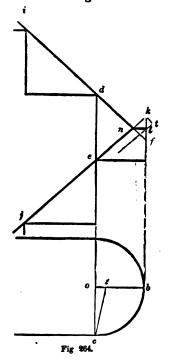
368.-Elucidation of the foregoing method. This excellent plan for obtaining the face-moulds for the hand-rail of a platform stairs, has never before been published. It was communicated to me by an eminent stair-builder of this city : and having seen rails put up from it, I am enabled to give it my unqualified recommendation. In order to have it fully understood, I have introduced Fig. 263; in which the cylinder, for this purpose, is made rectangular instead of circular. The figure gives a perspective view of a part of the upper and of the lower flights, and a part of the platform about the cylinder. The heavy lines, i m, m c and c j, show the direction of the rail, and are supposed to pass through the centre of it. When the rake of the second flight is the same as that of the first, which is here and is generally the case, the face-mould for the lower twist will, when reversed, do for the upper flight: that part of the rail, therefore, which passes from e to c and from c to l, is all that will need explanation.

Suppose, then, that the parallelogram, $e \ a \ o \ c$, represent a plane lying perpendicularly over $e \ a \ b \ f$, being inclined in the direction, $e \ c$, and level in the direction, $c \ o$; suppose this plane, $e \ a \ o \ c$,



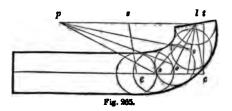
be revolved on ec as an axis, in the manner indicated by the arcs, on and ax, until it coincides with the plane, ertc; the line, a o, will then be represented by the line, xn; then add the parallelogram, xrtn, and the triangle, ctl, deducting the triangle, ers; and the edges of the plane, eslc, inclined in the direction, ec, and also in the direction, cl, will lie perpendicularly over the plane, eabf. From this we gather that the line, co, being at right angles to

nst, in order to reach the point, l, be lengthened the distance, and the right angle, $e \ c \ t$, be made obtuse by the addition to he angle, $t \ c \ l$. By reference to Fig. 261, it will be seen his lengthening is performed by forming the right-angled le, $c \ o \ t$, corresponding to the triangle, $c \ o \ t$, in Fig. 263. ine, $c \ t$, is then transferred to Fig. 262, and placed at right s to $e \ c$; this angle, $e \ c \ t$, being increased by adding the an $c \ l$, corresponding to $t \ c \ l$, Fig. 263, the point, l, is reached, a proper position and length of the lines, $e \ c \ and \ c \ l$ ob-L. To obtain the face-mould for a rail over a cylindrical sole, the same process is necessary to be followed until the ngth and position of these lines are found; then, by forming urallelogram, $e \ c \ l \ s$, and describing a quarter of an ellipse n, the proper form will be given.

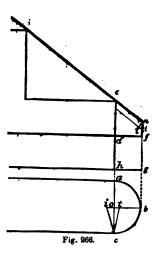


-CASE 2. When the cylinder is large. Fig. 264 re-

presents a plan and a vertical section of a line passing through the centre of the rail as before. From b, draw b k, parallel to c d; extend the lines, i d and j e, until they meet k b in k and f; from n, draw n l, parallel to o b; through l, draw l t, parallel to j k; from k, draw k t, at right angles to j k; on the line, o b, make o t equal to k t. Make e c, (Fig. 265.) equal to e k at Fig. 264; from c,



draw c t, at right angles to e c, and equal to c t at Fig. 264; from t, draw t p, parallel to c e, and make t l equal to t l at Fig. 264; complete the parallelogram, e c l s, and find the points, o, o, o, as before; then describe the circles and complete the mould as in Fig. 262. The difference between this and Case 1 is, that the line, c t, instead of being raised and thrown out, is lowered and drawn in.



370.-CASE 3.- Where the rake meets the level. In Fig.

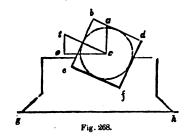
266, a b c is the plan of a line passing through the centre of the rail around the cylinder as before, and j and e is a vertical section of two steps starting from the floor, h g. Bisect e h in d, and through d, draw d f, parallel to h g; bisect f n in l, and from l, draw l t, parallel to n j; from n, draw n t, at right angles to j n; on the line, o b, make o t equal to n t. Then, to obtain a mould for the twist going up the flight, proceed as at Fig. 262; making e c in that figure equal to e n in Fig. 266, and the other lines of a length and position such as is indicated by the letters of reference in each figure. To obtain the mould for the level rail, extend b o, (Fig. 266,) to i; make o i equal to f l, and join i and c; make c i, (Fig. 267,) equal to c i at Fig. 266; through c, draw c d, at



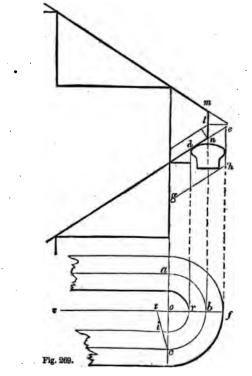
right angles to ci; make dc equal to df at Fig. 266, and complete the parallelogram, odci; then proceed as in the previous cases to find the mould.

371.—All the moulds obtained by the preceding examples have been for round rails. For these, the mould may be applied to a plank of the same thickness as the rail is intended to be, and the plank sawed square through, the joints being cut square from the face of the plank. A twist thus cut and truly rounded will hang in a proper position over the plan, and present a perfect and graceful wreath.

372.—To bore for the balusters of a round rail before rounding it. Make the angle, o c t, (Fig. 268,) equal to the angle, o c t, at Fig. 261; upon c, describe a circle with a radius equal to half the thickness of the rail; draw the tangent, b d, parallel to t c, and complete the rectangle, e b d f, having sides tangical to the circle; from c, draw c a, at right angles to o c; then, b dbeing the bottom of the rail, set a gauge from b to a, and run it the whole length of the stuff; in boring, place the centre of the



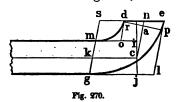
bit in the gauge-mark at a, and bore in the direction, a c. To do this easily, make *chucks* as represented in the figure, the bottom edge, g h, being parallel to o c, and having a place sawed out, as e f, to receive the rail. These being nailed to the bench, the rail will be held steadily in its proper place for boring vertically. The distance apart that the balusters require to be, on the under side of the rail, is one-half the length of the *rake-side* of the pitch-board.



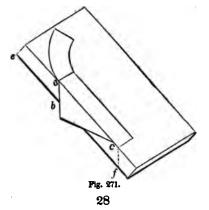
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373.—To obtain, by the foregoing principles, the face-mould for the twists of a moulded rail upon platform stairs. In Fig. 269, a b c is the plan of a line passing through the centre of the rail around the cylinder as before, and the lines above it are a vertical section of steps, risers and platform, with the lines for the rail obtained as in Fig. 261. Set half the width of the rail from b to f and from b to r, and from f and r, draw f e and r d, parallel to c a. At Fig. 270, the centre lines of the



rail, k c and c n, are obtained as in the previous examples. Make c i and c j, each equal to c i at Fig. 269, and draw the lines, im and j g, parallel to c k; make n e and n d equal to n e and n d at Fig. 269, and draw d o and e l, parallel to n c; also, through k, draw s g, parallel to n c; then, in the parallelograms, m s d o and g s e l, find the elliptic curves, d m and e g, according to Art. 118, and they will define the curves. The line, d e, being drawn through n parallel to k c, defines the joint, which is to be cut through the plank vertically. If the rail crosses the platform rather steep, a butt joint will be preferable, to obtain which see Art. 405.



374.—To apply the mould to the plank. The mould obtained according to the last article must be applied to both sides of the plank, as shown at Fig. 271. Before applying the mould, the edge, ef, must be bevilled according to the angle, ctx, at Fig. 269; if the rail is to be canted up, the edge must be bevilled at an obtuse angle with the upper face; but if it is to be canted down, the angle that the edge makes with the upper face must be acute. From the spring of the curve, a, and the end, c, fraw vertical lines across the edge of the plank by applying the pitchboard, a b c; then, in applying the mould to the other side, place the points, a and c, at b and f; and, after marking around it, saw the rail out vertically. After the rail is sawed out, the bottom and the top surfaces must be squared from the sides.

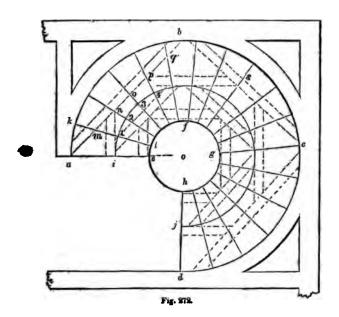
375.—To ascertain the thickness of stuff required for the twists. The thickness of stuff required for the twists of a round rail, as before observed, is the same as that for the straight; but for a moulded rail, the stuff for the twists must be thicker than that for the straight. In Fig. 269, draw a section of the rail between the lines, dr and ef, and as close to the line, de, as possible; at the lower corner of the section, draw gh, parallel to de; then the distance that these lines are apart, will be the thickness required for the twists of a moulded rail.

The foregoing method of finding moulds for rails is applicable to all stairs which have continued rails around cylinders, and are without winders.

WINDING STAIRS.

376.—Winding stairs have steps tapering narrower at one end than at the other. In some stairs, there are steps of parallel width incorporated with tapering steps; the former are then called *flyers* and the latter *winders*.

377.—To describe a regular geometrical winding stairs. In Fig. 272, a b c d represents the inner surface of the wall enclosing the space allotted to the stairs, a e the length of the steps, and e f g h the cylinder, or face of the front string. The line,

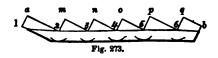


 $a e_{i}$ is given as the face of the first riser, and the point, j_{i} for the limit of the last. Make e i equal to 18 inches, and upon o, with o i for radius, describe the arc, i j; obtain the number of risers and of treads required to ascend to the floor at j, according to Art. 361, and divide the arc, *i j*, into the same number of equal parts as there are to be treads; through the points of division, 1, 2, 3, &c., and from the wall-string to the front-string, draw lines tending to the centre, o; then these lines will represent the face of each riser, and determine the form and width of the steps. Allow the necessary projection for the nosing beyond a e, which should be equal to the thickness of the step, and then a e l k will be the dimensions for each step. Make a pitch-board for the wall-string having a k for the tread, and the rise as previously ascertained; with this, lay out on a thicknessed plank the several risers and treads, as at Fig. 256, gauging from the upper edge of the string for the line at which to set the pitch-board.

Upon the back of the string, with a $1\frac{1}{4}$ inch dado plane, make

a succession of grooves $1\frac{1}{4}$ inches apart, and parallel with the lines for the risers on the face. These grooves must be cut along the whole length of the plank, and deep enough to admit of the plank's bending around the curve, $a \ b \ c \ d$. Then construct a drum, or cylinder, of any common kind of stuff, and made to fit a curve having a radius the thickness of the string less than $o \ a$; upon this the string must be bent, and the grooves filled with strips of wood, called *keys*, which must be very nicely fitted and glued in. After it has dried, a board thin enough to bend around on the outside of the string, must be glued on from one end to the other, and nailed with clout nails. In doing this, be careful not to nail into any place where a riser or step is to enter on the face.

After the string has been on the drum a sufficient time for the glue to set, take it off, and cut the mortices for the steps and risers on the face at the lines previously made; which may be done by boring with a centre-bit half through the string, and nicely chiseling to the line. The drum need not be made so large as the whole space occupied by the stairs, but merely large enough to receive one piece of the wall-string at once—for it is evident that more than one will be required. The front string may be constructed in the same manner; taking e l instead of a k for the tread of the pitch-board, dadoing it with a smaller dado plane, and bending it on a drum of the proper size.

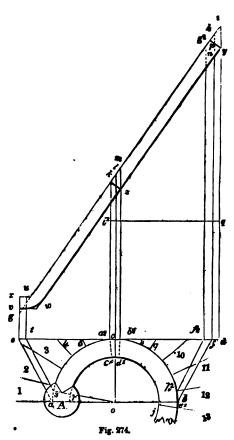


378.—To find the shape and position of the timbers necessary to support a winding stairs. The dotted lines in Fig. 272 show the proper position of the timbers as regards the plan: the shape of each is obtained as follows. In Fig. 273, the line, 1 a, is equal to a riser, less the thickness of the floor, and the lines, 2 m, 3 n, 4 o, 5 p and 6 q, are each equal to one riser. The.

line, a 2, is equal to a m in Fig. 272, the line, m 3 to m n in that figure, &c. In drawing this figure, commence at a, and make the lines, a 1 and a 2, of the length above specified, and draw them at right angles to each other; draw 2 m, at right angles to a 2, and m 3, at right angles to m 2, and make 2 m and m 3 of the lengths as above specified; and so proceed to the end. Then, through the points, 1, 2, 3, 4, 5 and 6, trace the line, 1 b; upon the points, 1, 2, 3, 4, &c., with the size of the timber for radius, describe arcs as shown in the figure, and by these the lower line may be traced parallel to the upper. This will give the proper shape for the timber, a b, in Fig. 272; and that of the others may be found in the same manner. In ordinary cases, the shape of one face of the timber will be sufficient, for a good workman can easily hew it to its proper level by that; but where great accuracy is desirable, a pattern for the other side may be found in the same manner as for the first.

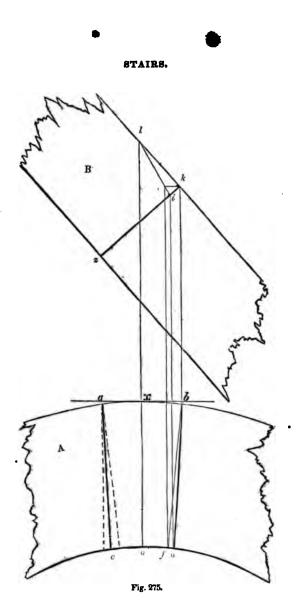
379.—To find the falling-mould for the rail of a winding stairs. In Fig. 274, a c b represents the plan of a rail around half the cylinder, A the cap of the newel, and 1, 2, 3, &c., the face of the risers in the order they ascend. Find the stretch-out, ef, of a c b, according to Art. 92; from o, through the point of the mitre at the newel-cap, draw os; obtain on the tangent, ed, the position of the points, s and h^2 ,* as at t and f^2 ; from etf^2 and f, draw ex, tu, f^2g^2 and fh, all at right angles to ed; make egequal to one rise and f^2g^3 equal to 12, as this line is drawn from the 12th riser; from g, through g^2 , draw gi; make gx equal to about three-fourths of a rise, (the top of the newel, x, should be $3\frac{1}{2}$ feet from the floor;) draw xu, at right angles to ex, and ease off the angle at u; at a flistance equal to the thickness of

[•] In the above, the references, a^2 , b^2 , &c;, are introduced for the first time. During the time taken to refer to the figure, the memory of the *form* of these may pass from the mind, while that of the sound alone remains; they may then be mistaken for a^2 , b^2 , &c. This can be avoided in reading by giving them a sound corresponding to their meaning, which is arread by first or a second beyond



the rail, draw v w y, parallel to x u i; from the centre of the plan, o, draw o l, at right angles to e d; bisect h n in p, and through p, at right angles to g i, draw a line for the joint; in the same manner, draw the joint at k; then x y will be the falling-mould for that part of the rail which extends from s to b on the plan.

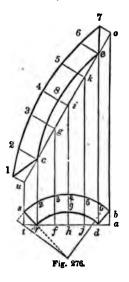
380.—To find the face-mould for the rail of a winding-stairs. From the extremities of the joints in the falling-mould, as k, zand y, (Fig. 274,) draw $k a^2, z b^2$ and y d, at right angles to e d; make $b e^2$ equal to f d. Then, to obtain the direction of the joint, $a^2 c^2$, or $b^2 d^2$, proceed as at Fig. 275, at which the parts are



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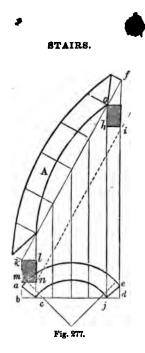
wn at half their full size. A is the plan of the rail, and B is falling-mould; in which k z is the direction of the butt-joint. m k, draw k b, parallel to l o, and k e, at right angles to k b; n b, draw b f, tending to the centre of the plan, and from f, draw parallel to b k; from l, through e, draw l i, and from i, draw iarallel to e f; join d and b, and d b will be the proper direction

for the joint on the plan. The direction of the joint on the other side, a c, can be found by transferring the distances, x france; to x a and o c. (See Art. 384.)



Having obtained the direction of the joint, make s r d b, (Fig. 276,) equal to $s r d^2 b^3$ in Fig. 274; through r and d, draw t a; through s and from d, draw t u and d e, at right angles to t a; make t u and d e equal to t u and $b^2 m$, respectively, in Fig. 274; from u, through e, draw u o; through b, from r, and from as many other points in the line, t a, as is thought necessary, as f, h and j, draw the ordinates, r c, f g, h i, j k and a o; from u, c, g, i, k, e and o, draw the ordinates, u 1, c 2, g 3, i 4, k 5, e 6 and o 7, at right angles to u o; make u 1 equal to t s, c 2 equal to r 2, g 3 equal to f 3, &c., and trace the curve, 1 7, through the points thus found; find the curve, c e, in the same manner, by transferring the distances between the line, t a, and the arc, r d; join 1 and c, also e and 7; then, 1 c e 7 will be the face-mould required for that part of the rail which is denoted by the letters, $s r d^2 b^3$, on the plan at Fig. 274.

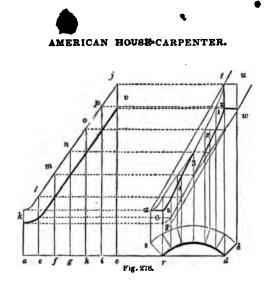
To ascertain the mould for the next quarter, make a c j e, (Fig.



277,) equal to $a^2 c^2 j e^2$ at Fig. 274; at any convenient height on the line, d i, in that figure, draw $q i^2$, parallel to e d; through cand j, (Fig. 277,) draw b d; through a, and from j, draw b k and j o, at right angles to b d; make b k and j o equal to $i^2 k$ and qi, respectively, in Fig. 274; from k, through o, draw k f; and proceed as in the last figure to obtain the face-mould, A.

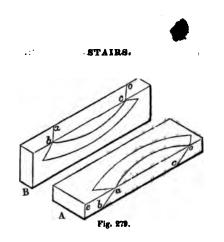
381.—To ascertain the requisite thickness of stuff. CASE 1.—When the falling-mould is straight. Make o h and k m, (Fig. 277,) equal to i y at Fig. 274; draw h i and m n, parallel to b d; through the corner farthest from k f, as n or i, draw n i, parallel to k f; then the distance between k f and n i will give the thickness required.

382.—CASE 2.— When the falling-mould is curved. In Fig. 278, s r d b is equal to $s r d^2 b^2$ in Fig. 274. Make a c equal to the stretch-out of the arc, s b, according to Art. 92, and divide a c and s b, each into a like number of equal parts; from a and c, and from each point of division in the line, a c, draw a k, e l, &c., at right angles to a c; make a k equal to t u in Fig. 274, and c j equal to $b^2 m$



in that figure, and complete the talling-mould, k j, every way equal to u m in Fig. 274; from the points of division in the arc, sb, draw lines radiating towards the centre of the circle, dividing the arc, r d, in the same proportion as s b is divided; from d and b, draw d t and b u, at right angles to a d, and from j and v, draw j u and v w, at right angles to j c; then x t u w will be a vertical projection of the joint, d b. Supposing every radiating line across s r d b corresponding to the vertical lines across k j-to represent a joint, find their vertical projection, as at 1, 2, 3, 4, 5 and 6; through the corners of those parallelograms, trace the curve lines shown in the figure ; then 6 u will be a *helinet*, or vertical projection, of s r d b. To find the thickness of plank necessary to get out this part of the rail, draw the line, z t, touching the upper side of the helinet in two places: through the corner farthest projecting from that line, as w, draw y w, parallel to z t; then the distance between those lines will be the proper thickness of stuff for this part of the The same process is necessary to find the thickness of rail. stuff in all cases in which the falling-mould is in any way curved.

383.—To apply the face-mould to the plank. In Fig. 279, A represents the plank with its best side and edge in view, and B the same plank turned up so as to bring in view the other side

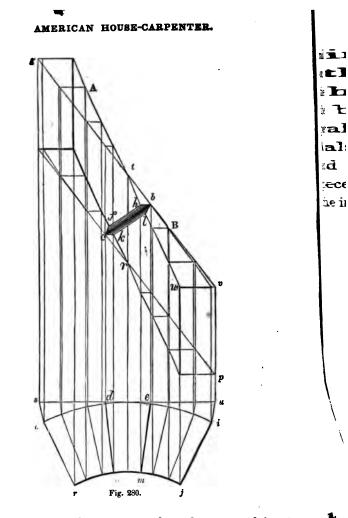


and the same edge, this being square from the face. Apply the tips of the mould at the edge of the plank, as at a and o, (A_i) and mark out the shape of the twist; from a and o, draw the lines, a b and o c, across the edge of the plank, the angles, e a b and e o c, corresponding with k f d at Fig. 277; turning the plank up as at B, apply the tips of the mould at b and c, and mark it out as shown in the figure. In sawing out the twist, the saw must be be moved in the direction, a b; which direction will be perpendicular when the twist is held up in its proper position.

In sawing by the face-mould, the *sides* of the rail are obtained; the top and bottom, or the upper and the lower surfaces, are obtained by squaring from the sides, after having bent the fallingmould around the outer, or convex side, and marked by its edges. Marking across by the ends of the falling-mould will give the position of the butt-joint.

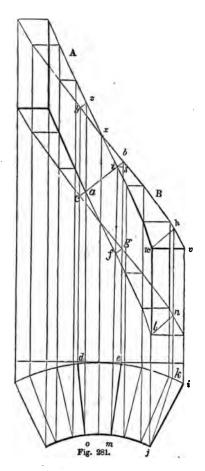
384.—Elucidation of the process by which the direction of the butt-joint is obtained in Art. 380. Mr. Nicholson, in his *Carpenter's Guide*, has given the joint a different direction to that here shown; he radiates it towards the centre of the cylinder. This is erroneous—as can be shown by the following operation:

In Fig. 280, a r j i is the plan of a part of the rail about the joint, s u is the stretch-out of a i, and g p is the helinet, or vertical projection of the plan, a r j i, obtained according to Art.

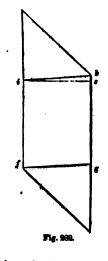


382. Bisect r t, part of an ordinate from the centre of the plan and through the middle, draw c b, at right angles to g v; from b and c, draw c d and b e, at right angles to s u; from d and e, draw lines radiating towards the centre of the plan: then d oand e m will be the direction of the joint on the plan, according to Nicholson, and c b its direction on the falling-mould. It will be admitted that all the lines on the upper or the lower side of the rail which radiate towards the centre of the cylinder, as d o, e m or i, j, are level; for instance, the level line, w v, on the top of the

n the helinet, is a true representation of the radiating line, j i, ne plan. The line, b h, therefore, on the top of the rail in elinet, is a true representation of e m on the plan, and k c on obtain of the rail truly represents d o. From k, draw k l, lel to c b, and from h, draw hf, parallel to b c; join l and so c and f; then c k l b will be a true representation of the of the lower piece, B, and c f h b of the end of the upper A; and f k or h l will show how much the joint is open on uner, or concave side of the rail.



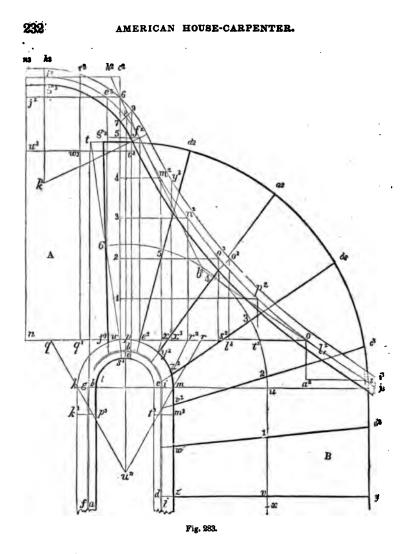
To show that the process followed in Art. 380 is correct, let do and em, (Fig. 281,) be the direction of the butt-joint found as at Fig. 275. Now, to project, on the top of the rail in the helinet, a line that does not radiate towards the centre of the cylinder, as j k, draw vertical lines from j and k to w and h, and join w and h; then it will be evident that wh is a true representation in the helinet of j k on the plan, it being in the same plane as j k, and also in the same winding surface as w v. The line, l n, also, is a true representation on the bottom of the helinet of the line, j k, in the plan. The line of the joint, e m, therefore, is projected in the same way and truly by i b on the top of the helinet; and the line, d o, by c a on the bottom. Join a and i, and then it will be seen that the lines, c a, a i and i b, exactly coincide with c b, the line of the joint on the convex side of the rail; thus proving the lower end of the upper piece, A, and the upper end of the lower piece, B, to be in one and the same plane, and that the direction of the joint on the plan is the true one. By reference to Fig. 275, it will be seen that the line, l i, corresponds to x i in Fig. 281; and that e k in that figure is a representation of f b, and i k of d b.



In getting out the twists, the joints, before the falling-mould is

applied, are cut perpendicularly, the face-mould being long enough to include the overplus necessary for a butt-joint. The face-mould for A, therefore, would have to extend to the line, $i \ b$; and that for B, to the line, yz. Being sawed vertically at first, a section of the joint at the end of the face-mould for A, would be represented in the helinet by $b \ i f g$. To obtain the position of the line, $b \ i$, on the end of the twist, draw $i \ s$, (Fig. 282,) at right angles to $i \ f$, and make $i \ s$ equal to $m \ e \ at Fig. 281$; through s, draw $s \ g$, parallel to $i \ f$, and make $s \ b$ equal to $s \ b \ at Fig. 281$; join $b \ and \ i \ j$ make $i \ f$ equal to $i \ f \ at Fig. 281$, and from f, draw $f \ g$, parallel to $i \ b \ f \ m$ will be a perpendicular section of the rail over the line, $e \ m$, on the plan at Fig. 281, corresponding to $i \ b \ f \ f$ in the helinet at that figure ; and when the rail is squared, the top, or back, must be trimmed off to the line, $i \ b$, and the bottom to the line, $f \ g$.

385.—To grade the front string of a stairs, having winders in a quarter-circle at the top of the flight connected with flyers at the bottom. In Fig. 283, a b represents the line of the facia along the floor of the upper story, $b \ e \ c$ the face of the cylinder, and c d the face of the front string. Make g b equal to $\frac{1}{2}$ of the diameter of the baluster, and draw the centre-line of the rail, fg, g h i and i j, parallel to a b, b e c and c d; make g k and g leach equal to half the width of the rail, and through k and l, draw lines for the convex and the concave sides of the rail, parallel to the centre-line; tangical to the convex side of the rail, and parallel to k m, draw n o; obtain the stretch-out, q r, of the semi-circle, kp m, according to Art. 92; extend a b to t, and k m to s; make c s equal to the length of the steps, and i u equal to 18 inches, and describe the arcs, s t and u 6, parallel to m p; from t, draw t w, tending to the centre of the cylinder; from 6, and on the line, 6 ux, run off the regular tread, as at 5, 4, 3, 2, 1 and v; make u x equal to half the arc, u 6, and make the point of division nearest to x, as v, the limit of the parallel steps, or flyers; make r o equal to m z; from o, draw $o a^2$, at right angles to n o, and equal to one rise;



from a^s , draw $a^2 s$, parallel to n o, and equal to one tread; from s, through o, draw $s b^2$.

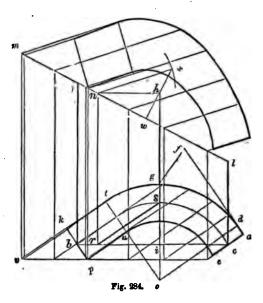
Then from w, draw $w c^{2}$, at right angles to n o, and set up, on the line, $w c^{2}$, the same number of risers that the floor, A, is above the first winder, B, as at 1, 2, 3, 4, 5 and 6; through 5, (on the arc, 6 u,) draw $d^{2} e^{2}$, tending to the centre of the cylinder; from e^{2} , draw $e^{2} f^{2}$, at right angles to n o, and through 5, (on the line,

 $w c^2$,) draw $g^2 f^2$, parallel to n o; through 6, (on the line, $w c^2$,) and f^2 , draw the line, $h^2 b^2$; make 6 c^2 equal to half a rise, and from c^2 and 6, draw $c^4 i^2$ and 6 j^3 , parallel to $n \circ j$ make $h^2 i^4$ equal to $h^{2} f^{2}$; from i^{2} , draw $i^{2} k^{2}$, at right angles to $i^{2} h^{2}$, and from f^{2} , draw $f^2 k^2$, at right angles to $f^2 h^2$; upon k^2 , with $k^2 f^2$ for radius, describe the arc, $f^2 i^2$; make $b^2 l^2$ equal to $b^3 f^2$, and ease off the angle at b^2 by the curve, $f^2 l^2$. In the figure, the curve is described from a centre, but in a full-size plan, this would be impracticable; the best way to ease the angle, therefore, would be with a tanged curve, according to Art. 89. Then from 1, 2, 3 and 4, (on the line, $w c^2$,) draw lines parallel to n o, meeting the curve in m^2 , n^2 , o^2 and p^2 ; from these points, draw lines at right angles to *n* o, and meeting it in x^2 , r^2 , s^2 and t^2 ; from x^2 and r^2 , draw lines tending to u^2 , and meeting the convex side of the rail in y^2 and z^2 ; make $m v^2$ equal to $r s^2$, and $m w^2$ equal to $r t^2$; from y^2 , z^2 , v^2 , and w^2 , through 4, 3, 2 and 1, draw lines meeting the line of the wall-string in a^3 , b^3 , c^3 and d^3 ; from e^3 , where the centre-line of the rail crosses the line of the floor, draw $e^{s} f^{3}$, at right angles to n o, and from f^3 , through 6, draw $f^3 g^2$; then the heavy lines, $f^3 g^2$, $e^{i} d^{3}$, $y^{2} a^{3}$, $z^{2} b^{3}$, $v^{2} c^{3}$, $w^{4} d^{3}$, and z y, will be the lines for the risers, which, being extended to the line of the front string, $b \ e \ c \ d$, will give the dimensions of the winders, and the grading of the front string, as was required.

386.— To obtain the falling-mould for the twists of the lastmentioned stairs. Make $i^2 g^3$ and $i^2 h^3$, (Fig. 283,) each equal to half the thickness of the rail; through h^3 and g^3 , draw $h^3 i^3$ and $g^3 j^3$, parallel to $i^2 s$; assuming $k k^3$ and $m m^3$ on the plan as the amount of straight to be got out with the twists, make n qequal to $k k^3$, and $r l^3$ equal to $m m^3$; from n and l^3 , draw lines at right angles to n o, meeting the top of the falling-mould in n^3 and o^3 ; from o^3 , draw a line crossing the falling-mould at right angles to a chord of the curve, $f^2 l^3$; through the centre of the cylinder, draw u^3 8, at right angles to n o; through 8, draw 7 9, tending to k^3 ; then n^3 7 will be the falling-mould for the upper twist, and 7 o^3 the falling-mould for the lower twist.

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387.— To obtain the face-moulds. The moulds for the twists of this stairs may be obtained as at Art. 380; but, as the fallingmould in its course departs considerably from a straight line, it would, according to that method, require a very thick plank for the rail, and consequently cause a great waste of stuff. In order, therefore, to economize the material, the following method is to be preferred—in which it will be seen that the heights are taken in three places instead of two only, as is done in the previous method.

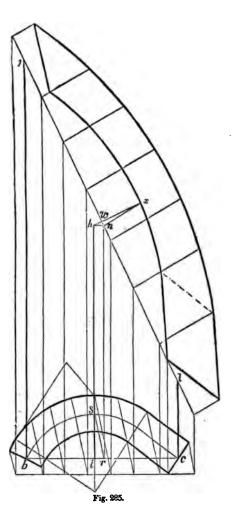


CASE 1.— When the middle height is above a line joining the other two. Having found at Fig. 283 the direction of the joint, $w s^3$ and $p \ e$, according to Art. 380, make $k \ p \ e \ a$, (Fig. 284,) equal to $k^3 \ p^3 \ e \ p$ in Fig. 283; join b and c, and from o, draw $o \ h_i$ at right angles to $b \ c$; obtain the stretch-out of $d \ g$, as $d \ f$, and at Fig. 283, place it from the axis of the cylinder, p, to q^3 ; from q^3 in that figure, draw $q^3 \ r^3$, at right angles to $n \ o$; also, at a convenient height on the line, $n \ n^3$, in that figure, and at right angles to that line, draw $u^3 \ v^3$; from b and c, in Fig. 284,

draw b j and c l, at right angles to b c; make b j equal to $u^s n^s$ in Fig. 283, i h equal to $w^s r^s$ in that figure, and c l equal to $v^s 9$; from l, through j, draw lm; from h, draw hn, parallel to cb; from n, draw n r, at right angles to b c, and join r and s; through he lowest corner of the plan, as p, draw v e, parallel to b c; from $\boldsymbol{a}, \boldsymbol{e}, \boldsymbol{u}, \boldsymbol{p}, \boldsymbol{k}, \boldsymbol{t}, \text{ and from as many other points as is thought ne$ cessary, draw ordinates to the base-line, v e, parallel to r s; through h, draw w x, at right angles to m l; upon n, with r s for radius, describe an intersecting arc at x, and join n and x; from the points at which the ordinates from the plan meet the baseline, v e, draw ordinates to meet the line, m l, at right angles to ve; and from the points of intersection on m l, draw corresponding ordinates, parallel to n x; make the ordinates which are parallel to n x of a length corresponding to those which are parallel to r s, and through the points thus found, trace the face-mould as required.

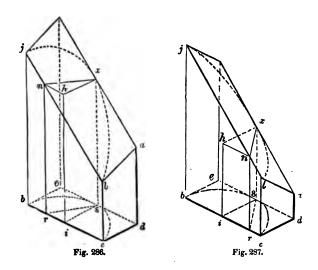
CASE 2.— When the middle height is below a line joining the other two. The lower twist in Fig. 283 is of this nature. The face-mould for this is found at Fig. 285 in a manner similar to that at Fig. 284. The heights are all taken from the top of the falling-mould at Fig. 283; b j being equal to w 6 in Fig. 283, i h equal to $x^3 y^3$ in that figure, and c l to $l^3 o^3$. Draw a line through j and l, and from h, draw h n, parallel to b c; from n, draw n r, at right angles to b c, and join r and s; then r s will be the bevil for the lower ordinates. From h, draw h x, at right angles to j l; upon n, with r s for radius, describe an intersecting arc at x, and join n and x; then n x will be the bevil for the upper ordinates, upon which the face-mould is found as in Case 1.

388.—Elucidation of the foregoing method.—This method of finding the face-moulds for the handrailing of winding stairs, being founded on principles which govern cylindric sections, may be illustrated by the following figures. Fig. 286 and 287 represent solid blocks, or prisms, standing upright on a level base, bd; the upper surface, ja forming oblique angles with the face, bl—



in Fig. 286 obtuse, and in Fig. 287 acute. Upon the base, describe the semi-circle, $b \ s \ c$; from the centre, *i*, draw *i s*, at right angles to $b \ c$; from *s*, draw $s \ x$, at right angles to $e \ d$, and from *i*, draw *i h*, at right angles to $b \ c$; make *i h* equal to $s \ x$, and join $h \ and \ x$; then, $h \ and \ x$ being of the same height, the line, $h \ x$, joining them, is a level line. From h, draw $h \ n$, parallel to $b \ c$; and from *n*, draw $n \ r$, at right angles to $b \ c$; join $r \ and \ s$, also $n \ r$.

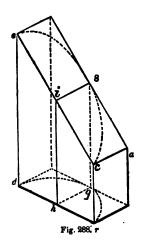




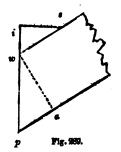
and x; then, n and x being of the same height, n x is a level line; and this line lying perpendicularly over r s, n x and r s must be of the same length. So, all lines on the top, drawn parallel to nx, and perpendicularly over corresponding lines drawn parallel to r s on the base, must be equal to those lines on the base; and by drawing a number of these on the semi-circle at the base and others of the same length at the top, it is evident that a curve, jx l, may be traced through the ends of those on the top, which shall lie perpendicularly over the semi-circle at the base.

It is upon this principle that the process at Fig. 284 and 285 is founded. The plan of the rail at the bottom of those figures is supposed to lie perpendicularly under the face-mould at the top; and each ordinate at the top over a corresponding one at the base. The ordinates, n x and r s, in those figures, correspond to n x and r s in Fig. 286 and 287.

In Fig. 288, the top, e a, forms a right angle with the face, d c; all that is necessary, therefore, in this figure, is to find a line corresponding to h x in the last two figures, and that will lie level and in the upper surface; so that all ordinates at right angles to d r on the base, will correspond to those that are at right angles

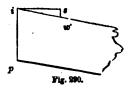


to e c on the top. This elucidates Fig. 276; at which the lines, h 9 and i 8, correspond to h 9 and i 8 in this figure.

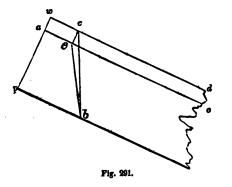


389.—To find the bevil for the edge of the plank. The plank, before the face-mould is applied, must be bevilled according to the angle which the top of the imaginary block, or prism, in the previous figures, makes with the face. This angle is determined in the following manner: draw wi, (Fig. 289,) at right angles to *is*, and equal to wh at Fig. 284; make *is* equal to *is* in that figure, and join w and s; then sw p will be the bevil required in order to apply the face-mould at Fig. 284. In Fig. 285, the middle height being below the line joining the other two, the bevil is therefore acute. To determine this, draw *is*, (Fig. 290,) at





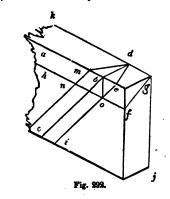
right angles to ip, and equal to is in Fig. 285; make sw equal to hw in Fig. 285, and join w and i; then wip will be the bevil required in order to apply the face-mould at Fig. 285. Although the falling-mould in these cases is curved, yet, as the plank is *sprung*, or bevilled on its edge, the thickness necessary to get out the twist may be ascertained according to Art. 381 taking the vertical distance across the falling-mould at the joints, and placing it down from the two outside heights in Fig. 284 or 285. After bevilling the plank, the moulds are applied as at Art. 383—applying the pitch-board on the bevilled instead of a square edge, and placing the tips of the mould so that they will bear the same relation to the edge of the plank, as they do to the line, jl, in Fig. 284 or 285.



390.—To apply the moulds without bevilling the plank. Make w p, (Fig. 291,) equal to w p at Fig. 289, and the angle, b c d, equal to b j l in Fig. 284; make p a equal to the thickness of the plank, as w a in Fig. 289, and from a draw a o, parallel to w d; from c, draw c e, at right angles to w d, and join e

and b; then the angle, b e o, on a square edge of the plank, having a line on the upper face at the distance, p a, in Fig. 289, at which to apply the tips of the mould—will answer the same purpose as bevilling the edge.

If the bevilled edge of the plank, which reaches from p to w, is supposed to be in the plane of the paper, and the point, a, to be above the plane of the paper as much as a, in Fig. 289, is distant from the line, w p; and the plank to be revolved on p b as an axis until the line, p w, falls below the plane of the paper, and the line, p a, arrives in it; then, it is evident that the point, c, will fall, in the line, c e, until it lies directly behind the point, e, and the line, b c, will lie directly behind b e.



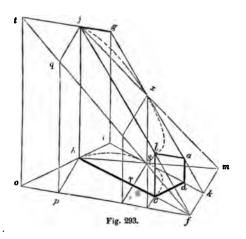
391.—To find the bevils for splayed work. The principle employed in the last figure is one that will serve to find the bevils for splayed work—such as hoppers, bread-trays, &c.—and a way of applying it to that purpose had better, perhaps, be introduced in this connection. In Fig. 292, $a \ b \ c$ is the angle at which the work is splayed, and $b \ d$, on the upper edge of the board, is at right angles to $a \ b$; make the angle, $f \ g \ j$, equal to $a \ b \ c$, and from f, draw $f \ h$, parallel to $e \ a$; from b, draw $b \ o$, at right angles to $a \ b$; through o, draw $i \ e$, parallel to $c \ b$, and join $e \ and$ d; then the angle, $a \ e \ d$, will be the proper bevil for the ends from the inside, or $k \ d \ e$ from the outside. If a mitre-joint is re-

quired, set f g, the thickness of the stuff on the level, from e to m, and join m and d; then k d m will be the proper bevil for a mitre-joint.

If the upper edges of the splayed work is to be bevilled, so as to be horizontal when the work is placed in its proper position, f g j, being the same as a b c, will be the proper bevil for that purpose. Suppose, therefore, that a piece indicated by the lines, k g, g f and f h, were taken off; then a line drawn upon the bevilled surface from d, at right angles to k d, would show the true position of the joint, because it would be in the direction of the board for the other side; but a line so drawn would pass through the point, o,—thus proving the principle correct. So, if a line were drawn upon the bevilled surface from d, at an angle of 45 degrees to k d, it would pass through the point, n.

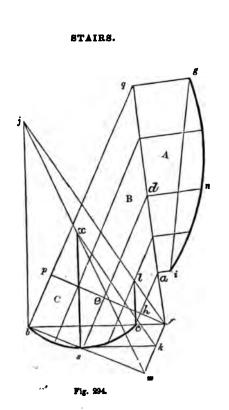
392.—Another method for face-moulds. It will be seen by reference to Art. 388, that the principal object had in view in the preparatory process of finding a face-mould, is to ascertain upon it the direction of a horizontal line. This can be found by a method different from any previously proposed; and as it requires fewer lines, and admits of less complication, it is probably to be preferred. It can be best introduced, perhaps, by the following explanation:

In Fig. 293, j d represents a prism standing upon a level base, b d, its upper surface forming an acute angle with the face, b l, as at Fig. 287. Extend the base line, b c, and the raking line, j l, to meet at f; also, extend e d and g a, to meet at k; from f, through k, draw f m. If we suppose the prism to stand upon a level floor, o f m, and the plane, j g a l, to be extended to meet that floor, then it will be obvious that the intersection between that plane and the plane of the floor would be in the line, f k; and the line, f k, being in the plane of the floor, and also in the inclined plane, j g k f, any line made in the plane, j g k f, parallel to f k, must be a level line. By finding the position of a perpendicular plane, at right angles to the raking plane, j f k g, we shall greatly shorten the process for obtaining ordinates.



This may be done thus: from f, draw f o, at right angles to fm; extend e b to o, and g j, to t; from o, draw o t, at right angles to o f, and join t and f; then t o f will be a perpendicular plane, at right angles to the inclined plane, t g k f; because the base of the former, o f, is at right angles to the base of the latter, f k, both these lines being in the same plane. From b, draw b p, at right angles to o f, or parallel to fm; from p, draw p q, at right angles to o f, and from q, draw a line on the upper plane, parallel to fm, or at right angles to t f; then this line will obviously be drawn to the point, j, and the line, q j, be equal to p b. Proceed, in the same way, from the points, s and c, to find x and l.

Now, to apply the principle here explained, let the curve, $b \ s \ c_i$ (Fig. 294,) be the base of a cylindric segment, and let it be required to find the shape of a section of this segment, cut by a plane passing through three given points in its curved surface: one perpendicularly over b, at the height, $b \ j$; one perpendicularly over b, at the height, $b \ j$; one perpendicularly over s, at the height, $s \ x$; and the other over c, at the height, $c \ l$ —these lines being drawn at right angles to the chord of the base, $b \ c$. From j, through l, draw a line to meet the chord line extended to f; from s, draw $s \ k$, parallel to $b \ f$, and from x, draw $x \ k$, parallel to jf; from f, through k, draw $f \ m$; then $f \ m$ will be the intersecting line of the plane of the section with the



s of the base. This line can be proved to be the intersection less planes in another way; from b, through s, and from j, ligh x, draw lines meeting at m; then the point, m, will be e intersecting line, as is shown in the figure, and also at 293.

com f, draw f p, at right angles to f m; from b and c, and as many other points as is thought necessary, draw ordinates, llel to f m; make p q equal to b j, and join q and f; from points at which the ordinates meet the line, q f, draw others sht angles to q f; make each ordinate at A equal to its coronding ordinate at C, and trace the curve, g n i, through the ts thus found.

ow it may be observed that A is the plane of the section, B plane of the segment, corresponding to the plane, q p f, of . 293, and C is the plane of the base. To give these planes : proper position, let A be turned on q f as an axis until it

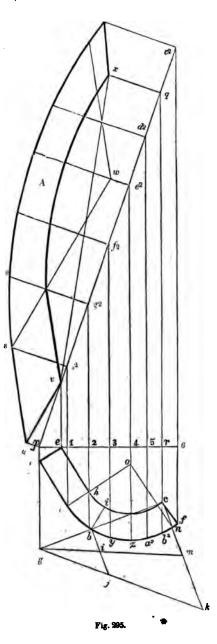
stands perpendicularly over the line, q f, and at right angles to the plane, B; then, while A and B are fixed at right angles, let B be turned on the line, p f, as an axis until it stands perpendicularly over p f, and at right angles to the plane, C; then the plane, A, will lie over the plane, C, with the several lines on one corresponding to those on the other; the point, i, resting at l, the point, n, at x, and g at j; and the curve, g n i, lying perpendicularly over $b \ s \ c$ —as was required. If we suppose the cylinder to be cut by a level plane passing through the point, l, (as is done in finding a face-mould,) it will be obvious that lines corresponding to q f and p f would meet in l; and the plane of the section, A, the plane of the segment, B, and the plane of the base, C, would all meet in that point.

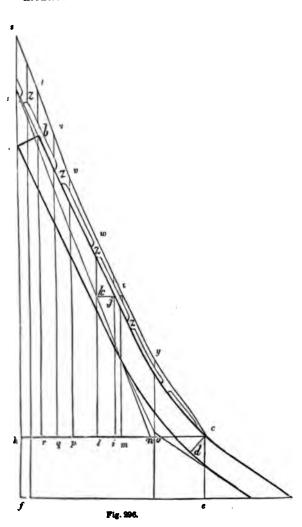
393.—To find the face-mould for a hand-rail according to the principles explained in the previous article. In Fig. 295, a e c f is the plan of a hand-rail over a quarter of a cylinder; and in Fig. 296, a b c d is the falling-mould; f e being equal to the stretch-out of a df in Fig. 295. From c, draw c h, parallel $t \mathcal{O}$ ef; bisect h c in i, and find a point, as b, in the arc, d f, (Fig -295,) corresponding to i in the line, h c; from i, (Fig. 296,) t the top of the falling-mould, draw i j, at right angles to hc; at Fig-295, from c, through b, draw c g, and from b and c, draw b j an \mathbb{Z} c k, at right angles to g c; make c k equal to h g at Fig. 296and b j equal to i j at that figure; from k, through j, draw kg_{π} and from g, through a, draw g p; then g p will be the intersecting line, corresponding to fm in Fig. 293 and 294; through e, draw p 6, at right angles to g p, and from c, draw c q, parallel to g p; make r q equal to h g at Fig. 296; join p and q, and proceed as in the previous examples to find the face-mould, A. The joint of the face-mould, u v, will be more accurately determined by finding the projection of the centre of the plan, o, as at w; joining s and w, and drawing u v, parallel to s w.

It may be noticed that c k and b j are not of a length corresponding to the above directions: they are but $\frac{1}{2}$ the length given.

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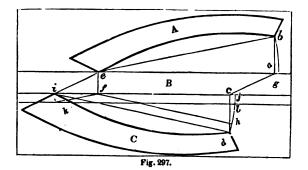
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The object of drawing these lines is to find the point, g, and that can be done by taking any proportional parts of the lines given, as well as by taking the whole lines. For instance, supposing ck and b j to be the full length of the given lines, bisect one in iand the other in m; then a line drawn from m, through i, will give the point, g, as was required. The point, g, may also be

ained thus: at Fig. 296, make h l equal to c b in Fig. 295; m l, draw l k, at right angles to h c; from j, draw j k, parallel h c; from g, through k, draw g n; at Fig. 295, make b gal to ln in Fig. 296; then g will be the point required. The reason why the points, a, b and c, in the plan of the rail at g. 295, are taken for resting points instead of e, i and f, is this : top of the rail being level, it is evident that the points, a and e, he section a e, are of the same height; also that the point, i, is of same height as b, and c as f. Now, if a is taken for a point the inclined plane rising from the line g p, e must be below t plane; if b is taken for a point in that plane, i must be below and if c is in the plane, f must be below it. The rule, then, taking these points, is to take in each section the one that is rest to the line, g p. Sometimes the line of intersection, g p, opens to come almost in the direction of the line, er: in such e, after finding the line, see if the points from which the ghts were taken agree with the above rule; if the heights re taken at the wrong points, take them according to the rule we, and then find the true line of intersection, which will not y much from the one already found.



394.—To apply the face-mould thus found to the plank. he face-mould, when obtained by this method, is to be applied a square-edged plank, as directed at Art. 383, with this differce: instead of applying both tips of the mould to the edge of

the plank, one of them is to be set as far from the edge of the plank, as x, in Fig. 295, is from the chord of the section p q—as is shown at Fig. 297. A, in this figure, is the mould applied on the upper side of the plank, B, the edge of the plank, and C, the mould applied on the under side; a b and c d being made equal to q x in Fig. 295, and the angle, e a c, on the edge, equal to the angle, p q r, at Fig. 295. In order to avoid a waste of stuff, it would be advisable to apply the tips of the mould, e and b, immediately at the edge of the plank. To do this, suppose the moulds to be applied as shown in the figure; then let A be revolved upon e until the point, b, arrives at g, causing the line, e b, to coincide with e g: the mould upon the under side of the plank must now be revolved upon a point that is perpendicularly beneath e_i as f_i ; from f_i draw f_i , parallel to $i d_i$ and from d_i draw dh, at right angles to id; then revolve the mould, C, upon f, until the point, h, arrives at j, causing the line, f h, to coincide with f j, and the line, i d, to coincide with k l; then the tips of the mould will be at k and l.

The rule for doing this, then, will be as follows: make the angle, i f k, equal to the angle q v x, at Fig. 295; make f k equal to f i, and through k, draw k l, parallel to i j; then apply the corner of the mould, i, at k, and the other corner d, at the line, k l.

The thickness of stuff is found as at Art. 381.

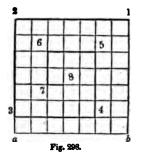
395.—To regulate the application of the falling-mould. Obtain, on the line, h c, (Fig. 296,) the several points, r, q, p, land m, corresponding to the points, b^2 , a^2 , z, y, &c., at Fig. 295; from r q p, &c., draw the lines, r t, q u, p v, &c., at right angles to h c; make h s, r t, q u, &c., respectively equal to $6 c^2$, r q, $5 d^2$, &c., at Fig. 295; through the points thus found, trace the curve, s w c. Then get out the piece, g s c, attached to the falling-mould at several places along its length, as at z, z, &c. In applying the falling-mould with this strip thus attached, the edge, s w c, will coincide with the upper surface of the rail piece

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before it is squared; and thus show the proper position of the falling-mould along its whole length. (See Art. 403.)

SCROLLS FOR HAND-RAILS.

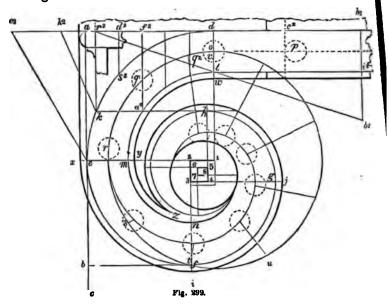
396.—General rule for finding the size and position of the regulating square. The breadth which the scroll is to occupy, the number of its revolutions, and the relative size of the regulating square to the eye of the scroll, being given, multiply the number of revolutions by 4, and to the product add the number of times a side of the square is contained in the diameter of the eye, and the sum will be the number of equal parts into which the breadth is to be divided. Make a side of the regulating square equal to one of these parts. To the breadth of the scroll add one of the parts thus found, and half the sum will be the length of the longest ordinate.



397.—To find the proper centres in the regulating square. Let $a \ 2 \ 1 \ b$, (Fig. 298,) be the size of a regulating square, found according to the previous rule, the required number of revolutions being 1³/₄. Divide two adjacent sides, as $a \ 2$ and $2 \ 1$, into as many equal parts as there are quarters in the number of revolutions, as seven; from those points of division, draw lines across the square, at right angles to the lines divided; then, 1 being the first centre, 2, 3, 4, 5, 6 and 7, are the centres for the other quarters, and 8 is the centre for the eye; the heavy lines that deter-

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mine these centres being each one part less in length than its preceding line.

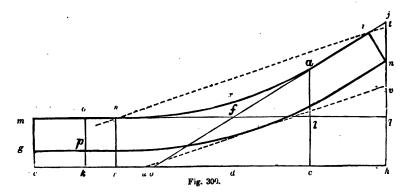


398.—To describe the scroll for a hand-rail over a curtail step. Let a b, (Fig. 299,) be the given breadth, $1\frac{3}{4}$ the given number of revolutions, and let the relative size of the regulating square to the eye be $\frac{1}{3}$ of the diameter of the eye. Then, by the rule, $1\frac{3}{4}$ multiplied by 4 gives 7, and 3, the number of times a side of the square is contained in the eye, being added, the sum is 10. Divide a b, therefore, into 10 equal parts, and set one from b to c; bisect a c in e; then a e will be the length of the longest ordinate, (1 d or 1 e.) From a, draw a d, from e, draw e 1, and from b, draw b f, all at right angles to a b; make e 1 equal to ea, and through 1, draw 1 d, parallel to a b; set b c from 1 to 2, and upon 1 2, complete the regulating square; divide this square as at Fig. 298; then describe the arcs that compose the scroll, as follows: upon 1, describe d e; upon 2, describe e f; upon 3, describe f g; upon 4, describe g h, &c.; make d l equal to the

width of the rail, and upon 1, describe lm; upon 2, cescribe m, &c.; describe the eye upon 8, and the scroll is completed.

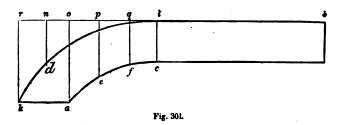
399.—To describe the scroll for a curtail step. Bisect dl, (Fig. 299,) in o, and make o v equal to $\frac{1}{2}$ of the diameter of a baluster; make v w equal to the projection of the nosing, and e x equal to w l; upon 1, describe w y, and upon 2, describe y z; also upon 2, describe x i; upon 3, describe ij, and so around to z; and the scroll for the step will be completed.

400.— To determine the position of the balusters under the scroll. Bisect dl, (Fig. 299,) in o, and upon 1, with 1 o for radius, describe the circle, oru; set the baluster at p fair with the face of the second riser, c^{3} , and from p, with half the tread in the dividers, space off as at o, q, r, s, t, u, &c., as far as q^{3} ; upon 2, 3, 4 and 5, describe the centre-line of the rail around to the eye of the scroll; from the points of division in the circle, oru, draw lines to the centre-line of the rail, tending to the centre of the eye, 8; then, the intersection of these radiating lines with the centre-line of the rail, will determine the position of the balusters, as shown in the figure.



401.—To obtain the falling-mould for the raking part of the scroll. Tangical to the rail at h, (Fig. 299,) draw h k, parallel to d a; then $k a^2$ will be the joint between the twist and the other part of the scroll. Make $d e^2$ equal to the stretch-out of d e, and upon d

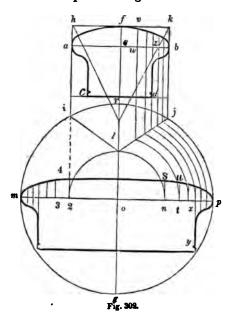
 e^* , find the position of the point, k, as at k^* ; at Fig. 300, make edequal to $e^2 d$ in Fig. 299, and d c equal to $d c^2$ in that figure; from c, draw c a, at right angles to e c, and equal to one rise; make c b equal to one tread, and from b, through a, draw b j; bisect a c in l, and through l, draw m q, parallel to e h; m q is the height of the level part of a scroll, which should always be about $3\frac{1}{2}$ feet from the floor; ease off the angle, m f j, according to Art. 89, and draw g w n, parallel to m x j, and at a distance equal to the thickness of the rail; at a convenient place for the joint, as i, draw in, at right angles to b j; through n, draw j h, at right angles to eh; make dk equal to dk^{*} in Fig. 299, and from k, draw k o, at right angles to e h; at Fig. 299, make d h^2 equal to d h in Fig. 300, and draw h^2 b^2 , at right angles to d h^{2} ; then k a^{2} and h^{2} i^{2} will be the position of the joints on the plan, and at Fig. 300, o p and i n, their position on the fallingmould; and p o in, (Fig. 300,) will be the falling-mould required.



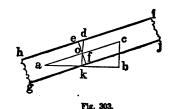
402.—To describe the face-mould. At Fig. 299, from k, draw $k r^3$, at right angles to $r^2 d$; at Fig. 300, make h r equal to $k^2 r^2$ in Fig. 299, and from r, draw r s, at right angles to r h; from the intersection of r s with the level line, m q, through i, draw s t; at Fig. 299, make $h^2 b^2$ equal to q t in Fig. 300, and join b^2 and r^4 ; from a^3 , and from as many other points in the arcs, $a^2 l$ and k d, as is thought necessary, draw ordinates to $r^2 d$, at right angles to the latter; make r b, (Fig. 301,) equal in its length and in its divisions to the line, $r^2 b^3$, in Fig. 299; from r, n, o, p, q

and *l*, draw the lines, r k, n d, o a, p e, q f and *l* c, at right angles to r b, and equal to $r^2 k$, $d^2 s^2$, $f^2 a^2$, &c., in Fig. 299; through the points thus found, trace the curves, k l and a c, and complete the face-mould, as shown in the figure. This mould is to be applied to a square-edged plank, with the edge, l b, parallel to the edge of the plank. The rake lines upon the edge of the plank are to be made to correspond to the angle, s t h, in Fig. 300. The thickness of stuff required for this mould is shown at Fig. 300, between the lines s t and u v - u v being drawn parallel to s t.

403.—All the previous examples given for finding face-moulds over winders, are intended for *moulded* rails. For *round* rails, the same process is to be followed with this difference: instead of working from the sides of the rail, work from a centre-line. After finding the projection of that line upon the upper plane, describe circles upon it, as at *Fig.* 262, and trace the sides of the moulds by the points so found. The thickness of stuff for the twists of a round rail, is the same as for the straight; and the twists are to be sawed square through.



404.—To ascertain the form of the newel-cap from a section of the rail. Draw a b, (Fig. 302,) through the widest part of the given section, and parallel to c d; bisect a b in e, and through a, e and b, draw h i, f g, and k j, at right angles to a b; at a convenient place on the line, fg, as o, with a radius equal to half the width of the cap, describe the circle, i j g; make r l equal to e b or e a; join l and j, also l and i; from the curve, f b, to the line, l j, draw as many ordinates as is thought necessary, parallel to f g; from the points at which these ordinates meet the line, l j, and upon the centre, o, describe arcs in continuation to meet o p; from n, t, x, &c., draw n s, t u, &c., parallel to <math>f g; make n s, t u, &c., equal to e f, w v, &c.; make x y, &c., equalto z d, &c.; make o 2, o 3, &c., equal to o n, o t, &c.; make 24 equal to n s, and in this way find the length of the lines crossing om; through the points thus found, describe the section of the newel-cap, as shown in the figure.



405.—To find the true position of a butt joint for the twists of a moulded rail over platform stairs. Obtain the shape of the mould according to Art. 373, and make the line a b, Fig. 303, equal to a c, Fig. 269; from b, draw b c, at right angles to a b, and equal in length to n m, Fig. 269; join a and c, and bisect a c in o; through o draw e f, at right angles to a c, and d k, parallel to c b; make o d and o k each equal to half e h at Fig. 269; through e and f, draw h i and g j, parallel to a c. At Fig. 270, make n a equal to e d, Fig. 303, and through a, draw r p, at right angles to n c; then r p will be the true position on the face-mould for a butt joint, as was required. The sides must be sawn verti91

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cally as described at Art. 374, but the joint is to be sawn square through the plank. The moulds obtained for round rails, (Art. 371,) give the line for the joint, when applied to either side of the plank; but here, for moulded rails, the line for the joint can be obtained from only one side. When the rail is canted up, the joint is taken from the mould laid on the upper side of the lower twist, and on the under side of the upper twist; but when it is canted down, a course just the reverse of this is to be pursued. When the rail is not canted, either up or down, the vertical joint, obtained as at Art. 373, will be a butt joint, and therefore, in such a case, the process described in this article will be unnecessary.

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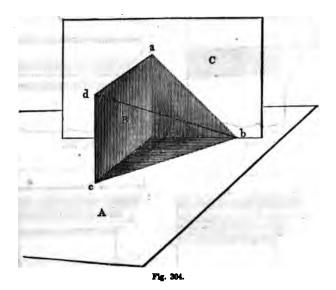
SECTION VII.—SHADOWS.

406.—The art of drawing consists in representing solids upon a plane surface: so that a curious and nice adjustment of lines is made to present the same appearance to the eye, as does the human figure, a tree, or a house. It is by the effects of light, in its reflection, shade, and shadow, that the presence of an object is made known to us; so, upon paper, it is necessary, in order that the delineation may appear real, to represent fully all the shades and shadows that would be seen upon the object itself. In this section I propose to illustrate, by a few plain examples, the simple elementary principles upon which shading, in architectural subjects, is based. The necessary knowledge of drawing, preliminary to this subject, is treated of in the Introduction, from Art. 1 to 14.

407.—The inclination of the line of shadow. This is always, in architectural drawing, 45 degrees, both on the elevation and the plan; and the sun is supposed to be behind the spectator, and over his left shoulder. This can be illustrated by reference to Fig. 304, in which A represents a horizontal plane, and B and C two vertical planes placed at right angles to each other. A represents the plan, C the elevation, and B a vertical projection from the elevation. In finding the shadow of the plane, B, the

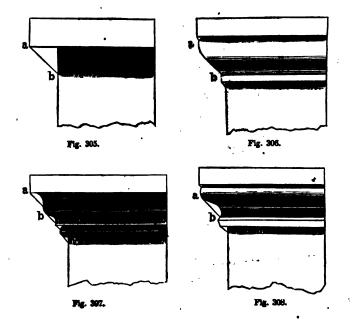


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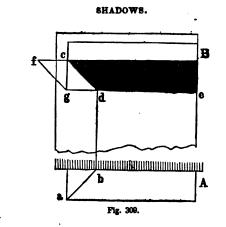
, a b, is drawn at an angle of 45 degrees with the horizon, and line, c'b, at the same angle with the vertical plane, B. The ie, B, being a rectangle, this makes the true direction of the 's rays to be in a course parallel to d b; which direction has 1 proved to be at an angle of 35 degrees and 16 minutes with horizon. It is convenient, in shading, to have a set-square 1 the two sides that contain the right angle of equal length; will make the two acute angles each 45 degrees; and will the requisite bevil when worked upon the edge of the Tare. One reason why this angle is chosen in preference to her, is, that when shadows are properly made upon the drawby it, the depth of every recess is more readily known, since breadth of shadow and the depth of the recess will be equal. 'o distinguish between the terms shade and shadow, it will be erstood that all such parts of a body as are not exposed to the et action of the sun's rays, are in shade; while those parts ch are deprived of light by the interposition of other bodies, in shadow.

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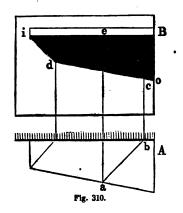


408.—To find the line of shadow on mouldings and other horizontally straight projections. Fig. 805, 306, 307 and 308, represent various mouldings in elevation, returned at the left, in the usual manner of mitreing around a projection. A mere inspection of the figures is sufficient to see how the line of shadow is obtained; bearing in mind that the ray, a b, is drawn from the projections at an angle of 45 degrees. Where there is no return at the end, it is necessary to draw a section, at any place in the length of the mouldings, and find the line of shadow from that.

409.—To find the line of shadow cast by a shelf. In Fig. 309, A is the plan, and B is the elevation of a shelf attached to a wall. From a and c, draw a b and c d, according to the angle previously directed; from b, erect a perpendicular intersecting c d at d; from d, draw d e, parallel to the shelf; then the lines, c d and d e, will define the shadow cast by the shelf. There is another method of finding the shadow, without the plan, A. Extend the lower line of the shelf to f, and make c f equal to the projection of the shelf

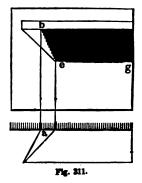


the wall; from f, draw f g, at the customary angle, and from op the vertical line, c g, intersecting f g at g; from g, draw parallel to the shelf, and from c, draw c d, at the usual angle; the lines, c d and d e, will determine the extent of the shadow fore.

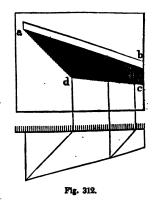


0.—To find the shadow cast by a shelf, which is wider at end than at the other. In Fig. 310, A is the plan, and B levation. Find the point, d, as in the previous example, and any other point in the front of the shelf, as a, erect the perpenar, a e; from a and e, draw a b and e c, at the proper angle, from b, erect the perpendicular, b c, intersecting e c in c;

from d, through c, draw $d \circ j$; then the lines, i d and $d \circ j$, will give the limit of the shadow cast by the shelf.

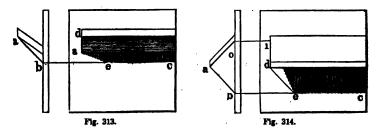


411.—To find the shadow of a shelf having one end acute or obtuse angled. Fig. 311 shows the plan and elevation of an acute-angled shelf. Find the line, eg, as before; from a, erec the perpendicular, ab; join b and e; then b e and eg will define the boundary of shadow.



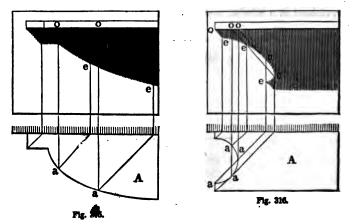
412.—To find the shadow cast by an inclined shelf. In Fig. 312, the plan and elevation of such a shelf is shown, having also one end wider than the other. Proceed as directed for finding the shadows of Fig. 310, and find the points, d and c; then a d and d c will be the shadow required. If the shelf had been

barallel in width on the plan, then the line, d c, would have been barallel with the shelf, a b.

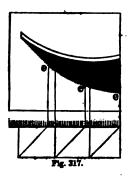


413.—To find the shadow cast by a shelf inclined in its vertical section either upward or downward. From a, (Fig. 313 and 314,) draw a b, at the usual angle, and from b, draw b c, parallel with the shelf; obtain the point, e, by drawing a line from d, at the usual angle. In Fig. 313, join e and i; then i e and e c will define the shadow. In Fig. 314, from o, draw o i, parallel with the shelf; join i and e; then i e and e c will be the shadow required.

The projections in these several examples are bounded by straight lines; but the shadows of curved lines may be found in the same manner, by projecting shadows from several points in the curved line, and tracing the curve of shadow through these points. Thus—

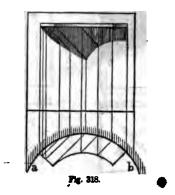


414.—To find the shadow of a shelf having its front edge, or end, curved on the plan. In Fig. 315 and 316, A and A show an example of each kind. From several points, as a, a, in the plan, and from the corresponding points, o, o, in the elevation, draw mays and perpendiculars intersecting at e, e, &cc.; through these points of intersection trace the curve, and it will define the shadow.



415.—To find the shadow of a shelf curved in the elevation. In Fig. 317, find the points of intersection, e, e and e, as in the last examples, and a curve traced through them will define the shadow.

The preceding examples show how to find shadows when cast upon a vertical plane; shadows thrown upon curved surfaces are ascertained in a similar manner. Thus—



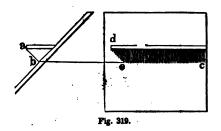
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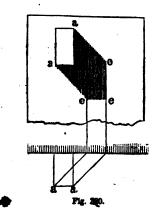
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416.—To find the shadow cast upon a cylindrical wall by a projection of any kind. By an inspection of Fig. 318, it will be seen that the only difference between this and the last examples, is, that the rays in the plan die against the circle, a b, instead of a straight line.



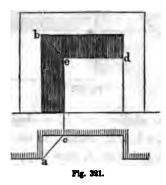
417.—To find the shadow cast by a shelf upon an inclined wall. Cast the ray, a b, (Fig. 319,) from the end of the shelf to the face of the wall, and from b, draw b c, parallel to the shelf; cast the ray, d e, from the end of the shelf; then the lines, d e and e c, will define the shadow.

. These examples might be multiplied, but enough has been given to illustrate the general principle, by which shadows in all instances are found. Let us attend now to the application of this principle to such familiar objects as are likely to occur in practice.

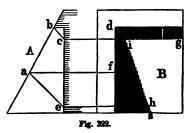


418.—To find the shadow of a projecting horizontal beam. From the points, a, a, &c., (Fig. 320,) cast rays upon the wall; the intersections, e, e, e, of those rays with the perpendiculars drawn from the plan, will define the shadow. If the beam be inclined, either on the plan or elevation, at any angle other than a sight angle, the difference in the manner of proceeding can be seen by reference to the preceding examples of inclined shelves, &c.

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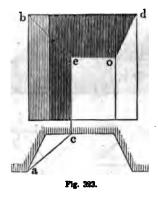
419.—To find the shadow in a recess. From the point, a, (Fig. 321,) in the plan, and b in the elevation, draw the rays, a c and b e; from c, erect the perpendicular, c e, and from e, draw the horizontal line, e d; then the lines, c e and e d, will show the extent of the shadow. This applies only where the back of the recess is parallel with the face of the wall.



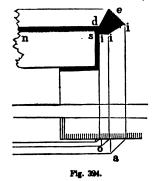
420.—To find the shadow in a recess, when the face of the wall is inclined, and the back of the recess is vertical. In Fig. 322, A shows the section and B the elevation \clubsuit a recess of this

SHADOWS.

kind. From b, and from any other point in the line, ba, as a, draw the rays, bc and ae; from c, a, and e, draw the horizontal lines, cg, af, and eh; from d and f, cast the rays, di and fh; from i, through h, draw is; then si and ig will define the shadow.

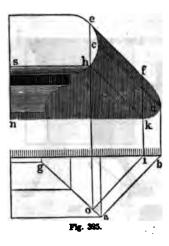


421.—To find the shadow in a fireplace. From a and b, (Fig. 323,) cast the rays, a c and b e, and from c, erect the perpendicular, c e; from e, draw the horizontal line, e o, and join o and d; then c e, e o, and o d, will give the extent of the shadow.



422.—To find the shadow of a moulded window-lintel. Cast rays from the projections, a, o, &c., in the plan, (Fig. 324,) and d, e, &c., in the elevation, and draw the usual perpendiculars intersecting the rays at i, i, and i; these intersections connected 34

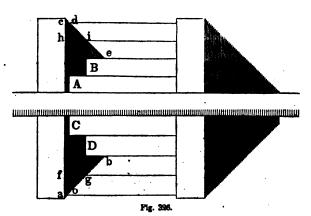
and horizontal lines drawn from them, will define the shadow. The shadow on the face of the lintel is found by casting a ray back from i to s, and drawing the horizontal line, s n.



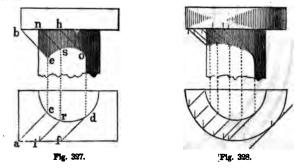
423.—To find the shadow cast by the nosing of a step. From a, (Fig. 325,) and its corresponding point, c, cast the rays, a b and c d, and from b, erect the perpendicular, b d; tangical to the curve at e, cast the ray, e f, and from e, drop the perpendicular, e o, meeting the mitre-line, a g, in o; cast a ray from o to i, and from i, erect the perpendicular, i f; from h, draw the ray, h k; from f to d and from d to k, trace the curve as shown in the figure; from k and h, draw the horizontal lines, k n and h s; then the limit of the shadow will be completed.

424.—To find the shadow thrown by a pedestal upon steps. From a, (Fig. 326,) in the plan, and from c in the elevation, draw the rays, $a \ b$ and $c \ e$; then $a \ o$ will show the extent of the shadow on the first riser, as at A; $f \ g$ will determine the shadow on the second riser, as at B; $c \ d$ gives the amount of shadow on the first tread, as at C, and $h \ i$ that on the second tread, as at D; which completes the shadow of the left-hand pedestal, both on the plan and elevation. A mere inspection of the figure will be suf-



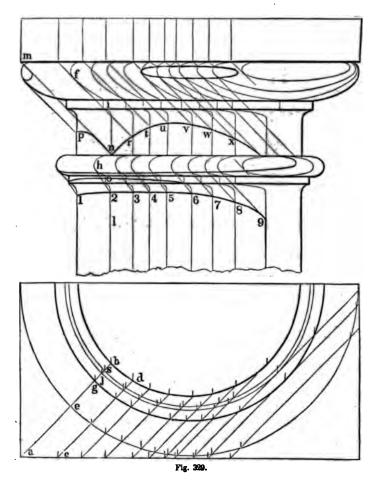


ficient to show how the shadow of the right-hand pedestal is obtained.



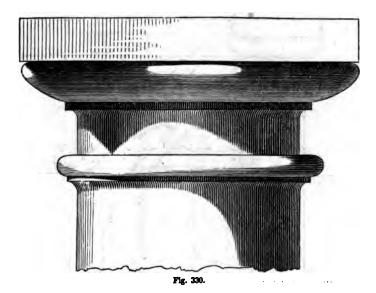
425.—To find the shadow thrown on a column by a square abacus. From a and b, (Fig. 327,) draw the rays, a c and b e, and from c, erect the perpendicular, c e; tangical to the curve at d, draw the ray, d f, and from h, corresponding to f in the plan, draw the ray, h o; take any point between a and f, as i, and from this, as also from a corresponding point, n, draw the rays, i r and n s; from r, and from d, erect the perpendiculars, r s and d o; through the points, e, s, and o, trace the curve as shown in the figure; then the extent of the shadow will be defined.

426.—To find the shadow thrown on a column by a circular abacus. This is so near like the last example, that no explanation will be necessary farther than a reference to the preceding article.



427.—To find the shadows on the capital of a column. This may be done according to the principles explained in the examples already given; a quicker way of doing it, however, is as follows. If we take into consideration one ray of light in connection with all those perpendicularly under and over it, it is evident that these several rays would form a vertical plane, standing at an angle of 45 degrees with the face of the elevation. Now, we may suppose the column to be *sliced*, so to speak, with planes of this

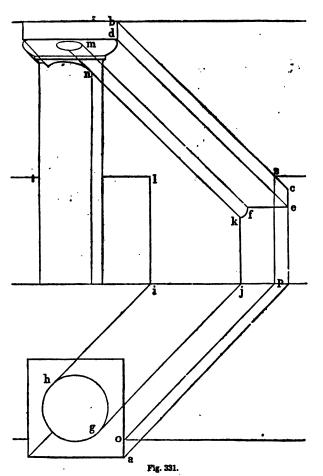
SHADOWS.



nature—cutting it in the lines, $a \ b, c \ d, \&c.$, (Fig. 329,) and, in the elevation, find, by squaring up from the plan, the lines of section which these planes would make thereupon. For instance: in finding upon the elevation the line of section, $a \ b$, the plane cuts the ovolo at e, and therefore f will be the corresponding point upon the elevation; h corresponds with g, i with j, o with s, and l with b. Now, to find the shadows upon this line of section, cast from m, the ray, $m \ n$, from h, the ray, $h \ o$, &c.; then that part of the section indicated by the letters, $m \ f \ i \ n$, and that part also between h and o, will be under shadow. By an inspection of the figure, it will be seen that the same process is applied to each line of section, and in that way the points, p, r, t, u, v, w, x, as also 1, 2, 3, &c., are successively found, and the lines of shadow traced through them.

Fig. 330 is an example of the same capital with all the shadows finished in accordance with the lines obtained on Fig. 329.

428.—To find the shadow thrown on a vertical wall by a column and entablature standing in advance of said wall. Cast



rays from a and b, (Fig. 331,) and find the point, c, as in the previous examples; from d, draw the ray, d e, and from e, the horizontal line, e f; tangical to the curve at g and h, draw the rays, g j and h i, and from i and j, erect the perpendiculars, i l and j k; from m and n, draw the rays, m f and n k, and trace the curve between k and f; cast a ray from o to p, a vertical line from p to s, and through s, draw the horizontal line, s t; the shadow as required will then be completed.

SHADOWS.

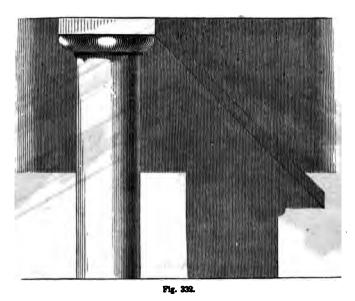
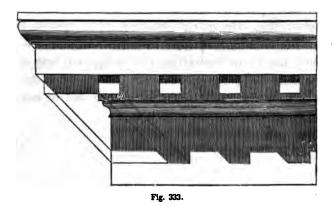


Fig. 332 is an example of the same kind as the last, with all the shadows filled in, according to the lines obtained in the preceding figure.



429.—Fig. 333 and 334 are examples of the Tuscan cornice. The manner of obtaining the shadows is evident.

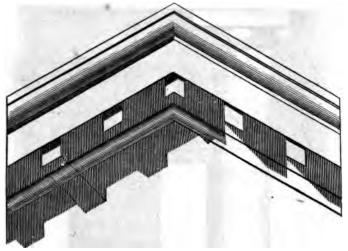


Fig. 334.

430.—Reflected light. In shading, the finish and life of an object depend much on reflected light This is seen to advantage in Fig. 330 and on the column in Fig. 332. Reflected rays are thrown in a direction exactly the reverse of direct rays; therefore, on that part of an object which is subject to reflected light, the shadows are reversed. The fillet of the ovolo in Fig. 330 is an example of this. On the right-hand side of the column, the face of the fillet is much darker than the cove directly under it. The reason of this is, the face of the fillet is deprived both of direct and reflected light, whereas the cove is subject to the latter. Other instances of the effect of reflected light will be seen in the other examples.

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GLOSSARY.

Terms not found here can be found in the lists of definitions in other parts of this book, or in common dictionaries.

Abacus.-The uppermost member of a capital.

Abbatoir.--- A slaughter-house.

Abbey.-The residence of an abbot or abbess.

Abutment.—That part of a pier from which the arch springs. Acanthus.—A plant called in English, bear's-breech. Its leaves are employed for decorating the Corinthian and the Composite capitals.

Acropolis.—The highest part of a city; generally the citadel. Acroteria.—The small pedestals placed on the extremities and apex of a pediment, originally intended as a base for sculpture.

Aisle.—Passage to and from the pews of a church. In Gothic architecture, the lean-to wings on the sides of the nave.

Alcove.-Part of a chamber separated by an estrade, or partition of columns. Recess with seats, &c., in gerdens.

Altar.-A pedestal whereon sacrifice was offered. In modern churches, the area within the railing in front of the pulpit.

Alto-relievo .- High relief; sculpture projecting from a surface so as to appear nearly isolated.

Amphitheatre.—A double theatre, employed by the ancients for the

exhibition of gladiatorial fights and other shows. Ancones.—Trusses employed as an apparent support to a cornice upon the flanks of the architrave.

Annulet.--- A small square moulding used to separate others; the fillets in the Doric capital under the ovolo, and those which separate the flutings of columns, are known by this term.

Antæ.---A pilaster attached to a wall.

Apiary.—A place for keeping beehives.

Arabesque.--A building after the Arabian style.

Areostyle .- An intercolumniation of from four to five diameters.

Arcade-A series of arches.

Arch.-An arrangement of stones or other material in a curviline form, so as to perform the office of a lintel and carry superincumbent weights.

Architrave.-That part of the entablature which rests upon the capital of a column, and is beneath the frieze. The casing and mouldings about a door or window.

Archivolt.--The ceiling of a vault : the under surface of an arch. Area.-Superficial measurement. An open space, below the level

of the ground, in front of basement windows.

Arsenal.-A public establishment for the deposition of arms and arlike stores.

Astragal.-A small moulding consisting of a half-round with a fillet on each side.

Attic.-A low story erected over an order of architecture. A low additional story immediately under the roof of a building.

Aviary.-A place for keeping and breeding birds.

Balcony.-An open gallery projecting from the front of a building. Baluster.—A small pillar or pilaster supporting a rail.

Balustrade.—A series of balusters connected by a rail. Barge-course.—That part of the covering which projects over the gable of a building.

Base.—The lowest part of a wall, column, &c.

Basement-story.-That which is immediately under the principal story, and included within the foundation of the building.

Basso-relievo.-Low relief; sculptured figures projecting from a surface one-half their thickness or less. See Alto-relievo.

Battering.—See Talus.

Battlement.-Indentations on the top of a wall or parapet.

Bay-window.---A window projecting in two or more planes, and not forming the segment of a circle.

Bazaar.-A species of mart or exchange for the sale of various articles of merchandise.

Bead.-A circular moulding.

Bed-mouldings.-Those mouldings which are between the corona and the frieze.

Belfry .--- That part of a steeple in which the bells are hung: anciently called campanile.

Belvedere.-An ornamental turret or observatory commanding a pleasant prospect.

Bow-window.---A window projecting in curved lines.

Bressummer.-Abeam or iron tie supporting a wall over a gateway or other opening.

Brick-nogging.—The brickwork between stude of partitions.

Buttress.—A projection from a wall to give additional strength.

Cable.—A cylindrical moulding placed in flutes at the lower part of the column.

Camber.-To give a convexity to the upper surface of a beam.

Campanile.---A tower for the reception of bells, usually, in Italy, **theparated** from the church.

Canopy.—An ornamental covering over a seat of state.

Cantalivers .- The ends of rafters under a projecting roof. Pieces of wood or stone supporting the eaves.

Capital.-The uppermost part of a column included between the shaft and the architrave.

Caravansera.-In the East, a large public building for the reception of travellers by caravans in the desert.

Carpentry.-(From the Latin, carpentum, carved wood.) That department of science and art which treats of the disposition, the construction and the relative strength of timber. The first is called descriptive, the second constructive, and the last mechanical carpentry.

Caryatides.-Figures of women used instead of columns to support an entablature.

Casino.—A small country-house.

Castellated .- Built with battlements and turrets in imitation of ancient castles.

Castle.-A building fortified for military defence. A house with towers, usually encompassed with walls and moats, and having a donjon, or keep, in the centre.

Catacombs.-Subterraneous places for burying the dead.

Cathedral.-The principal church of a province or diocese, wherein the throne of the archbishop or bishop is placed.

Cavetto.-A concave moulding comprising the quadrant of a circle.

Cemetery.—An edifice or area where the dead are interred. Cenotaph.—A monument erected to the memory of a person buried in another place.

Centring.-The temporary woodwork, or framing, whereon any vaulted work is constructed.

Cesspool.-A well under a drain or pavement to receive the wastewater and sediment.

Chamfer.-The bevilled edge of any thing originally right-angled.

Chancel.-That part of a Gothic church in which the altar is placed. Chantry.-A little chapel in ancient churches, with an endowment

for one or more priests to say mass for the relief of souls out of purgatory

Chapel.—A building for religious worship, erected separately from a church, and served by a chaplain.

Chaplet .- A moulding carved into beads, olives, &c.

Cincture.-The ring, listel, or fillet, at the top and bottom of a column, which divides the shaft of the column from its capital and base.

Circus.-A straight, long, narrow building used by the Romans for the exhibition of public spectacles and chariot races. At the present day, a building enclosing an arena for the exhibition of feats of horsemanship.

Clere-story .--- The upper part of the nave of a church above the roofs of the aisles.

Cloister.-The square space attached to a regular monastery or large church, having a peristyle or ambulatory around it, covered with a range of buildings.

Coffer-dam.-A case of piling, water-tight, fixed in the bed of a river, for the purpose of excluding the water while any work, such as a wharf, wall, or the pier of a bridge, is carried up.

Collar-beam.—A horizontal beam framed between two principal rafters above the tie-beam.

Collonade.—A range of columns.

Columbarium .- A pigeon-house.

Column.—A vertical, cylindrical support under the entablature of an order.

Common-rafters.—The same as jack-rafters, which see

Conduit.—A long, narrow, walled passage underground, for secret communication between different apartments. A canal or pipe for the conveyance of water.

Conservatory.—A building for preserving curious and rare exotic plants.

Consoles .--- The same as ancones, which see.

Contour.-The external lines which bound and terminate a figure.

Convent.—A building for the reception of a society of religious per-

Coping.—Stones laid on the top of a wall to defend it from the weather.

Corbels.—Stones or timbers fixed in a wall to sustain the timbers of a floor or roof.

Cornice.—Any moulded projection which crowns or finishes the part to which it is affixed.

Corona.—That part of a cornice which is between the crownmoulding and the bed-mouldings.

Cornucopia.—The horn of plenty.

Corridor.—An open gallery or communication to the different apartments of a house.

Cove.—A concave moulding.

Cripple-rafters.—The short rafters which are spiked to the hip-rafter of a roof.

Crockets.—In Gothic architecture, the ornaments placed along the angles of pediments, pinnacles, &c.

Crosettes.—The same as ancones, which see.

Crypt.—The under or hidden part of a building.

Culvert.—An arched channel of masonry or brickwork, built beneath the bed of a canal for the purpose of conducting water under it. Any arched channel for water underground.

Cupola.—A small building on the top of a dome.

Curtail-step.—A step with a spiral end, usually the first of the flight. Cusps.—The pendents of a pointed arch.

Cyma.—An ogee. There are two kinds; the cyma-recta, having the upper part concave and the lower convex, and the cyma-reversa, with the upper part convex and the lower concave.

Dado.—The die, or part between the base and cornice of a pedestal. Dairy.—An apartment or building for the preservation of milk, and the manufacture of it into butter, cheese, &c.

Dead-shoar.—A piece of timber or stone stood vertically in brickwork, to support a superincumbent weight until the brickwork which is to carry it has set or become hard.

Decastyle.—A building having ten columns in front.

Dentils.—(From the Latin, *dentes*, teeth.) Small rectangular blocks used in the bed-mouldings of some of the orders.

Diastyle.—An intercolumniation of three, or, as some say, four diameters.

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Die.—That part of a pedestal included between the base and the cornice; it is also called a *dado*.

Dodecastyle.—A building having twelve columns in front.

Donjon.—A massive tower within ancient castles to which the garrison might retreat in case of necessity.

Dooks.—A Scotch term given to wooden bricks.

Dormer.—A window placed on the roof of a house, the frame being placed vertically on the rafters.

Dormitory.-A sleeping-room.

Dovecote.---A building for keeping tame pigeons. A columbarium.

Echinus.—The Grecian ovolo.

Elevation.—A geometrical projection drawn on a plane at right angles to the horizon.

Entablature.—That part of an order which is supported by the columns; consisting of the architrave, frieze, and cornice.

Eustyle.—An intercolumniation of two and a quarter diameters.

Exchange.—A building in which merchants and brokers meet to transact business.

Extrados.—The exterior curve of an arch.

Façade.—The principal front of any building.

Face-mould—The pattern for marking the plank, out of which handrailing is to be cut for stairs, &c.

Facia, or Fascia.—A flat member like a band or broad fillet.

Falling-mould.—The mould applied to the convex, vertical surface of the rail-piece, in order to form the back and under surface of the rail, and finish the squaring.

Festoon.—An ornament representing a wreath of flowers and leaves.

Fillet.—A narrow flat band, listel, or annulet, used for the separation of one moulding from another, and to give breadth and firmness to the edges of mouldings.

Flutes.—Upright channels on the shafts of columns.

• Flyers.—Steps in a flight of stairs that are parallel to each other.

Forum.—In ancient architecture, a public market; also, a place where the common courts were held, and law pleadings carried on.

. Foundry.—A building in which various metals are cast into moulds or shapes.

Frieze.—That part of an entablature included between the architrave and the cornice.

Gable.—The vertical, triangular piece of wall at the end of a root, from the level of the eaves to the summit.

Gain.—A recess made to receive a tenon or tusk.

Gallery.—A common passage to several rooms in an upper story. A long room for the reception of pictures. A platform raised on columns, pilasters, or piers.

Girder.—The principal beam in a floor for supporting the binding and other joists, whereby the bearing or length is lessened.

Glyph.—A vertical, sunken channel. From their number, those in the Doric order are called *triglyphs*.

Granary.—A building for storing grain, especially that intended to be kept for a considerable time.

Groin.—The line formed by the intersection of two arches, which cross each other at any angle.

Gutta.—The small cylindrical pendent ornaments, otherwise called *drops*, used in the Doric order under the triglyphs, and also pendent from the mutuli of the cornice.

Gymnasium.—Originally, a space measured out and covered with sand for the exercise of athletic games : afterwards, spacious buildings devoted to the mental as well as corporeal instruction of youth.

Hall.—The first large apartment on entering a house. The public room of a corporate body. A manor-house.

Ham.—A house or dwelling-place. A street or village : hence Nottingham, Buckingham, &c. Hamlet, the diminutive of ham, is a small street or village.

Helix.—The small volute, or twist, under the abacus in the Corinthian capital.

Hem.—The projecting spiral fillet of the Ionic capital.

Hexastyle.—A building having six columns in front.

Hip-rafter.—A piece of timber placed at the angle made by two adjacent inclined roofs.

Homestall.—A mansion-house, or seat in the country.

Hotel, or Hostel.—A large inn or place of public entertainment. A large house or palace.

Hot-house.--- A glass building used in gardening.

Hovel.—An open shed.

Hut.—A small cottage or hovel generally constructed of earthy materials, as strong loamy clay, &c.

Impost.—The capital of a pier or pilaster which supports an arch. Intaglio.—Sculpture in which the subject is hollowed out, so that the impression from it presents the appearance of a bas-relief.

Intercolumniation.—The distance between two columns. Intrados.—The interior and lower curve of an arch.

Jack-rafters.—Rafters that fill in between the principal rafters of a roof; called also common-rafters.

Jail.-A place of legal confinement.

Jambs.—'The vertical sides of an aperture.

Joggle-piece.—A post to receive struts.

Joists.—The timbers to which the boards of a floor or the laths of a ceiling are nailed.

Keep .--- The same as donjon, which see.

Key-stone.—The highest central stone of an arch.

Kiln.—A building for the accumulation and retention of heat, in order to dry or burn certain materials deposited within it.

King-post.—The centre-post in a trussed roof.

Knee.-A convex bend in the back of a hand-rail. See Ramp.

Lactarium.—The same as dairy, which see.

Lantern.—A cupola having windows in the sides for lighting an apartment beneath.

Larmier.-The same as corona, which see.

Lattice.—A reticulated window for the admission of air, rather than light, as in dairies and cellars.

Lever-boards.—Blind-slats: a set of boards so fastened that they may be turned at any angle to admit more or less light, or to lap upon each other so as to exclude all air or light through apertures.

Lintel.—A piece of timber or stone placed horizontally over a door, window, or other opening.

Listel.—The same as fillet, which see.

Lobby.—An enclosed space, or passage, communicating with the principal room or rooms of a house.

Lodge.—A small house near and subordinate to the mansion. A cottage placed at the gate of the road leading to a mansion.

Loop.—A small narrow window. Loophole is a term applied to the vertical series of doors in a warehouse, through which goods are delivered by means of a crane.

Luffer-boarding.—The same as lever-boards, which see. Luthern.—The same as dormer, which see.

Mausoleum.—A sepulchral building—so called from a very celebrated one erected to the memory of Mausolus, king of Caria, by his wife Artemisia.

Metopa.—The square space in the frieze between the triglyphs of the Doric order.

Mezzanine.—A story of small height introduced between two of greater height.

Minaret.—A slender, lofty turret having projecting balconies, common in Mohammedan countries.

Minster.—A church to which an ecclesiastical fraternity has been or is attached.

Moat.—An excavated reservoir of water, surrounding a house, castle or town.

Modillion.—A projection under the corona of the richer orders, resembling a bracket.

Module.—The semi-diameter of a column, used by the architect as a measure by which to proportion the parts of an order.

Monastery.—A building or buildings appropriated to the reception of monks.

Monopteron.—A circular collonade supporting a dome without an enclosing wall.

Mosaic.—A mode of representing objects by the inlaying of small cubes of glass, stone, marble, shells, &c.

Mosque.---A Mohammedan temple, or place of worship.

Mullions.—The upright posts or bars, which divide the lights in a Gothic window.

Muniment-house.—A strong, fire-proof apartment for the keeping and preservation of evidences, charters, seals, &c., called muniments. 1* Museum.—A repository of natural, scientific and literary, ouriosities, or of works of art.

Mutule.—A projecting ornament of the Doric cornice supposed to represent the ends of rafters.

Nave.—The main body of a Gothic church.

Newel.-A post at the starting or landing of a flight of stairs.

Nicke.—A cavity or hollow place in a wall for the reception of a statue, vase, &co.

Nogs.—Wooden bricks.

Nosing.—The rounded and projecting edge of a step in stairs.

Nunnery.—A building or buildings appropriated for the reception of nuns.

Obelisk.—A lofty pillar of a rectangular form.

Octastyle,—A building with eight columns in front.

Odeam.—Among the Greeks, a species of theatre wherein the poets and musicians rehearsed their compositions previous to the public production of them.

Ogee.—See Cyma.

Orangery.—A gallery or building in a garden or parterre fronting the south.

Oricl-window.—A large bay or recessed window in a hall, chapel, or other apartment.

Ovolo.—A convex projecting moulding whose profile is the quadrant of a circle.

Pagoda.-A temple or place of worship in India.

Palisade.—A fence of pales or stakes driven into the ground.

. Parapet.—A small wall of any material for protection on the sides of bridges, quays, or high buildings.

Pavilion.—A turret or small building generally insulated and comprised under a single roof.

Pedestal.—A square foundation used to elevate and sustain a column, statue, &c.

Pediment.—The triangular crowning part of a portico or aperture which terminates vertically the sloping parts of the roof: this, in Gothic architecture, is called a *gable*.

Penitentiary.—A prison for the confinement of criminals whose orimes are not of a very heinous nature.

Piazza.—A square, open space surrounded by buildings. This term is often improperly used to denote a *portico*.

Pter.—A rectangular pillar without any regular base or capital. The upright, narrow portions of walls between doors and windows are known by this term.

Pilaster.—A square pillar, sometimes insulated, but more common by engaged in a wall, and projecting only a part of its thickness.

Piles.—Large timbers driven into the ground to make a secure foundation in marshy places, or in the bed of a river.

Pillar.-A column of irregular form, always disengaged, and al-

ways deviating from the proportions of the orders ; whence the distinction between a pillar and a column.

Pinnacle.—A small spire used to ornament Gothic buildings.

Planceer .- The same as soffit, which see.

Plinth.-The lower square member of the base of a column, pedestal, or wall.

Porch.-An exterior appendage to a building, forming a covered approach to one of its principal doorways.

Portal.-The arch over a door or gate; the framework of the gate; the lesser gate, when there are two of different dimensions at one entrance.

Portcullis.---A strong timber gate to old castles, made to slide up and down vertically.

Portico.-A colonnade supporting a shelter over a walk, or ambulatory.

Priory.-A building similar in its constitution to a monastery or abbey, the head whereof was called a prior or prioress.

Prism.-A solid bounded on the sides by parallelograms, and on the ends by polygonal figures in parallel planes.

Prostyle.—A building with columns in front only.

Purlines.-Those pieces of timber which lie under and at right angles to the rafters to prevent them from sinking.

Pycnostyle.—An intercolumniation of one and a half diameters.

Pyramid.—A solid body standing on a square, triangular or polygonal basis, and terminating in a point at the top.

Quarry.—A place whence stones and slates are procured. Quay.—(Pronounced, key.) A bank formed towards the sea or on the side of a river for free passage, or for the purpose of unloading merchandise.

Quoin.—An external angle. See Rustic quoins.

Rabbet, or Rebate.—A groove or channel in the edge of a board. Ramp.-A concave bend in the back of a hand-rail.

Rampant arch.-One having abutments of different heights.

Regula.-The band below the tænia in the Doric order.

Riser .- In stairs, the vertical board forming the front of a step.

Rostrum.-An elevated platform from which a speaker addresses an audience.

Rotunda.—A circular building.

Rubble-wall.-A wall built of unhewn stone.

Rudenture.---The same as cable, which see.

Rustic quoins.—The stones placed on the external angle of a build. ing, projecting beyond the face of the wall, and having their edges bevilled.

Rustic-work.-A mode of building masonry wherein the faces of the stones are left rough, the sides only being wrought smooth where the union of the stones takes place.

Salon, or Saloon.—A lofty and spacious apartment comprehending the height of two stories with two tiers of windows.

Sarcophagus.---A tomb or coffin made of one stone.

Scantling.—The measure to which a piece of timber is to be or has been cut.

Scarfing.—The joining of two pieces of timber by bolting or nailing transversely together, so that the two appear but one.

Scotia.—The hollow moulding in the base of a column, between the fillets of the tori.

Scroll.—A carved curvilinear ornament, somewhat resembling in profile the turnings of a ram's horn.

Sepulchre.-A grave, tomb, or place of interment.

Sever.—A drain or conduit for carrying off soil or water from any place.

Shaft.—The cylindrical part between the base and the capital of a column.

Shoar.—A piece of timber placed in an oblique direction to support a building or wall.

Sill.—The horizontal piece of timber at the bottom of framing; the timber or stone at the bottom of doors and windows.

Soffit—The underside of an architrave, corona, &c. The underside of the heads of doors, windows, &c.

Summer.—The lintel of a door or window; a beam tenoned into a girder to support the ends of joists on both sides of it.

Systyle.—An intercolumniation of two diameters.

Tania.—The fillet which separates the Doric frieze from the architrave.

Talus.—The slope or inclination of a wall, among workmen called battering.

Terrace.—An area raised before a building, above the level of the ground, to serve as a walk.

Tesselated pavement.—A curious pavement of Mosaic work, composed of small square stones.

Tetrastyle.—A building having four columns in front.

Thatch.—A covering of straw or reeds used on the roofs of cottages, barns, &c.

Theatre.—A building appropriated to the representation of drama...c spectacles.

Tile.—A thin piece or plate of baked clay or other material used for the external covering of a roof.

Tomb.—A grave, or place for the interment of a human body, including also any commemorative monument raised over such a place.

Torus.—A moulding of semi-circular profile used in the bases of columns.

Tower.—A lofty building of several stories, round or polygonal.

Transept.—The transverse portion of a cruciform church.

Transom.—The beam across a double-lighted window; if the window have no transom, it is called a *clere-story* window.

Tread.—That part of a step which is included between the face of its riser and that of the riser above.

Trellis.-A reticulated framing made of thin bars of wood for screens, windows, &c.

Triglyph.-The vertical tablets in the Doric frieze, chamfered on the two vertical edges, and having two channels in the middle.

Tripod.—A table or seat with three legs.

Trochilus.-The same as scotia, which see.

Truss.—An arrangement of timbers for increasing the resistance to cross-strains, consisting of a tie, two struts and a suspending-piece.

Turret.—A small tower, often crowning the angle of a wall, &c.

Tusk-A short projection under a tenon to increase its strength.

Tympanum.-The naked face of a pediment, included between the level and the raking mouldings.

Underpinning.—The wall under the ground-sills of a building.

University.—An assemblage of colleges under the supervision of a senate, &c.

Vault.--- A concave arched ceiling resting upon two opposite parallel walls.

Venetian-door.---A door having side-lights.

Venetian-window.—A window having three separate apertures.

Veranda.-An awning. An open portico under the extended roof of a building.

Vestibule.—An apartment which serves as the medium of communication to another room or series of rooms.

Vestry.-An apartment in a church, or attached to it, for the preservation of the sacred vestments and utensils.

Villa.—A country-house for the residence of an opulent person.

Vinery.—A house for the cultivation of vines.

Volute.—A spiral scroll, which forms the principal feature of the Ionic and the Composite capitals.

Voussoirs .--- Arch-stones

Wainscoting.—Wooden lining of walls, generally in panels. Water-table.—The stone covering to the projecting foundation or other walls of a building.

Well.-The space occupied by a flight of stairs. The space left beyond the ends of the steps is called the well-hole.

Wicket.—A small door made in a gate.

Winders.—In stairs, steps not parallel to each other.

Zophorus.—The same as frieze, which see.

Zystos.—Among the ancients, a portico of unusual length, commonly appropriated to gymnastic exercises.

TABLE OF SQUARES, CUBES, AND ROOTS.

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2	4	8	1.4142136		69	4761	328509	8.3066239	
3	9	27	1.7320508	1.442250	70 71	4900	343000	8.3666003	
345678	16	64	2.0000000		71	5041	357911	8-4261498	4-14081
5	25	125	2.2360680		72	5184	373248	8-4852814	4.16016
0	36	216	2.4494897		73	5329	389017	8.5440037	
6	49 64	343	2.6457513		74	5476	405224	8.6023253	
9		512 729	2.8284271		75	5625 5776	421875 438976	8.6602540	
10	* 81 100	1000	3.0000000		76	5929	456533	8-7177979	
11	121	1331	3.1622777 3.3166248	2-154435 2-223980	77	6084	474552	8·7749644 8·8317609	
12	144	1728	3.4641016		79	6241	493039	8.8881944	
13	169	2197	3.6055513		80	6400	512000	8.9442719	
12 13 14	196	2744	3.7416574		81	6561	531441	9-0000000	
15	225	3375	3.8729833		82	6724	551368	9.0553851	4.34448
16	256	4096	4.0000000		83	6889	571787	9-1104336	4.36207
17	289	4913	4.1231056	2.571232	84	7056	592704	9.1651514	
18	324	5832	4.2426407	2.620741	85	7225	614125	9.2195445	
19	361	6859	4-3588989		86	7396	636056	9.2736185	
20 21	400	8000	4.4721360		87	7569	658503	9.3273791	4-43104
22	441	9261 10648	4.5825757	2.758924	88	7744	681472	9.3808315	4-44796
23	484 529	12167	4.6904158	2.802039	89	7921 8100	704969	9-4339811	4-46474
24	576	13824	4.7958315		90 91	8281	729000 753571	9·4868330 9·5393920	4.48140
25	625	15625	5.0000000	2.924018	91	8464	778688	9.5916630	4.51435
26	676	17576	5.0990195	2.962496	93	8649	804357	9.6436508	4-53065
27	729	19683	5.1961524	3.000000	94	8836	830584	9.6953597	4.54683
28	784	21952	5 2915026	3.036589	95	9025	857375	9.7467943	4.56290
29	841	24389	5.3851648	3.072317	96	9216	884736	9.7979590	4.57885
30	900	27000	5.4772256		97	9409	912673	9.8488578	4.59170
31	961	29791	5.5677644	3.141331	98	9604	941192	9.8994949	4.61043
32	1024	32768	5.6568542	3.174802	99	9801	970299	9.9498744	4-62606
33	1089	35937	5.7445626	3.207534	.100	10000	1000000	10.0000000	4.64158
34 35	1156	39304 42875	5.8309519		101	10201	1030301	10.0498755	4 65700
36	1225 1296	46656	5.9160798	3.271066	102	10404	1061208	10.0995049	4.67232
37	1369	50653	6.0000000 6.0827625	3-301927 3-332222	103 104	10609	1092727 1124864	10-1488916	4.68754
38	1444	54872	6.1644140		104	10816 11025	1157625	10.1980390 10.2469508	4-70266 4-71769
39	1521	59319	6.2449980	3-391211	106	11236	1191016	10-2956301	4.73262
40	1600	64000	6.3245553	3 419952	107	11449	1225043	10.3440804	4.74745
41	1681	68921	6-4031242	3.448217	108	11664	1259712	10-3923048	4.76220
42	1764	74088	6-4807407	3.476027	109	11881	1295029	10.4403065	4.77685
43	1849	79507	6.5574385	3.503398	110	12100	1331000	10.4880885	4.79142
44	1936	85184	6.6332496	3.530348	111	12321	1367631	10.5356538	4.80589
45	2025	91125	6.7082039	3.556893	112	12544	1404928	10.5830052	4.82028
46	2116	97336	6.7823300	3.583048	113	12769	1442897	10.6301458	4.83458
47 48	2209	103323	6-8556546	3.608826	114	12996	1481544	10.6770783	4.84880
48	2304 2401	110592 117649	6.9282032		115	13225	1520875	10 7238053	4.86294
49 50	2401	125000	7-0000000	3.659306	116	13456	1560896	10.7703296	4.87699
51	2601	132651	7.0710678	3.684031	117	13689	1601613	10.8166538	4.89097
52	2704	140608	7:2111026	3.708430	118	13924	1643032	10.8627805	4.90486
53	2809	148877	7.2301099	3·732511 3·756286	119 120	14161 14400	1685159 1728000	10.9087121 10.9544512	4.93245
54	2916	157464	7.3184692	3.779763	121	14641	1771561	11.0000000	4.94608
55	3025	166375	7.4161985	3.802952	122	14884	1815848	11.0453610	4-95967
56	3136	175616	7.4833148	3.825862	123	15129	1860867	11.0905365	4.97319
57	3249	185193	7.5198344	3.848501	124	15376	1906624	11.1355287	4.9866
58	3364	195112	7.6157731	3.870877	125	15625	1953125	11.1803399	5.00000
59	3481	205379	7.6811457	3.892996	126	15876	2000376	11.2249722	5.01329
60	3600	216000	7.7459667	3.914868	127	16129	2048383	11.2694277.	5.02652
61	3721	226981	7.8102497	3.936497	128	16384	2097152	11.3137085	5.03968
62	3844	238328	7.8740079	3.957891	129	16641	2146689	11.3578167	5.05277
63	3969	250047	7.9372539	3.979057	130	16900	2197000	11.4017543	5.06579
64	4096	262144	8.0000000	4.000000	131	17161	2248091	11.4455231	5.07875
65 66	4225	274625	8-0622577	4.020726	132	17424	2299968	11.4891253	5.09164
67	4356	287496 300763	8.1240334	4.041240	133	17689	2352637	11.5325626	5.10446
01	4489	300103	8.1853528	4.061548	134	17956	2406104	11.5758369	5.11723

No.	Square.	Cube,	Sq. Root.	CubeRoot.	No.	Square.	Cube.	Sq. Root.	CubeRoo
135	18225	2460375	11-6189500	5.129928	202	40804	8242408	14-2126704	5.86746
136	18496	2515456	11.6619038	5.142563	203	41209	8365427	14.2478068	5.87713
137	18769	2571353	11.7046999	5.155137	204	41616	8489664	14:2828569	5.88676
138	19044	2628072	11.7473401	5.167649	205	42025	8615125	14:3178211	5.89636
139	19321	2685619	11.7898261	5-180101	206	42436	8741816	14.3527001	5.90594
140	19600	2744000	11.8321596	5.192494	207	42849	8869743	14.3874946	5.91548
141	19881	2803221	11.8743422	5.204828	208	43264	8998912	14.4222051	5.92499
142	20164	2863288	11.9163753	5.217103	209	43681	9129329	14:4568323	5.93447
143	20449		11.9582607	5-229321	210	44100	9261000		5.94392
		2924207						14-4913767	
144	20736	2985984	12.0000000	5.241483	211	44521	9393931	14.5258390	5.95334
145	21025	3048625	12.0415946		212	44944	9528128	14.5602198	5.96273
146	21316	3112136	12.0830460	5.265637	213	45369	9663597	14.5945195	5.97209
147	21609	3176523	12.1243557	5.277632	214	45796	9800344	14 6287338	5.9814
148	21904	3241792	12.1655251	5.289572	215	46225	9938375	14 6628783	5.99072
149	22201	3307949	12.2065556	5.301459	216	46656	10077696	14.6969385	6.00000
150	22500	3375000	12.2474487	5.313293	217	47089	10218313	14-7309199	6.00924
151	22801	3442951	12.2882057	5.325074	218	47524	10360232	14.7648231	6.01846
152	23104	3511808	$12 \cdot 3288280$		219	47961	10503459	14.7986486	6.02765
153	23409	3581577	12.3693169	5.348481	220	48400	10648000	14.8323970	6.03681
154	23716	3652264	12.4096736	5.360108	221	48841	10793861	14.8660687	6.04594
	24025		12-4096730	5.371685	222	49284	10941048	14.8996644	6.05504
155		3723875			223		11089567		6.06415
156	24336	3796416	12.4899960	5.383213		49729		14.9331845	
157	24649	3869893	12.5299641	5.394691	224	50176	11239424	14-9666295	6.0731
158	24964	3944312	12.5698051	5-406120	225	50625	11390625	15.0000000	6.08220
159	25281	4019679	12.6095202	5.417501	226	51076	11543176	15-0332964	6.09119
160	25600	4096000	12.6491106	5.428835	227	51529	11697083	15-0665192	6.10017
161	25921	4173281	12.6885775	5.440122	228	51984	11852352	15.0996689	6.10911
162	26244	4251528	12.7279221	5.451362	229	52441	12008989	15-1327460	6.11803
163	26569	4330747	12.7671453	5.462556	230	52900	12167000	15-1657509	6.12692
164	26896	4410944	12.8062485	5.473704	231	53361	12326391	15-1986842	6-13579
165	27225	4492125	12.8452326	5.484807	232	53824	12487168	15.2315462	6-14463
166	27556	4574296	12.8840987	5.495865	233	54289	12649337	15-2643375	6.15344
100				5.506878			12812904		6.16224
167	27889	4657463	12.9228480		234	54756		15-2970585	6.1710
168	28224	4741632	12.9614814	5.517848	235	55225	12977875	15.3297097	6-17100
169	28561	4826809	13.0000000	5.528775	236	55696	13144256	15.3622915	6.17974
170	28900	4913000	$13 \cdot 0384048$		237	56169	13312053	15.3948043	6.18846
171	29241	5000211	13.0766968	5.550499	238	56644	13481272	15 4272486	6-19715
172	29584	5088448	13-1148770	5.561298	239	57121	13651919	15.4596248	6-20582
173	29929	5177717	13.1529464	5.572055	240	57600	13824000	15-4919334	6.21446
174	30276	5268024	13.1909060	5.582770	241	58081	13997521	15.5241747	6.22308
175	30625	5359375	13-2287566	5.593445	242	58564	14172488	15.5563492	6-23168
176	30976	5451776	13-2664992	5.604079	243	59049	14348907	15.5884573	6.24025
177	31329	5545233	13.3041347	5.614672	244	59536	14526784	15.6204994	6-24880
178	31684		13-3416641	5.625226		60025	14706125	15.6524758	6.2573
179	32041	5639752 5735339	13.3790882		245	60516	14886936	15 6843871	6-26582
					246				
180	32400	5832000	13-4164079	5.646216	247	61009	15069223	15.7162336	6.27430
181	32761	5929741	13-4536240		248	61504	15252992	15.7480157	6-28276
182	33124	6028568	13 4907376	5.667051	249	62001	15433249	15.7797338	6-29119
183	33489	6128487	13.5277493		250	62500	15625000	15-8113883	6.29960
184	33856	6229504	13.5646600	5-687734	251	63001	15813251	15.8429795	6.30799
185	34225	6331625	13.6014705	5-698019	252	63504	16003008	15.8745079	6-31636
186	34596	6434856	13-6381817	5.708267	253	64009	16194277	15.9059737	6.32470
187	34969	6539203	13.6747943		254	64516	16387064	15.9373775	6.33305
188	35344	6644672	13.7113092		255	65025	16581375	15-9687194	6.3413
189	35721	6751269	13.7477271	5.738794	256	65536	16777216	16.0000000	6.34960
190	36100	6859000	13.7840488		257	66049	16974593	16.0312195	6-35786
191	36481		13.8202750		258	66564	17173512	16.0623784	6.36609
		6967871							
192	36864	7077888	13.8564065		259	67081	17373979	16.0934769	6.37431
193	37249	7189057	13-8924440		260	67600	17576000	16.1245155	6.38250
194	37636	7301384	13.9283883		261	68121	17779581	16.1554944	6.39067
195	38025	7414875	13 9642400		262	68644	17984728	16-1864141	6.39889
196	38416	7529536	14.0000000	5.808786	263	69169	18191447	16-2172747	6.40695
197	38809	7645373	14-0356688		264	69696	18399744	16.2480768	6.41506
198	39204	7762392	14-0712473		265	70225	18609625	16-2788206	6.4231
199	39601	7880599	14.1067360		266	70756	18821096	16.3095064	6.43129
200	40000	8000000	14-1421356		267	71289	19034163	16-3401346	6.43927
	10000	0000000	TT 1141000	000000	1001	11000		10 0101010	1 10000

APPENDIX

No.	Square.	Cube.	Sq. Root.	CubeRoot.	No.	Square.	Cube.	Sq Root.	CubeRoo
269	72361	19465109	16-4012195	6-455315	336	112896	37933056	18.3303028	6-9520
270	72900	19683000	16-4316767	6-463304	337	113569	38272753	18.3575598	6-9589
271	73441	19902511	16-4620776	6-471274	338	114244	38614472	18.3847763	6-9658
272	73984	20123648	16-4924225		339	114921	38958219	18.4119526	6.9726
273	74529	20346417	16.5227116		340	115600	39304000	18.4390889	6-9795
274	75076	20570824	16-5529454		341	116281	39651821	18.4661853	6-9863
275	75625	20796875	16.5831240		342	116964	40001688	18.4932420	6-9931
276	76176	21024576	16.6132477	6.510830	343	117649	40353607	18.5202592	7.0000
277	76729	21253933	16.6433170		344	118336	40707584	18.5472370	7.0067
278	77284	21484952	16.6733320	6.526519	345	119025	41063625	18.5741756	7-0135
279	77841	21717639	16.7032931	6.534335	346	119716	41421736	18.6010752	7.0203
280	78400	21952000	16.7332005	6.542133	347	120409	41781923	18 6279360	7-0271
281	78961	22188041	16.7630546	6.549912	348	121104	42144192	18.6547581	7.0338
282	79524	22425768	16.7928556	6.557672	349	121801	42508549	18.6815417	7.0405
283	80089	22665187	16-8226038	6.565414	350	122500	42875000	18.7082869	7-0472
284	80656	22906304	16-8522995	6.573139	351	123201	43243551	18.7349940	7.0540
285	81225	23149125		6.580844	352	123904	43614208		7-0606
286	81796	23393656	16-8819430	6.588532	353	124609	43985977	18-7616630	
287	82369		16 9115345		354		44361864	18.7882942	7.0673
288		23639903	16-9410743			125316		18.8148877	7.0740
	82944	23887872	16-9705627	6.603854	355	126025	44738875	18-8414437	7-0806
289	83521	24137569	17-0000000	6-611489	356	126736	45118016	18.8679623	7.0873
290	84100	24389000	17-0293864	6.619106	357	127449	45499293	18.8944436	7.0939
291	84681	24642171	17.0587221	6.626705	358	128164	45882712	18.9208879	7.1005
292	85264	24897088	17.0880075	6.634287	359	128881	46268279	18-9472953	7.1071
293	85849	25153757	17-1172428	6.641852	360	129600	46656000	18.9736660	7.1137
294	86436	25412184	17.1464282	6.649400	361	130321	47045981	19.0000000	7.1203
295	87025	25672375	17.1755640	6:656930	362	131044	47437928	19.0262976	7.1269
296	87616	25934336	17.2046505	6.664444	363	131769	47832147	19.0525589	7.1334
297	88209	26198073	17.2336879	6.671940	364	132496	48228544	19.0787840	7.1400
298	88804	26463592	17.2626765	6.679420	365	133225	48627125	19.1049732	7.1465
299	89401	26730899	17.2916165	6.686883	366	133956	49027896	19-1311265	7.1530
300	90000	27000000	17.3205081	6.694329	367	134689	49430863	19.1572441	7.1595
301	90601	27270901	17.3493516		368	135424	49836032	19.1833261	7-1660
302	91204	27543608	17.3781472		369	136161	50243409	19.2093727	7.1725
303	91809	27818127	17-4068952		370	136900	50653000	19-2353841	7.1790
304	92416	28094464	17-4355958		371	137641	51064811	19-2613603	7.1855
305	93025	28372625	17-4642492		372	138384	51478848	19-2873015	7-1919
306	93636	29652616	17-4928557	6.738664	373	139129	51895117	19.3132079	7.1984
307	94249	28934443	17.5214155	6.745997	374	139876	52313624	19.3390796	7.2048
308	94864	29218112	17.5499288	6.753313	375	140625	52734375	19.3649167	7.2115
309	95481	29503629	17.5783958	6.760614	376	141376	53157376	19-3907194	7-2176
310	96100	29791000	17.6068169	6.767899	377	142129	53582633		7.2240
311	96721	30080231	17-6351921			142884		19-4164878	7.2304
312	97344	30371328	17.6635217	6.775169	378 379	143641	54010152	19-4422221	7.236
313	97969	30664297		6.782423			54439939	19.4679223	
314	98596	30959144	17-6918060		380	144400	54872000	19.4935887	7-243
315	99225	31255875	17.7200451	6.796884	381	145161	55306341	19.5192213	7-249
316	99856	31554496	17.7482393		382	145924	55742968	19.5448203	7.2558
317	100489		17.7763388	6.811285	383	146689	56181887	19.5703858	7.262
318	101124	31855013 32157432	17-8044938	6.818462	384	147456	56623104	19.5959179	7-2684
319	101761	32461759	17-8325545	6.825624	385	148225	57066625	19.6214169	7.274
320	102400	32768000	17-8605711	6.832771	386	148996	57512456	19.6468827	7.2810
321	103041		17.8885438	6.839904	387	149769	57960603	19.6723156	7.287
322	103684	33076161 33386248	17.9164729	6.847021	388	150544	58411072	19.6977156	7.293
323			17.9443584	6.854124	389	151321	58863869	19.7230829	7-2998
324	104329	33698267	17-9722008	6.861212	390	152100	59319000	19-7484177	7-3061
325	104976	34012224	18-0000000		391	152881	59776471	19-7737199	7.312
	105625	34328125	18.0277564	6.875344	392	153664	60236288	19.7989899	7.3180
326	106276	34645976	18.0554701	6.882389	393	154449	60693457	19.8242276	7.3248
327	106929	34965783	18-0831413		394	155236	61162984	19.8494332	7.3310
328	107584	35287552	18-1107703		395	156025	61629875	19.8746069	7.3375
329	108241	35611289	18-1333571	6.903436	396	155816	62099136	19-8997487	7.3434
330	108900	35937000	18-1659021	6.910423	397	157609	62570773	19.9248588	7.3495
331	109561	36264691	18-1934054	6.917396	398	158404	63044792	19.9499373	7.3557
332	110224	36594368	18-2208672		399	159201	63521199	19.9749844	7.3619
333	110889	36926037	18-2482376	6.931301	400	160000	64000000	20.0000000	7.3680
334	111556	37259704	18-2756669		401	160801	64481201	20-0249844	7.3741
335	112225	37595375	18-3030052		402	161604	64964808	20.0499377	7-3303

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APPENDIX.

	Cube.	Sq. Root.	CubeRoot	No.	Square.	Cube.	Sq. Root.	CubeRoot
162409	65450827	20.0748599	7.336437	470	220900	103823000	21.6794834	7.77498
163216	65939264	20.0997512		471	221841	104487111	21.7025344	7-78049
164025		20.1246118		472	222784	105154048	21.7255610	7.78599
164836	66923416	20.1494417	7.404721	473	223729	105823817	21.7485632	7.79148
165649	67419143	20-1742410	7.410795	474	224676	106496424	21.7715411	7.79697
166464	67917312	20.1990099	7.416859	475	225625	107171875	21.7944947	7.80245
167281	68417929	20-2237484	7.422914	476	226576	107850176	21.8174242	7.80792
168100		20.2484567	7.428959	477	227529	108531333	21.8403297	7.81338
168921	69426531	20.2731349	7.434994	478	228484	109215352	21.8632111	7.81884
169744	69934528	20.2977831	7.441019	479	229441	109902239	21.8860686	7.82429
170569	70444997	20.3224014	7.447034	480	230400	110592000	21.9089023	7.82973
171396	70957944	20.3469899	7.453040	481	231361	111284641	21.9317122	7.83516
172225	71473375	20.3715488	7.459036	482	232324	111980168	21.9544934	7.84059
173056		20-3960781	7.465022	483	233289	112678587	21-9772610	7.84601
173889	72511713	20.4205779	7.470999	484	234256	113379904	22.0000000	7.85142
174724	73034632	20.4450483		485	235225	114084125	22.0227155	7.85682
175561	73560059	20.4694895	7.482924	486	236196 237169	114791256	22 0454077	7.86222
176400		20-4939015	7.488872	487	238144	115501303	22.0680765	7.86761
177241	74618461	20.5182845	7.494811	488	239121	116214272 116930169	22.0907220 22.1133444	7·87299 7·87836
178084	75151448 75686967	20.5426386 20.5669638	7.500741	489 490	240100	117649000	22-1359436	7.88373
178929	76225024	20.5912603	7·506661 7·512571	490	241081	118370771	22.1585198	7-88909
179776 180625	76765625	20.6155281	7.518473	492	242064	119095488	22.1810730	7.89444
181476	77308776	20.6397674	7.524365	493	243049	119823157	22.2036033	7.89979
182329	77854483	20.6639783	7.530248	494	244036	120553784	22-2261108	7.90512
183184	78402752	20.6881609	7.536122	495	245025	121287375	22-2485955	7.91046
184041	78953589	20.7123152		496	246016	122023936	22.2710575	7.91578
184900	79507000	20.7364414	7.547842	497	247009	122763473	22-2934968	7.92109
185761	80062991	20.7605395	7.553689	498	248004	123505992	22.3159136	7.92640
186624	80621568	20.7846097	7:559526	499	249001	124251499	22.3333079	7.93171
187489		20.8086520	7.565355	500	250000	125000000	22.3606798	7.93700
188356	81746504	20.8326667	7.571174	501	251001	125751501	22.3830293	7.94229
189225	82312875	20-8566536		502	252004	126506008	22.4053565	7.94757
190096	82881856	20.8806130	7.582786	503	253009	127263527	22.4276615	7.95284
190969	83453453	20.9045450	7.588579	504	254016	128024064	22.4499443	7.95811
191844	84027672	20.9284495	7.594363	505	255025	128787625	22.4722051	7.96337
192721	84604519	20.9523268	7.600138	506	256036	129554216	22-4944438	7.96862
193600	85184000	20.9761770	7.605905	507	257049	130323843	22:5166605	7.97387
194481	85766121	21.0000000	7.611663	508	253064	131096512	22.5388553	7.97911
195364	86350888	21.0237960	7.617412	509	259081	131872229	22.5610283	7.98434
196249	86938307	21.0475652	7.623152	510	260100	132651000	22.5831796	7.98957
197136	87528384	21.0713075	7.628884	511	261121	133432831	22.6053091	7-99478
198025	88121125	21.0950231	7.634607	512	262144	134217728	22.6274170 22.6495033	8.00000
198916	88716536	21-1187121	7 640321	513	263169	135005697		8-00520
199809	89314623	21.1423745	7.646027	514	264196 265225	135796744 136590875	22.6715681 22.6936114	8-01040 8-01559
200704	89915392	21-1660105 21-1896201	7.651725 7.657414	515	266256	137388096	22.7156334	8-02077
201601 202500	90518849 91125000	21-2132034	7.663094	516 517	267289	138188413	22.7376340	8.02595
202500	91125000	21-2132034	7.668766	518	268324	138991832	22.7596134	8.03112
203401	91735851 92345408	21-2602916	7.674430	519	269361	139798359	22.7815715	8-03629
204304		21-2837967	7.680086	520	270400	140608000	22.8035085	8-04145
205205		21.3072758	7.685733	521	271441	141420761	22.8254244	8.04660
207025	94196375	21.3307290	7.691372	522	272484	142236648	22.8473193	8-05174
207936		21.3541565	7.697002	523	273529	143055667	22-8691933	8 05688
208849	95443993	21.3775583	7.702625	524	274576	143877824	22.8910463	8.06201
209764	96071912	21.4009346	7.708239	525	275625	144703125	22.9128785	8-06714
210681	96702579	21.4242853	7.713845	526	276676	145531576	22.9346399	8.07226
211600		21.4476106	7.719443	527	277729	146363183	22.9554806	8.07737
212521	97972181	21.4709106	7.725032	528	278784	147197952	22.9782506	8.08248
213444	98611128	21.4941853	7.730614	529	279841	148035889	23.0000000	8.08757
214369	99252847	21.5174348	7.736188	530	280900	148877000	23.0217289	8.09267
215296	99897344	21.5406592	7.741753	531	281961	149721291	23.0434372	8.09775
216225	100544625	21.5633587	7.747311	532	283024		23.0651252	8.10253
217156		$21 \cdot 5870331$	7.752861	533	284089			8.10791
218089		21.6101828		534				8.11298
219024		21.6333077	7.763936	535			23.1300670	8-11804
219961	103161709	21.6564078	7.769462	536	287296	153990656	23.1516738	8.12309
214369 215296 216225 217156 218089 219024		99252847 99897344 100544625 101194696 101847563 102503232	99252847 21:5174348 99897344 21:5406592 100544625 21:563587 101194696 21:5870331 101847563 21:6101828 102503232 21:6333077	99252347 21-5174348 7736183 99897344 21-5406592 7-741753 100544625 21-5633587 7-747311 101194696 21-5870331 7-752861 101847563 21-6101828 7-758402 102502322 21-6333077 7-763036 103161709 21-6564078 7-769462	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	99852847 21-5174348 7736188 530 280900 148877000 23/0217283 99897344 21-5406592 7-741753 531 281961 149721291 23/0434372 100544625 21-563587 7-747311 532 283024 150568768 23/0651852 101194696 21-5870331 7-752861 533 284089 151419437 23/0867928 101847563 21-6101828 7-758402 534 285156 152273304 23/1084400 10250232 21-6330077 7-763936 535 286225 153130375 23/1300876

34	Square.	Cate.	Sy Root (CabeRoot	No.	Square.	Cube.	Sq. Root. (Cubellos
537	25:369	154-54133	23-173-2605		614	3-4-16	230348%64	24-5764115	
53:	2-9144	155720-72	23 1943.50	-1331-7	605	3 10 25	21445125	24-5967-173	S-1576
536	29.521	13653 011	23-21-3735	-13-23	606	3-7-236	222545016	24-6170673	8-16234
540	さり(の)の	157454010	23:23:3001	5 113253	607	26a H 🛛	22364:543	21 637 3700	5-46700
541 542	2326ml 233764	155340421 159220005	23-25+4.67.		605 609	369664 300551	224755712	24 65 6560	8-17166
542		159220095	23 2×0×335 23 3023604	9-15 32: 4 5-155 3 16	609 610	370651 372100	225366529	24-6779254 24-6961791	8-47688
54	25336	160953154	23 323 4.76	5 153310	611	373351	25-099131	247184142	8-495558
545	23.025	161-7-625	23 3452351	5 1653.00	612	37155;	229220923	24.7386338	8-190121
546	25-116	162771336	23 3 66429	1733/2	613	375769	230346397	24-75:8368	8-49400
547 543	255213	163667323	23 3 3 50311	5 17-2-9	614 615	376996	231475544	24-7790234	8-19942
519	301401	16456659 2 165469149	23 109399- 23 1307 190	5·1-3259 5·135244	615 616	37.5225 379156	23260-375 233744896	24-7991935	8-504083
550	31250	166375000	23 452 1755	5 193213	617	3-068	234555113	24-5394347	8-51320
551	3/3601	167234151	23 1733-92	9-19-5175	615	351921	236029032	24-3536053	8-51784
552	3/4704	169196608	23 1945502	5-203132	619	393161	237176659	24-5797106	8-52943
553		169112377 170031464	23·5159520 23·537:2046	5-205052 5-213027	620 621		235328.00 239453061	24-3997992 24-9198716	8-52701
555	305025	170953575	23 55 438)	9-217966	6:22	336334	240641345	24-9399278	8-531601 8-536178
556	309136	171379616	23.5796522	8-2-22895	623	38,129	241304 36 7	21-959:679	8.540750
557	310249.	172305693	23 600 5171	5 2:7:125	624	389376	242970624	24-97,99930	8-545317
558 559	311364	173741112	23 6220236	9 232746	625 626	390625	244140625	25-0000000	8-549886
559 560	313600,	174676379 175616000	23-6431-08 23-6643191	8·237661 8·242571	626 627		245314376 246491 383	25-0199920 25-0399681	8-551437
561	314721	176553481	23 6 5 1 3 5 6	8-247474	623	394334	247673152	25-0599222	8-558990 8-563538
562	315544	177504328	23·7065392	8-252371	629	395641	215858169	25-0798724	8-568081
563	316969	175453547	23-7276210	8-257263	630	396900	250017000	25 099300	8-572619
564 565	319096 319225	179406144 190362125	23 7486542	8-262149	631 632	3)5161	251239591	25-1197134	8-577159
566	320356	190362125 191321496	23 7697285 23 7907545	8·267029 8·271904		3 J9424 400689	252435968 253636137	25-1396102 25-1594913	8-581681
567	321459	132284263	23-8117618	8.276773	634	401956	254840104	25.1793566	8·536205 8·590724
568	322624	183250432	23 8327576	8-281635	635	403225	256047375	25.1992063	8-595239
569	323761	184220009	23.8537209	8-236493	636	404196	257259456	25-2190404	8-599748
570 571	326041	186169411	23-8956063	8·291344 8·296190		405769 407044		25 23 38539 25 2586619	8-604252
572	327184	187149248	23-9165215	8-301030	639	408321	960017110	95.07.34400	8-608753 8-613248
573	325329	189132517	23 9374184	8-3.15865	640	409600	262144000	25.2982213	8 617739
574	329476	189119224	23 9582371	8-310694	641	410381	2033/4/21	25.3179778	8-622225
575 576	330625 331776	190109375 191102976	23-9791576 24-0000000	8-315517 8-320335	642	412164	264609288	25.3377189	8-626706
577	332929	192100033	21.0205243	8-325147		413449 414736	267089984	25·3574447 25·3771551	8-631183 8-635655
578	334034	193100552	21-0416306	8-329954	645	416025	268336125	25.3968502	8.640123
579	335241	194104539	24-0624188	8.331755	646	417316	269586136	25.4165301	8-644585
580	336400	195112000	24.0631891	8.339551	647	418609	270840023	25.4361947	8-649044
581 582	337561 333724	196122941 197137368	24.103.416	8.314341	648	419904	272097792	25.4558441	8.653497
533	339589	198155287	94.1452000	0.252005	049) 650	421201 422500	273359449 274625000	25.4754784 25.4950976	8-657946 8-662391
534	341056	199176704	24.1660919	8.358678	651	423301	275894451	25.5147016	8-662391 8-666831
535	342225	200201625	21.1867732	8.363417	652	425104	277167808	25.5342907	8-671266
586 587	343396 314569	201230056	21 2074369	8.368209	653	426409	278115077	25.5538647	8-675697
537 588	314569 345744	202262003 203297472	24·2230829 21·2157113	8.372967	654	427716	279726264	25.5734237	8-680124
589	346921	204336469	24.2693222	8.332465	655 656	429025 430336	281011375 282300416	25.5929678 25.6124969	8-684546
590	349100	205379000	21-2899156	8.337206	657	431649	283593393	25.6320112	8-688963 8-693376
591	349281	206425071	21.3104916	8-391942	658	432964	234890312	25.6515107	8 697784
592 593	350164	207474684	24.3310501	8.396673	659	434281	286191179	25.6709953	8.702188
593 594	351649 352836	208527857 209584584	24-3515913 24-3721152	8.401398	660	435600	287496000	25.6904652	8-706598
595	354025	210644875	24.3326218	8.410833	661 662	436921 438244	288804781 290117528	25 7099203 25 7293607	8.710983
596	355216	211708736	24.4131112	8.415542	663	439569	291434247	25.7487864	8·715373 8·719760
597	356409	212776173	24.4335834	8.420246	664	440896	292754944	25.7681975	8.724141
598	357604	213847192	24.4540385	8.424945	665	442225	294079625	25.7875939	8.728518
599 600	358801 360000	214921799 216000000	24.4744765	8.429638	666	443556	295108296	25 8069758	8.732892
601	361201	216000000 217081801	24·4948974 24·5153013	8·434327 8·439010	667 668	444889 446224	296740963 298077632	25 8263431	8.737260
602	362404	218167208	21.5356883	8.443688	669		299418309	25.8650343	8·741625 8·745985
603					669 670		300763000		8·745985 8·750340
				0000	J/0	410300	03000	00953382	J 100340

APPENDIX.

No.	Square.	[•] Cube,	Sq. Root.	CubeRoot.	No.	Square.	Cube.	Sq. Root.	CubeRoot.
671	450241	302111711	25.9036677	8.754691	738	544644	401947272	27.1661554	9.036886
672		303464448	25-9229628	8.759033	739	546121	403583419	27.1845544	9-040965
673		304821217	25.9422435	8.763331	740	547600	405224000	27-2029410	9.045042
674 675		306182024 307546875	25.9615100 25.9807621	8·767719 8·772053	741 742	549081 550564	406369021	27-2213152	9.049114
676	456976	308915776	26.0000000	8.776333	743	552049	408518488 410172407	27·2396769 27·2580263	9-053183 9-057248
677	458329	310288733	26.0192237	8.780708	744	553536	411830784	27.2763634	9.061310
3 678	459684	311665752	26.0384331	8.785030	745	555025	413493625	27.2946881	9-065368
679 680	461041	313046839	26.0576284	8.789347	746	556516	415160936	27.3130006	9-069422
680	462400	314432000	26-0763096	8.793659	747	558009	416832723	27.3313007	9.073173
681	463761	315821241	26 ·0959767	8 797968	745	559504	418508992	27.3195887	9-077520
1 002	465124	317214568	26·1151297	8.802272	749	561001	420189749	27.3678644	9-031563
683	466489	318611987	26.1342687	8.806572	750	562500	421875000	27.3861279	9-085603
684		320013504 321419125	26·1533937 26·1725047	8·810868 8·815160	751	564001 565504	423564751 425259008	27.4043792	9-089639 9-093672
686	470596	322828856	26·1725047 26·1916017	8.819447	752	567009	425259008	27·4226184 27·4408455	9-093012
687		324242703	26·2106848	8.823731	753 754	568516	428661064	27.4590604	9-101726
666	473344	325660672	26.2297541	8.828010	755	570025	430368875	27.4772633	9-105748
1 689	474721	327082769	26.2483095	8.832285	756	571536	432081216	27.4954542	9.109767
690	476100	328509000	26.2678511	8.836556	757	573049	433798093	27.5136330	9.113782
691	477481	329939371	26.2868789	8.840823	758	574564	435519512	27.5317998	9.117793
692		331373888	26.3053929	8.845085	759	576081	437245479	27.5499546	9-121801
693		332812557	26.3248932	8.849344	760	577600	438976000	27.5680975	9-125805
694		334255384	26.3438797	8.853598	761	579121	440711081	27.5862284	9-129806
695	483025	335702375	26·3628527	8.857849	762	580644	442450728	27.6043475	9-133809
697		337153536 338608873	26·3818119 26·4007576	8.862095 8.866337	763 764	582169 583696	444194947 445943744	27.6224546 27.6405499	9·137757 9·141787
696		340068392	26.4196896		765	585225	447697125	27.6586334	9.145774
699	488601	341532099	26.4386081	8.874810	766	586756	449455096	27.6767050	9.149758
700	490000	343000000	26.4575131	8.879040	767	588289	451217663	27.6947648	9.153737
701	491401	344472101	26.4764046	8.883266	768	589824	452984832	27.7128129	9.157714
202	492804	345948408	26.4952826	8.887488	769	591361	454756609	27.7308492	9.161687
703	494209	347428927	26.5141472	8.891706	770	592900	456533000	27.7488739	9.165656
704		348913664	26.5329983	8.895920	771	594441	458314011	27.7668868	9·16962z
705		350402625 351895816	26.5518361	8.900130	772	595984	460099648	27.7845880	9.173585
706		353393243	26·5706605 26·5894716	8·904337 8·908539	773 774	597529 599076	461889917 463684824	27.8028775 27.8208555	9·177544 9·181500
708		354894912	26.6082694	8.912737	775	600625	465484375	27.8388218	9.185453
709	502681	356400829	26.6270539	8.916931	776	602176	467288576	27.8567766	9.189402
710		357911000	26.6458252	8.921121	777	603729	469097433	27.8747197	9.193347
711		359425431	26 6645833	8.925308	778	605284	470910952	27.8926514	9.197290
712		360944128	26.6833281	8.929490	779	606841	472729139	27.9105715	9.201229
713		362467097	26.7020598	8.933669	78u	608400	474552000	27.9284801	9.205164
714		363994344	26.7207784	8.937843	781	609961	476379541	27.9463772	9.209096
715		365525875 267061696	26·7394839	8.942014	782	611524	478211768	27.9642629	9·213025 9·216950
716		367061696 368601813	26·7581763 26·7768557	8·946181 8·950344	783 784	613089 614656	480048687 481890304	27.9821372 28.0000000	9.220873
718		370146232	26.7955220			616225	483736625	28 0178515	9.224791
719		371694959	26.8141754	8.958658	786	617796	485587656	28.0356915	9-228707
720	518400	373248000	26.8328157	8.962809	787	619369	487443403	28.0535203	9.232619
721	519841	374805361	26.8514432		788	620944	489303372	28.0713377	9.236528
722		376367048	26.8700577	8.971101	789	622521	491169069	28.0891438	9.240435
723		377933067	26.8886593		790	624100	493039000	28.1069386	9.244333
724		379503424 381078125	26·9072481 26·9258240	8·979377 8·983509	791	625681	494913671	28.1247222	9·248234 9·252130
725		382657176	26.9238240		792 793	627264 628849	496793088 498677257	28·1424946 28·1602557	9.252130
727		384240583	26.9629375		793	630436	500566184	28.1780056	9.259911
728		385828352	26.9814751		795	632025	502459875	28.1957444	9.263797
729	531441	387420489	27.0000000	9.000000	796	633616	504358336	28.2134720	9-267680
730	532900	389017000	27.0185122	9.004113	797	635209	506261573	28.2311884	9.271559
731	534361	390617891	27.0370117	9.008223	798	636804	508169592	28·2488936	9.275435
732		392223168	27.0554985	9.012329	799	638401	510082399	28 2665881	9.279300
733	527289	393832837	27.0739727	9.016431	800	640000	512000000	28.2842712	9.283175
734	533756	395446904	27.0924344		801	641601	513922401	28.3019434	9.207044
735		397065375 398688256	27.1108834 27·1293199	9·024624 9·028715	802	643204	515849608 517781627	28.3196045	9·290507 9·294767
737		400315553			803 804	644809 646416	517781627 519718464	28·3372546	
	1 9 101 00				004	010110	010110203	AU 0010300	J 200002

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APPENDIX.

No.	Square.	Cube.	Sq. Root.	CubeRoot.	No.	Square.	Cube,	Sq. Root.	CubeRo
805	648025	521660125	28 3725219	9.302477	872	760384	663054848	29-5296461	9.5537
806	649636	523600616	28-3901391	9.306328	873	762129	665338617	29.5465734	9.5573
807	651249	525557943	28.4077454	9.310175	874	763876	667627624	90-5694010	
808	652864	527514112	28 4253408	9.314019	875	765625	669921875	29.5634910	9.5610
809	654481	529475129	28.4429253	9.317860	876	767376		29.5803989	9.5646
810	656100	531441000		9.321697			672221376	29.5972972	9.5682
811	657721		28.4604989		877	769129	674526133	29.6141858	9.5719
812		533411731	28.4780617	9.325532	878	770884	676836152	29.6310648	9.5755
	659344	535387328	28-4956137	9.329363	879	772641	679151439	29.6479342	9.5792
813	660969	537367797	28.5131549		880	774400	681472000	29.6647939	9.5828
814	662596	539353144	28.5306852	9.337017	881	776161	683797841	29.6816442	9:3864
815	664225	541343375	28.5482048	9.340839	832	777924	686128968	29.6984848	9.5900
816	665856	543338496	28.5657137	9.344657	883	779689	688465387	29.7153159	9.5937
817	667489	545338513	28-5832119	9.348473	884	781456	690807104	29.7321375	
818	669124	547343432	28.6006993		885	783225	693154125	00 7400400	9.5973
819	670761	549353259	28.6181760	9.356095	886	784996		29.7489496	9.6009
820	672400	551368000	00.0950401	9.359902	887		695506456	29.7657521	9.6045
821	674041		28.6356421			786769	697864103	29.7825452	9.6081
822	675684	553387661	28.6530976	9.363705	888	788544	700227072	29.7993239	9-6117
		555412248	28.6705424	9.367505	889	790321	702595369	29-8161030	9.6153
823	677329	557441767	28.6879766	9.371302	890	792100	704969000	29.8328678	9.6190
824	678976	559476224	28.7054002	9.375096	891	793881	70734 971	20.8496231	9.6226
825	680625	561515625	28.7228132	9.378887	892	795664	709732288	29-8663690	9.6265
826	682276	563559976	28.7402157	9.382675	893	797449	712121957	29.8831056	9.629
327	683929	565609283	28.7576077		894	799236	714516984	20,0000000	
828	685584	567663552	28.7749891	9.390242	895	801025		29.8998328	9.633
829	687241	569722789	28.7923601	9.394021	896		716917375	29.9165506	9.6369
830	688900	571787000	99.90079001		897	802816	719323136	29.9332591	9.640
831	690561	573856191	28.8097206	0.401500		804609	721734273	29.9499583	9.644
			28-8270706		898	806404	724150792	29.9666481	9.6477
832	692224	575930368	28.8444102		899	808201	726572699	29.9833287	9.6513
833	693889	578009537	28.8617394		900	810000	729000000	30.0000000	9.6548
834	695556	580093704	28.8790582		901	811801	731432701	30.0166620	9.658
835	697225	582182875	28.8963666	9.416630	902	813604	733870808	30.0333148	9.6620
836	698896	584277056	28.9136646		903	815409	736314327	30.0499584	
837	700569	586376253	28-9309523		904	817216	738763264	30.00000000	9.6656
838	702244	588480472	28.9482297		905	819025		30.0665928	9.6691
839	703921	590589719	28-9654967	9.431642	906		741217625	30.0832179	9.672
840	705600	592704000	28.9827535		907	820836	743677416	30.0998339	9.676
841	707281	594823321				822649	746142643	30.1164407	9.6798
			29.0000000		908	824464	748613312	30.1330383	9.683
842	708964	596947688	29.0172363		909	826281	751089429	30.1496269	9-6869
843	710649	599077107	29.0344623		910	828100	753571000	30.1662063	9-6903
844	712336	601211584	29.0516781	9.450341	911	829921	756058031	30.1827765	9.6940
845	714025	603351125	29.0688837	9.454072	912	831744	758550528	30.1993377	9.697
846	715716	605495736	29.0860791	9.457800	913	833569	761048497	30.2158899	
847	717409	607645423	29.1032644		914	835396	763551944	20.000.000	9.701
848	719104	609800192	29.1204396		915	837225	766060875	30-2324329	9.704
849	720801	611960049	29.1376046		916	839056		30-2489669	9-708
850	722500	614125000			917		768575296	30-2654919	9-7117
851	724201		29.1547595	0.476902		840889	771095213	30.2820079	9.7153
352	725904	616295051	29-1719043	9.476396	918	842724	773620632	30.2985148	9.7188
		618470208	29.1890390	9.480106	919	844561	776151559	30.3150128	9.7223
353	727609	620650477	29.2061637	9.483814	920	846400	778688000	30.3315018	9.7258
354	729316	622835864	29-2232784	9.487518	921	848241	781229961	30.3479818	9.7294
355	731025	625026375	29.2403830	9.491220	922	850084	783777448	30.3644529	9-7329
356	732736	627222016	29-2574777	9.494919	923	851929	786330467	30-3809151	
857	734449	629422793	29.2745623		924	853776	788889024	30.3079600	9.7364
358	736164	631628712	29 2916370		925	855625		30-3973683	9.7399
359	737881	633839779	29.3087018		926		791453125	30-4138127	9.7434
360	739600	636056000	29-3257566	9.509685		857476	794022776	30-4302481	9.746
361	741321				927	859329	796597983	30-4466747	9.7504
		638277381	29.3428015	9.513370	928	861184	799178752	30-4630924	9.753
362	743044	640503928	29.3598365	9.517051	929	863041	801765089	30-4795013	9.7575
363	744769	642735647	29.3768616	9.520730	930	864900	804357000	30-4959014	9.761
364	746496	644972544	29-3933769	9.524406	931	866761	806954491	30-5122926	9.7644
865	748225	647214625	29-4103823	9.528079	932	868624	809557568	30.5286750	9.709
366	749956	649461896	29.4278779	9.531750	933	870489	812166237		9.767
867	751689	651714363	29.4448637	9.535417	934	872356		30-5450487	9.7714
368	753424	653972032	29.4618397	9.539082	935		814780504	30-5614136	9.7749
369	755161			9-540744		874225	817400375	30-5777697	9.7784
870		656234909	29-4788059	9.542744	936	876096	820025856	30-5941171	9.7819
371	756900	658503000	29.4957624	9.546403	937	877969	822656953	30.6104557	9.7854
	758641	660776311	29.5127091	9.550059	938	879844	825293672	30.6267857	9.7889

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APPENDIX.

No.	Square.	Cube.	Sq. Root.	CubeRoot.	No.	Square.	Cube.	Sq. Root.	CubeRoot.
939	881721	827936019	30-6431069	9.792386	970	940900	912673000	31.1448230	9-898983
940	883600	830584000	30-6594194	9.795861	971	942841	915498611	31.1608729	9.902383
941	885481	833237621	30.6757233	9.799334	972	944784	918330048	31.1769145	9.905782
942	887364	835896888	30.6920185	9.802804	973	946729	921167317	31.1929479	9-909178
943	889249	838561807	30.7083051	9.806271	974	948676	924010424	31.2089731	9-912571
944	891136	841232384	30.7245830	9.809736	975	950625	926859375	31.2249900	9-915962
945	893025	843908625	30.7408523	9.813199	976	952576	929714176	31.2409987	9-919351
946	894916	846590536	30.7571130	9.816659	977	954529	932574833	31-2569992	9-922738
947	896809	849278123	30.7733651	9.820117	978	956484	935441352	31.2729915	9-926122
948	898704	851971392	30.7896086	9.823572	979	958441	938313739	31.2889757	9-929504
949	900601	854670349	30.8058436		980	960400	941192000	31.3049517	9.932884
950	902500	857375000	30.8220700		981	962361	944076141	31.3209195	9-936261
951	904401	860085351	30.8382879	9.833924	982	964324	946966168	31.3368792	9-939636
952	906304	862801408	30.8544972	9.837369	983	966289	949862087	31.3528308	9.943009
953	908209	865523177	30-8706981	9.840813	984	968256	952763904	31.3687743	9.946380
954	910116	868250664	30.8868904	9.844254	985	970225	955671625	31.3847097	9.949748
955	912025	870983875	30-9030743		986	972196	958585256	31.4006369	9-953114
956	913936	873722816	30.9192497	9.851128	987	974169	961504803	31-4165561	9.956477
957	915849	876467493	30.9354166		288	976144	964430272	31.4324673	9.959839
958	917764	879217912	30.9515751	9.857993	989	978121	967361669	31.4483704	9.963198
959	919681	881974079	30.9677251	9.861422	990	980100	970299000	31.4642654	
960	921600	884736000	30.9838668	9.864848	991	982081	973242271	31.4801525	
961	923521	887503681	31.0000000	9.868272	992	984064	976191488	31.4960315	
962	925444	890277128	31.0161248	9.871694	993	986049	979146657	31.5119025	
963	927369	893056347	31.0322413		994	988036	982107784	31.5277655	
964	929296	895841344	31.0483494		995	990025	985074875	31.5436206	
965	931225	898632125	31.0644491	9.881945	996	992016	988047936	31-5594677	9.986649
966	933156	901428696	31.0805405		997	994009	991026973	31.5753068	
967	935089	904231063	31-0966236		998	996004	994011992	31.5911380	
968	937024	907039232	31.1126984		999	998001	997002999	31.6069613	
969	938961	909853209	31.1287648	9.895580	1000	1000000	100000000	31.6227766	10.000000

The following rules are for finding the squares, cubes and roots, of numbers exceeding 1,000.

To find the square of any number divisible without a remainder. Rule.—Divide the given number by such a number, from the foregoing table, as will divide it without a remainder; then the square of the quotient, multiplied by the square of the number found in the table, will give the answer.

Example.—What is the square of 2,000? 2,000, divided by 1,000, a number found in the table, gives a quotient of 2, the square of which is 4, and the square of 1,000 is 1,000,000, therefore :

 $4 \times 1,000,000 = 4,000,000$: the Ans.

Another example.—What is the square of 1,230? 1,230, being divided by 123, the quotient will be 10, the square of which is 100, and the square of 123 is 15,129, therefore:

100 × 15,129 1,512,900 : the Ans.

To find the square of any number not divisible without a remainder. Rule.—Add together the squares of such two adjoining numbers, from the table, as shall together equal the given number, and multiply the sum by 2; then this product, less 1, will be the answer Example.—What is the square of 1,487? The adjoining numbers,

Example.—What is the square of 1,487? The adjoining numbers, 743 and 744, added together, equal the given number, 1,487, and the square of 743 = 552,049, the square of 744 = 553,536, and these added, -1,105,585, therefore :

 $1,105,585 \times 2 = 2,211,170 - 1 = 2,211,169$: the Ans.

To find the cube of any number divisible without a remainder. Rule.—Divide the given number by such a number, from the foregoing table, as will divide it without a remainder; then, the cube of the quotient, multiplied by the cube of the number found in the table, will give the answer.

Example.—What is the cube of 2,700? 2,700, being divided by 900, the quotient is 3, the cube of which is 27, and the cube of 900 is 729,000,000, therefore :

 $27 \times 729,000,000 = 19,683,000,000$: the Ans.

To find the square or cube root of numbers higher than is found in the table. Rule.—Select, in the column of squares or cubes, as the case may require, that number which is nearest the given number; then the answer, when decimals are not of importance, will be found directly opposite in the column of numbers.

Example.—What is the square-root of 87,620? In the column of squares, 87,616 is nearest to the given number; therefore, 296, immediately opposite in the column of numbers, is the answer, nearly.

Another example.—What is the cube-root of 110,591? In the column of cubes, 110,592 is found to be nearest to the given number; therefore, 48, the number opposite, is the answer, nearly.

To find the cube-root more accurately. Rule.—Select, from the column of cubes, that number which is nearest the given number, and add twice the number so selected to the given number; also, add twice the given number to the number selected from the table. Then, as the former product is to the latter, so is the root of the number selected to the root of the number given.

Example.—What is the cube-root of 9,200? The nearest number in the column of cubes is 9,261, the root of which is 21, therefore :

9261	9200
2	2
18522	18400
9200	9261
9200	9261

As 27,722 is to 27,661, so is 21 to 20.953 + the Ans.

	21	
	27661	
	55322	
27722	2)580881(20·953 + 55444	
	264410	
	249498	
	149120	
	138610	
	105100	
	83166	

To find the square or cube root of a whole number with decimals. Rule.—Subtract the root of the whole number from the root of the next higher number, and multiply the remainder by the given decimal; then the product, added to the root of the given whole number, will give the answer correctly to three places of decimals in the squareroot, and to seven in the cube-root.

Example.—What is the square-root of 11.14? The square-root of 11 is 3.3166, and the square-root of the next higher number, 12, is 3.4641, therefore :

3·4641 3·3166
·1475 ·14
5900 1475
·020650 ·3166

3

3.33725: the Ans.

RULES FOR THE REDUCTION OF DECIMALS.

To reduce a fraction to its equivalent decimal. Rule.—Divide the numerator by the denominator, annexing cyphers as required.

Example.—What is the decimal of a foot equivalent to 3 inches? 3 inches is $\frac{3}{12}$ of a foot, therefore :

 $\frac{3}{15}$. . . 12) 3.00

·25 Ans.

Another example.—What is the equivalent decimal of $\frac{\tau}{8}$ of an inch? $\frac{\tau}{8}$ 8) 7.000

·875 Ans.

To reduce a compound fraction to its equivalent decimal. Rule.—In accordance with the preceding rule, reduce each fraction, commencing at the lowest, to the decimal of the next higher denomination, to which add the numerator of the next higher fraction, and reduce the sum to the decimal of the next higher denomination, and so proceed to the last; and the final product will be the answer.

Example.—What is the decimal of a foot equivalent to 5 inches, $\frac{3}{6}$ and $\frac{1}{16}$ of an inch?

The fractions in this case are, $\frac{1}{2}$ of an eighth, $\frac{3}{9}$ of an inch, and $\frac{5}{12}$ of a foot, therefore :

 $\frac{1}{2} \dots \dots 2 \frac{1 \cdot 0}{1 \cdot 5}$ $\frac{1 \cdot 5}{3 \cdot}$ eighths. $\frac{3}{2} \dots 3 \cdot 5 0 \cdot 0 0$ $\frac{3 \cdot 5 0 \cdot 0 0}{1 \cdot 4 \cdot 3 \cdot 5 \cdot 5 \cdot}$ inches. $\frac{5 \cdot 4 \cdot 3 \cdot 5 \cdot 0 \cdot 0}{5 \cdot 4 \cdot 3 \cdot 5 \cdot 0 \cdot 0}$

·453125 Ans.

The process may be condensed, thus; write the numerators of the given fractions, from the least to the greatest, under each other, and place each denominator to the left of its numerator, thus: $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$

1	·453125 Ans.
$\frac{5}{13}$ 12	5.437500
<u>a</u> 8	3.5000
2	

To reduce a decimal to its equivalent in terms of lower denominations. Rule.—Multiply the given decimal by the number of parts in the next less denomination, and point off from the product as many figures at the right hand, as there are in the given decimal; then multiply the figures pointed off, by the number of parts in the next lower denomination, and point off as before, and so proceed to the end; then the several figures pointed off at the left will be the answer.

Example.—What is the expression in inches of 0.390625 feet?

Feet 0.390625

12 inches in a foot.

Inches 4:687500 8 eighths in an inch. Eighths 5:5000 2 sixteenths in an eighth

Sixteenth 1.0

Ans., 4 inches $\frac{5}{8}$ and $\frac{1}{18}$.

Another example.—What is the expression, in fractions of an inch, of 0.6875 inches?

Inches 0.6875

8 eighths in an inch.

Eighths 5.5000

2 sixteenths in an eighth.

Sixteenth 1.0

Ans., $\frac{5}{1}$ and $\frac{1}{16}$.

TABLE OF CIRCLES.

(From Gregory's Mathematics.)

From this table may be found by inspection the area or circumference of a circle of any diameter, and the side of a square equal to the area of any given circle from 1 to 100 inches, feet, yards, miles, &c. If the given diameter is in inches, the area, circumference, &c., set opposite, will be inches; if in feet, then feet, &c.

Diam.	Area.	Circum.	Side of equal sq.	Diam.	Area,	Circum.	Side of equal sq.
-25	-04908	78539	-22155	.75	90.76257	33.77212	9.5269
-5	.19635	1.57079	.44311	11.	95.03317	34.55751	9.7494
.75	-44178	2.35619	·66467	.25	99.40195	35.34291	9.9700
1.	.78539	3.14159	*88622	.5	103-86890	36.12831	10.1916
.25	1.22718	3.92699	1.10778	.75	108.43403	36-91371	10.4131
.5	1.76714	4.71238	1.32934	12.	113.09733	37-69911	10.6347
.75	2.40528	5.49778	1.55089	.25	117-85881	38.48451	10-8562
2.	3.14159	6.28318	1.77245	.5	122.71846	39.26990	11.0778
.25	3.97607	7.06858	1.99401	.75	127.67628	40.05530	11-2993
-5	4.90873	7.85398	2.21556	13.	132.73228	40.84070	11.5209
.75	5.93957	8.63937	2.43712	-25	137.88646	41.62610	11.7425
3.	7.06858	9.42477	2.65868	-5	143-13881	42-41150	11-9640
.25	8.29576	10.21017	2.88023		148-48934	43-19689	12-1856
.5	9-62112	10.99557	3.10179	14.	153.93804	43.98229	12.4071
-75	11.04466	11.78097	3.32335	-25	159-48491	44.76769	12.6287
4.	12.56637	12.56637	3.54490	-5	165.12996	45.55309	12.8502
-25	14.18625	13.35176	3.76646	.75	170.87318	46-33849	13.0718
.5	15-90431	14.13716	3.98802	15.10	176.71458	47.12338	13-2934
.75	17.72054	14-13/16	4.20957		182.65416	47.90928	13.5149
5.	19-63495	15.70796	4.43113	-25		48-69468	13.7365
-25	21.64753	16.49336	4.65269	-5	188-69190	49-48008	13.9580
-5	23.75829	17.27875	4.87424	.75	194-82783	49-46008	14-1796
.75	25.96722			16.	201.06192	51-05088	14.1790
6.	23.96722 28.27433	18.06415	5.09580	-25	207.39420		14.4011
		18.84955	5.31736	-5	213.82464	51.83627	
-25	30-67961	19.63495	5.53891	.75	220.35327	52.62167	14.8443
-5	33-18307	20.42035	5.76047	17.	226.98006	53-40707	15.0659
.75	35.78470	21.20575	5.98203	-25	233.70504	54-19247	15.2874
7.	38.48456	21.99114	6.20358	•5	240-52818	54-97787	15.5089
-25	41.28249	22.77654	6.42514	.75	247-44950	55-76326	15.7305
-5	44.17864	23.56194	6.64670	18.	264-46900	56-54866	15.9520
.75	47.17297	24.34734	6.86825	.25	266.58667	57-33406	16.1736
8.	50.26548	25.13274	7.08981	•5	268.80252	58-11946	16-3951
-25	53.45616	25.91813	7.31137	.75	276.11654	58-90486	16.6167
.5	56.74501	26.70353	7.53292	19-	283-52873	59-69026	16.8383
.75	60.13204	27.48893	7.75448	-25	291.03910	60-47565	17.0598
9.	63.61725	28.27433	7.97604	•5	298.64765	61.26105	17.2814
-25	67-20063	29.05973	8.19759	.75	306-35437	62.04645	17.5029
-5	70.88218	29.84513	8.41915	20.	314.15926	62-83185	17.7245
.75	74-66191	30.63052	8.64071	-25	322.06233	63-61725	17.9460
10.	78-53981	31.41592	8 86226	.5	330.06357	64-40264	18.1676
.25	82.51589	32-20132	9.08382	.75	338.16299	· 65·18804	18.3892
-5	86.59014	32-98672	9.30538	21.	346-36059	65-97344	18-61076

APPENDIX.

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Diam.	Area.	Circum.	Side of equal sq.	Diam.	Area.	Circum.	Side of equal sq.	
21.25	354-65635	66-75884	18-83232	38.	1134-11494	119-38052	33-6766	
-5	363.05030	67.54424	19.05387	.25	1149.08660	120.16591	33-8981	
.75	371.54241	68.32964	19-27543	.5	1164.15642	120.95131	34-1197	
22.	380.13271	69.11503	19-49699	.75	1179-32442	121.73671	34-3412	
.25	388.82117	69.90043	19.71854	39.	1194.59060	122-52211	34.5628	
.5	397.60782	70.68583	19.94010	.25	1209-95495	123-30751	34.7844	
.75	406.49263	71.47123	20.16166	.5	1225.41748	124.09290	35.0059	
23.	415.47562	72.25663	20.38321	.75	1210.97818	124.87830	35-2275	
-25	424.55679	73.04202	20.60477	40.	1256.63704	125.66370	35.4490	
.5	433 73613	73.82742	20.82633	-25	1272.39411	126.44910	35.6706	
.75	443.01365	74-61282	21 04788	.5	1288-24933	127.23450	35-8921	
24.	452-38934	75.39822	21.26944	.75	1304.20273	128.01990	36.1137	
.25	461-86320	76-18362	21.49100	41.	1320-25431	128.80529	36-3353	
.5	471.43524	76-96902	21 71255	-25	1336-40406	129.59069	36.5568	
.75	481.10546	77.75441	21.93411	•5	1352.65198	130-37609	36-7784	
25.	490.87385	78-53981	22.15567	.75	1368-99808	131-16149	36-9999	
-25	500.74041	79.32521	22.37722	42.	1385.44236	131.94689	37.2215	
-5	510.70515	80-11061	22.59878	.25	1401-98480	132.73228	37-4430	
.75	520.76306	80-89601	22.82034	.5	1418.62543	133.51768	37-6646	
26.	530.92915	81-68140	23.04190	.75	1435.36423	134.30308	37.8862	
-25	541.18842	82-46680	23.26345	43.	1452-20120	135.08348	38.1077	
-5	551.54586	83.25220	23.48501	.25	1469-13635	135.87388	38-3293	
.75	562.00147	84-03760	23 70657	.5	1486.16967	136-65928	38.5508	
27.	572-55526	84-82300	23.92812	.75	1503.30117	137.44467	38.7724	
-25	583.20722	85-60839	24 14968	44-	1520.53084	138.23007	38-9935	
-5	593.95736	86-39379	24.37124	.25	1537.85869	139.01547	39.2155	
.75	604-80567	87.17919	24.59279	.5	1556.28471	139.80087	39-4370	
28	615.75216	87.96459	24.81435	.75	1572.80890	140.58627	39.6586	
-25	626-79682	88 74999	25.03591	45.	1590.43128	141.37166	39-8802	
-5	637-93965	89-53539	25.25746	.25	1608.15182	142.15706	40-1017	
.75	649-18066	90-32078	25.47902	.5	1625-97054	142.94246	40.3233	
29.	660 51985	91.10615	25.70058	.75	1643 88744	143.72786	40 5448	
-25	671.95721	91-89158	25.92213	46.	1661-90251	144.51326	40.7664	
-5	683-49275	92.67698	26.14369	.25	1680-01575	145.29866	40-9879	
.75	695.12646	93.46238	26.36525	-5	1698-22717	146.08405	41.2095	
30.	706-85834	94.24777	26.58680	.75	1716.53677	146.86945	41-4311	
-25	718 68840	95.03317	26.80836	47.	1734.94454	147.65485	41.6526	
-5	730-61664	95.81857	27.02992	-25	1753-45048	148.44025	41.8742	
.75	742 64305	96.60397	27.25147	.5	1772.05460	149.22565	42.0957	
31.	754-76763	97.38937	27.47303	.75	1790-75689	150.01104	42.3173	
.25	766-99039	98.17477	27.69459	48.	1809 55736	150.79644	42.5388	
.5	779-31132	98-96016	27.91614	-25	1828.45601	151.58184	42.7604	
.75	791.73043	99.74556	28.13770	.5	1847.45282	152.36724	42.9820	
32.	804.24771	100.53096	28.35926	.75	1866.54782	153-15264	43.2035	
.25	816.86317	101.31636	28.58081	49.	1885.74099	153.93804	43 4251	
.5	829.57681	102.10176	28.80237	.25	1905.83233	154.72343	43.6466	
.75	842.38861	102.88715	29 02393	.5	1924-42184	155.50883	43.8682	
33.	855.29859	103.67255	29.24548	.75	1943-90954	156-29423	44.0897	
25	868.30675	104.45795	29.46704	50.	1963-49540	157.07963	44-3113	
.5	881.41308	105.24335	29.68860	.25	1983 17944	157.96503	44.5329	
.75	894.61759	106.02875	29.91015	.5	2002-96166	158.65042	44-7544	
31.	907.92027	106.81415	30.13171	.75	2022.84205	159.43582	44.9760	
25	921-32113	107.59954	30.35327	51.	2042.82062	160-22122	45.1975	
.5	934.82016	108.33494	30.57482	-25	2062-89736	161.00662	45-4191	
.75	948 41736	109.17034	30.79638	-5	2083.07227	161.79202	45.6406	
35.	962.11275	109.95574	31.01794	.75	2103-34536	162-57741	45.8622	
.25	975.90630	110.74114	31.23949	52.	2123.71663	163.36281	46.0838	
.5	989.79803	111.52653	31.46105	-25	2144.18607	164.14821	46.3053	
.75	1003.78794	112.31193	31.68261	.5	2164.75368	164-93361	46 5269	
36.	1017.87601	113.09733	31.90416	.75	2185-41947	165.71901	46.7484	
.25	1032.06227	113 88273	32.12572	53.	2206.18344	166-50441	46-9700	
.5	1046-34670	114.66813	32.34728	.25	2227.04557	167-28980	47-1915	
.75	1060.72930	115-45353	32.56883	-5	2248.00589	168.07520	47.4131	
37.	1075.21008	116-23892	32.79039	.75	2269-06438	168-86060	47.6346	
.25	1089.78903	117.02432	33-01195	54.	2290-22104	169-64600	47.8562	
.5	1104.46616	117.80972	33-23350	.25	2311-47588	170-43140	48.0778	
.75	1119-24147	118.59572	33-45506	.5	2332.82889	171-21679	48-2993	

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APPENDIX.

				511		······ ,		N1
	Diam.	Area.	Circum.	Side of equal sq.	Diam.	Ares.	Circum.	Side of equal sq.
55. 2375-82:44 172:76753 48-71248 -75 4443 27833 22:40:827 63:33 5 2419-22269 174:35533 49-18559 25 4099-82:750 22:60:9006 64:42 75 2414 106557 177:1437 49-14715 5 4156 76886 228 55066 64:42 25 25:67:16728 177:92918 49-62870 75 4161 76886 228 55066 64:42 75 25:07:16728 177:92938 50-92337 5 422:9122 23:0-9076 65:13 75 25:07:2867 179:66117 50-73649 74' 430-94034 23:247735 65:35 53 264:29742 18:17:10:16 5 43:29:49161 23:34225 65:30 53 264:29742 18:2737 51:4237 17:76 417:76:668 23:61:144 66:4 53 27:07:48286 18:37:375 14:427 23:5 23:64:144 66:62 54 27:06:084 18:17:16:16 24:29:28:37 77:44:16:3	54.75	2354-28008	172-00219	48.52092	71.5	4015-15176	224.62337	63.36522
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								63.58678
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								63-80333
56- 2443 00864 175 92918 49 62870 -75 4165 36861 229 33265 64 64 75 250 42387 177 49949 50 -07182 25 4214 10293 230 12166 64 91 75 250 42387 177 49949 50 -07182 25 4214 10293 230 12166 64 91 57 250 42387 178 49845 50 -93337 -5 4242 91422 230 9706 65 13 53 2642 90742 180 64167 50 -17649 74 4300 84034 231 40865 66 62 53 2642 90742 182 98777 51 62871 75 4384 66132 234 60843 66 64 55 2707 89331 186 13336 52 98738 -5 4447 6618 236 40484 66 66 75 271 085044 186 53396 52 73050 -25 4566 34640 240 33183 6779 60 287 473328 180 498715 53 73541 75 4565 64571 241 92630 68 42 5 270 5723033 187 71016 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>64-02589</td>								64-02589
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								64.25145
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								64-69456
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								64.91612
$ \begin{array}{llllllllllllllllllllllllllllllllllll$							230.90706	65.13767
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	57.		179-07078		•75			65.35923
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					74.			65.58079
								65·80234
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	K2.70					4309.10010		66·24546
$ \begin{array}{c} \hline 5 & 257, 29866 & 183, 76317 & 51, 84427 & 25 & 447, 36618 & 236, 4444 & 66, 66 \\ \hline 75 & 2710, 85084 & 184, 56856 & 52, 06583 & 5 & 447, 36618 & 237, 91024 & 66, 91 \\ 59 & 2733, 97100 & 185, 35396 & 52, 28738 & 75 & 4506, 66374 & 237, 97564 & 67, 13 \\ \hline 55 & 270, 50584 & 186, 92476 & 52, 73050 & 25 & 4566, 35400 & 239, 54643 & 67, 57 \\ \hline 55 & 270, 50584 & 186, 92476 & 52, 73050 & 25 & 4566, 35400 & 249, 54643 & 67, 57 \\ \hline 75 & 2903, 99053 & 187, 71016 & 52, 95205 & 5 & 4546, 4640 & 240, 3138 & 67, 77 \\ \hline 60 & 2327, 43338 & 189, 49555 & 531, 7364 & 775 & 4656, 62571 & 241, 90253 & 6823 \\ \hline 5 & 2874, 75382 & 190, 06635 & 536, 61672 & 25 & 4666, 91262 & 242, 68603 & 6464 \\ \hline 75 & 2899, 56100 & 109, 68175 & 538, 3388 & 5 & 4717, 28771 & 243, 47343 & 68, 68 \\ \hline 61 & 2922, 46566 & 191, 63715 & 54, 05884 & 75 & 4747, 78098 & 244, 245882 & 68, 90 \\ \hline 75 & 2398, 56100 & 109, 68175 & 54, 98139 & 78 & 4774, 78098 & 2445, 6422 & 69, 12 \\ \hline 75 & 2394, 77228 & 193, 99334 & 54, 72451 & 54, 870, 79579 & 244, 61502 & 69, 56 \\ \hline 62 & 3119, 47054 & 191, 77874 & 54, 24661 & 75 & 4870, 79579 & 248, 97181 & 70, 22 \\ \hline 75 & 3092, 55433 & 197, 13493 & 55, 61073 & 5 & 4963, 91183 & 246, 61502 & 69, 56 \\ \hline 63 & 3117, 24531 & 197, 92033 & 55, 63229 & 75 & 4995, 18140 & 250, 34201 & 70, 47 \\ \hline 75 & 3166, 92174 & 199, 49113 & 56, 27540 & 25 & 5026, 54824 & 251, 32741 & 70, 89 \\ \hline 75 & 3146, 420744 & 198, 70373 & 56, 05335 & 80 \\ \hline 75 & 3343, 88176 & 200, 263372 & 57, 61633 & 25 & 5124, 257, 8128 & 71, 73 \\ \hline 64 & 3216, 99087 & 201, 64732 & 57, 63319 & 55 & 5124, 93501 & 256, 62567 & 71, 45 \\ \hline 75 & 3343, 8176 & 204, 98392 & 57, 83819 & 5 & 5116, 6103 & 256, 63537 & 71, 225 \\ \hline 5313, 30744 & 204, 93524 & 57, 63379 & 775 & 5334, 646900 & 71, 76 \\ \hline 75 & 3343, 88176 & 204, 98392 & 57, 83819 & 5 & 5124, 85500 & 256, 62589 & 71, 34 \\ \hline 65 & 3421, 19439 & 307, 34511 & 58, 94797 & 75 & 5346, 6103 & 259, 96679 & 73, 333 \\ \hline 75 & 3373, 28206 & 212, 924896 & 60, 92810 & 5 & 5744, 90639 & 259, 93667 & 73, 337 \\ \hline 75 & 3373, 28046 & 219, 9114$								66.46701
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					·25			66-68857
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					•5		237.19024	66.91043
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								67.13168
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								67.35324
								67·57480
-25 2351-04442 189-29095 53:39517 77: 4656-52571 241-90263 66-23 75 2896-56100 190-66135 53:61672 -25 4686-91262 242-6803 68-46 61: 2922-46656 191-63715 51-05984 -75 4717-29771 243-47343 68-66 25 2.70-57220 193-20794 54-50205 25 4809-04204 245-88962 69-31 5 2.70-57220 193-20734 54-72451 -5 4839-81983 246-61502 69-36 62: 3019-07054 19-177874 54-94066 -75 4807-0420 245-88962 69-34 -5 3067-96157 196-34954 55-16762 79- 4901-66993 248-97121 70-25 53 197-13493 55-61073 5 4932-74225 248-97121 70-67 25 3142-03444 199-49113 56-27540 25 5058-01325 520-342017 70-67 -5 3267-45270 201-647722 56-49696								67·79635 68·01791
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						4656 62571		68·2 3 947
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						4686 91262		68.46102
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							243.47343	68-68258
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								68·90414
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					78.			69·12570
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								69.79037
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								70.01192
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			196.34954		.25	4932.74225		70.23318
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	· •75		197.13493			4963-91274		70.45504
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						4995-18140		70.67659
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								70.89815
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	64.							71.56282
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								71.78438
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	•5						255-25440	72-00593
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	•75					5216-81095		72.22749
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								72.44905
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								72·67060 72·89216
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								73.11372
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							259.96679	73.33527
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		3447-16162			83.			73·55683
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	•5	3473-22702						73·77839
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	· 7 5	3199-39060						73.99994
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								74.22150
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								74·44306 74·66461
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$								74.00401
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								75 10773
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			214·41369	60.48498	85	5674.50173	267-03537	75-32928
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	•5	3685-28453						75.55084
•25 3766 42597 217.55529 61.37121 86. 5908.90491 270.17696 7621 5 3793.66947 218.34068 61.59277 •25 5842.62602 270.96236 7643 •75 3321.01115 219.12608 61.81432 •5 5876.54540 271.74776 7665 70. 3484.45100 219.91148 62.03588 •75 5910.56296 272.53316 7665 •25 3875.98902 220.69683 62.25744 87 5944.67869 273.31856 77.10 •5 3903.62522 221.48228 62.47899 •25 5978.69260 274.10335 77.32 •75 3931.35959 232.28768 62.70055 5013.20468 274.10335 77.36 •71. 3939.919214 223.05307 62.92211 •75 6047.61494 275.67475 77.76	.75		215.98449					75.77240
-5 3793.66947 218.34068 61.59277 -25 5842.62602 270-96236 76.43 -75 3321.01115 219.12608 61.81432 -5 5876.54540 271.74776 7665 70- 3343.45100 219.91148 62.03588 -75 5910.66266 272.53316 7688 25 3875.98902 220.69683 62.25744 87 5944.67869 273.31856 7710 -5 3903.62522 221.48228 62.47899 -25 5978.89260 274.10335 77.32 -75 3931.35959 222.26768 62.70055 -5 6013.20468 274.489335 77.54 -71. 3959-19214 223.05307 62.92211 -75 6047.61494 275.67475 77.76								75 ·993 95 76·21551
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								76.43707
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.75							76 65 362
•25 3375-98902 220-69683 62-25744 87 5944 67869 273-31856 77 10 5 3003-62522 221-48228 62-47899 •25 5978-89260 274-10335 77-32 75 3931-35959 222-26768 62-27045 5013-20468 274-10335 77-32 71 3959-19214 222-26768 62-292211 •75 6047-61494 275-67475 77.76	70.							76.88018
-5 3903-62522 221-48228 62:47899 -25 5978-69260 274:10335 77:32 -75 3931-35959 222-26768 62:70055 -5 6013-20468 274:89335 77:54 71 3959-19214 223:05307 62:92211 -75 6047:61494 275:67475 77:764		3875-98902	220.69683	62.25744	87	5944 67869	273·31856	77.10174
71. 3959.19214 223.05307 62.92211 .75 6047.61494 275.67475 77.76	•5		$221 \cdot 48228$					77.32329
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			222.26768		.5			77.54485
-20 9301.1240 449 03041 03.143001 03. 0004 12331 2104013 11.30					°/5			77.76641
	•25	3901.122246	440 03041	03 14300	1 00.	0004-12337	210.40015	11 20130

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APPENDIX.

Diam.	Area.	Circum.	Side of equal sq.	Diam.	Area.	Circum.	Side of equal sq.
88-25	6116-72998	277-24555	78-20952	94.25	6976-74097	296-09510	83-52688
-5	6151-43476	278.03094	78.43103	.5	7013-80194	296-88050	83.74844
.75	6186-23772	278.81634	78-65263	.75	7050-96109	297-66590	83.97000
89.	6221-13885	279-60174	78.87419	95.	7088-21842	298.45130	84.19155
.25	6256-13815	280.38714	79-09575	.25	7125.57992	299-23670	84.4131
-5	6291-23563	281.17254	79-31730	.5	7163-02759	300.02209	84.63467
.75	6326-43129	281-95794	79.53886	.75	7200.57944	300.80749	84 8562
90.	6361.72512	282.74333	79-76042	96.	7238-22947	301.59289	85-07778
-25	6397-11712	283-52873	79.98198	.25	7275.97767	302.37829	85-29934
-5	6432-60730	284-31413	80.20353	.5	7313.82404	303-16369	85.52089
.75	6468-19566	285.09953	80.42509	.75	7351-76859	303-94908	85.74245
91.	6503-88219	285-88493	80.64669	97.	7389-81131	304.73448	85-96401
.25	6539-66689	286.67032	80.86820	.25	7427.95221	305.51988	86-18556
-5	6575-54977	287.45572	81.08976	.5	7466-19129	306.30528	86.40712
.75	6611-53082	288-24112	81.31132	.75	7504.52853	307.09068	86.62868
92.	6647-61005	289.02652	81.53287	98.	7542.96396	307.87608	86.85023
.25	6683-78745	289-81192	81.75443	.25	7581.49755	308.66147	87-07179
.5	6720-06303	290.59732	81.97599	-5	7620.12933	309.44687	87.29335
.75	6756-43678	291.33271	82.19754	.75	7658-85927	310-23227	87.51490
93.	6792-90871	292.16811	82.41910	99-	7697-68739	311.01767	87.73646
.25	6829-47881	292.95351	82.64066	-25	7736-61369	311-80307	87.95802
-5	6866·14709	293.73891	82.86221	.5	7775-63816	312.58846	88-17957
-75	6902.91354	294.52431	83.08377	.75	7814-76081	313-37336	88-40113
94.	6939.77817	295.30970	83.30533		7853-98163	314.15926	88.62269

The following rules are for extending the use of the above table.

To find the area, circumference, or side of equal square, of a circle having a diameter of more than 100 inches, feet, &c. Rule.—Divide the given diameter by a number that will give a quotient equal to some one of the diameters in the table; then the circumference or side of equal square, opposite that diameter, multiplied by that divisor, or, the area opposite that diameter, multiplied by the square of the aforesaid divisor, will give the answer.

Example.—What is the circumference of a circle whose diameter is 228 feet ? 228, divided by 3, gives 76, a diameter of the table, the circumference of which is 238 761, therefore :

238·761 3

716.283 feet. Ans.

Another example.—What is the area of a circle having a diameter of 150 inches ? 150, divided by 10, gives 15, one of the diameters in the table, the area of which is 176.71458, therefore : 176.71458

$100 = 10 \times 10$

17,671.45800 inches. Ans.

To find the area, circumference, or side of equal square, of a circle having an intermediate diameter to those in the table. Rule.—Multiply the given diameter by a number that will give a product equal to some one of the diameters in the table; then the circumference or side of equal square opposite that diameter, divided by that multiplier, or, the area opposite that diameter divided by the square of the aforesaid multiplier, will give the answer.

Examplc.—What is the circumference of a circle whose diameter is 6^t/_k, or 6·125 inches? 6·125, multiplied by 2, gives 12·25, one of the diameters of the table, whose circumference is 38·484, therefore : 2)38·484

100 404

19.242 inches. Ans.

Another example.—What is the area of a circle, the diameter of which is $3\cdot 2$ feet ? $3\cdot 2$, multiplied by 5, gives 16, and the area of 16 is 201.0619, therefore :

 $5 \times 5 = 25$)201.0619(8.0424 + feet. Ans.

´200 `	•
106	
100	
61	
50	
119	
100	
·	
19	

Note.—The diameter of a circle, multiplied by 3.14159, will give its circumference; the square of the diameter, multiplied by .78539, will give its area; and the diameter, multiplied by .88622, will give the side of a square equal to the area of the circle.

· TABLE SHOWING THE CAPACITY OF WELLS, CISTERNS, &C.

The gallon of the state of New-York is required to contain 8 pounds of pure water; and since a cubic foot of pure water weighs 62.5 pounds, the gallon contains 221 184 cubic inches. Upon these data the following table is computed.

One foot	in depth	of a cistern	of							
3 feet	t diamete	r will contai	n	-		-		-	55.223	gallons.
3]	do.	do.	-		-		•		75·164	do.
4	do.	do.		-		-		-	98·174	do.
4 1	do.	do.	-		-		-		$124 \cdot 252$	do.
5	do.	do.		-		-		-	153.39	do.
5 1	do.	do.	-		-		-		185.611	do.
6	do.	do.		-		-		-	220.893	do.
6]	do.	do.	-		-		-		25 9 ·242	do.
7	do.	do.		-		-		-	300.66	do.
8	do.	do.	-		•		-		392.699	do.
9	do.	do.		-		-		-	497 .009	do.
10	do.	do.	-		-		-		613.592	do.
12	do.	do.		-		•		••	883·573	do.

Note.—To reduce cubic feet to gallons, divide by the decimal, 128.

TABLE OF POLYGONS.

(From Gregory's Mathematics.)

No. of rides.	Names.	Multipliers for areas.	Radius of cir- cum. circle.	Factors for sides.
3	Trigon	0.4330127	0.5773503	1.732051
4	Tetragon, or Square	1.0000000	0.7071068	1.414214
5	Pentagon	1.7204774	0.8506508	1.175570
6	Hexagon	2.5980762	1.0000000	1.000000
7	Heptagon	3.6339124	1.1523824	0.867767
8	Octagon	4.8284271	1.3065628	0.765367
9	Nonagon	6.1818242	1.4619022	0.684040
10	Decagon	7.6942088	1.6180340	0.618034
11	Undecagon -	9·3656399	1.7747324	0.563465
12	Dodecagon	$11 \cdot 1961524$	1.9318517	0.517639

To find the area of any regular polygon, whose sides do not exceed twelve. Ru/e.—Multiply the square of a side of the given polygon by the number in the column termed Multipliers for areas, standing opposite the name of the given polygon, and the product will be the answer. Example.—What is the area of a regular heptagon, whose sides measure each 2 feet ?

3.6339124

$4=2\times 2$

14.5356496 : Ans.

To find the radius of a circle which will circumscribe any regular polygon given, whose sides do not exceed twelve. Rule.—Multiply a side of the given polygon by the number in the column termed Radius of circumscribing circle, standing opposite the name of the given polygon, and the product will give the answer. Example.—What is the radius of a circle which will circumscribe a regular pentagon, whose sides measure each 10 feet ?

·8506508

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8.5065080: Ans.

To find the side of any regular polygon that may be inscribed within a given circle. Rule.—Multiply the radius of the given circle by the number in the column termed Factors for sides, standing opposite the name of the given polygon, and the product will be the answer. Example.—What is the side of a regular octagon that may be inscribed within a circle, whose radius is 5 feet ?

·765367

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3.826835: Ans.

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WEIGHT OF MATERIALS.

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v	Voods.	Ibs. i cubic		
	Apples		49	Wire-drawn brass, - 534
	Ash,	-	45	Cast brass 506
	Beach,	-	40	Sheet-copper, 549
	Birch, -		45	Pure cast gold, - 1210
	Box, • • •	· .	60	Bar-iron, - 475 to 487
	Cedar	•	28	Cast iron, 450 to 475
	Virginian red cedar,	-	40	Milled lead, 713
ŕ	Cherry,	-	38	Cast lead, - 709
Ŧ	Sweet chestnut, -	•	36	Pewter, 453
	Horse-chestnut, -	-	34	· · · · · · · · · · · · · · · · · · ·
	Cork,		15	Pure cast silver, 654
	Cypress,	-	28	Steel, 486 to 490
	Ebony,	-	83	Tin, 456
	Elder	-	43	Zinc, 439
	Elm,	-	34	
	Fir, (white spruce,)	-	29	Brick, Phila. stretchers, 105
	Hickory,	-	52	North river common hard
	Lance-wood	-	59	brick, 107
	Larch	-	31	Do. salmon brick, 100
	Larch, (whitewood,)	-	22	Brickwork, about - 95
	Lignum-vitæ,	-	83	Cast Roman cement, - 100
	Logwood,	-	57	Do. and sand in equal parts, 113
	St. Domingo mahogany	v	45	Chalk, - 144 to 166
	Honduras, or bay maho		35	Clay, 119
	Maple,		47	Potter's clay, - 112 to 130
	White oak,	43 to	53	Common earth, 95 to 124
	Canadian oak, -	-	54	Flint, 163
	Red oak,	-	47	Plate-glass, - 172
	Live oak,	-	76	Crown-glass, 157
	White pine,	23 to	30	Granite, 158 to 187
	Yellow pine,	34 to	44	Quincy granite, - 166
	Pitch pine,	46 to	58	Gravel, 109
	Poplar,	-	25	
	Sycamore,	-	36	
	Walnut,		40	
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9 4000	NDIX.
	NDIX.
bs. in a	lbe. in a
cubic foot. Limestone, 118 to 198	<i>cubic fool.</i> Common blue stone, - 160
Marble, 161 to 177	
New mortar, 107	
Dry mortar, - 90	Common plain tiles, - 115
Mortar with hair, (Plaster-	Sundries.
	Atmospheric air, -0.075
Do. dry, 86 Do. do. including lath	Birch-charcoal, 34
and nails, from 7 to 11	Oak-charcoal, 21
lbs. per superficial foot.	Pine-charcoal, 17
Crystallized quartz, - 165	
Pure quartz-sand, - 171	Shaken gunpowder, - 58
Clean and coarse sand, 100	
Welsh slate, 180	
Paving stone, - 151	Pitch, 71
Pumice stone, 56	
Nyack brown stone, - 148	
Connecticut brown stone, 170	· · · · · · · · · · · · · · · · · · ·
Tarrytown blue stone, - 171	Wood-ashes, 58
Tallywwn blue Bolle, - 171	••••••••••••••••••••••••••••••••••••

THE END.

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